Talon Metals Corp
Eagle Mine

NI 43-101 Technical Report on the Eagle Mine, Michigan, USA

Effective date of Technical Report: April 29,2026

Effective date of Mineral Resources and Reserves Estimate: February 28,2026

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Document Distribution

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1. Summary

1.1 Executive Summary

WSP Canada Inc. (WSP) was retained by Talon Metals Corp (Talon) to prepare an independent Technical Report on the Eagle Mine (Eagle) property, located in the Upper Peninsula of Michigan, USA. The Eagle Mine, including the Eagle, Eagle East, and Keel deposits (collectively, the Eagle Mine), is 100% owned and operated by Eagle Mine LLC, an indirect wholly owned subsidiary of Talon. The purpose of this report is to support the public disclosure of the Mineral Resources and Mineral Reserves estimates of the Eagle Mine. This Technical Report was prepared in accordance with National Instrument (NI) 43-101 *Standards of Disclosure for Mineral Projects* (NI 43-101).

The Mineral Resources estimates for the Eagle Mine, which includes the Eagle, Eagle East, and Keel deposits, effective February 28, 2026, are summarized in Table 1.1. The Eagle Mine Mineral Reserves estimates as of February 28, 2026, are summarized in Table 1.2.

The Qualified Persons (QPs) consider that the Mineral Resources and Mineral Reserves estimates are classified and reported in accordance with Canadian Institute of Mining, Metallurgy and Petroleum (CIM) Definition Standards for Mineral Resources and Mineral Reserves, dated May 10, 2014 (CIM definitions), and CIM Estimation of Mineral Resources & Mineral Reserves Best Practice Guidelines, dated November 29, 2019, and NI 43-101 guidelines.

The QPs are not aware of any environmental, permitting, legal, title, taxation, socio-economic, marketing, political, or other relevant factors that could materially affect the Mineral Resources and Mineral Reserves estimates.

The Mineral Reserves will support the Mine Plan for the period 2026-2030, following which the mine is scheduled to close unless more economic mineralization is discovered, delineated, and evaluated to be feasibly mined.

Recommendations provided herein may, for the most part, be addressed by operating staff and budgets, given the operational status of the Eagle Mine. The recommendations are expected to be implemented by operations management and, as such, have not been costed out individually.

Unless otherwise specified, all dollar references and amounts in this technical report are U.S. dollars.

1.2 Property Description, Location, History, and Ownership

1.2.1 Property Description and Location

The Eagle Mine property, measuring approximately 0.63 square kilometers (km^2) in area, is located in the Upper Peninsula of Michigan, USA, at geographic co-ordinates 46° 45' north latitude by 87° 54' west longitude (UTM Zone 16N coordinates 5177557 m N, 432639 m E), in Michigamme Township, Marquette County. The Humboldt Mill (Humboldt) property, measuring approximately 1.42 km^2, is located 61 kilometers (km) west of Marquette and approximately 105 km by road from the mine site. The center point of the Humboldt Mill area (including all ownership of land) is 46º 29’ north latitude, 87º 54’ west longitude (UTM Zone 16N Zone coordinates 5148824 m N, 430843 m E). Eagle has a geological field office in Negaunee, 15 km west of Marquette, and an information center in Marquette.

1.2.2 Ownership

The Eagle Mine, including the Eagle, Eagle East, and Keel deposits, is 100% owned and operated by Eagle Mine LLC, an indirect wholly owned subsidiary of Talon. Eagle Mine LLC holds surface and mineral rights over a wide district encompassing portions of Sections 4-9 and 16-18, Township 50N, Range 28W, and Sections 1-5 and 8-17, Township 50N, Range 29W. The overall footprint of land controlled by Eagle Mine LLC comprises leases, agreements, or ownership totaling approximately 5,049 ha of mineral rights and approximately 2,698 ha of surface rights.

While the surface of the Eagle Mine is on Eagle Mine LLC property or property leased from the State of Michigan, the minerals comprising the Eagle Mine are either owned or leased from private owners or the State of Michigan. The state leases were renewed in 2022 for a period of 10 years. The private leases have various expiry dates that are extendable by continued payments or production. The Eagle deposit is situated on state and private mineral leases, with the Mineral Resource estimates split approximately equally between them. Royalty payment is made on a percentage of the Net Smelter Return (NSR), in place of an annual lease payment, while in production.

Lease payments would remain for the duration of mining at the Eagle Mine, although royalty payments related to Eagle would cease when production from the Eagle Mine ends. The royalties for the Eagle Mine follow mining industry norms.

Aside from lease and royalty payments, the QPs are not aware of any other significant factors or risks that may affect access, title, or the right or ability to perform work at the Eagle Mine.

1.2.3 History

Kennecott Exploration Company (KEX) started working in the region in 1991. Nickel exploration in the vicinity of Eagle was started in 1995, and in 2002, the Eagle deposit was first drilled by Rio Tinto with economic-grade mineralization being intersected. By the end of 2003, two separate high-grade sulfide zones were identified at Eagle. The lower zone was defined by 15 drill intercepts, and the upper zone was defined by six drill intercepts. This formed the basis of an order-of-magnitude study that was completed in early 2004. Following the order-of-magnitude study, an extensive resource and geotechnical drill program was completed in 2004, supplying the data to connect the former upper and lower zones and better establish the geometries of the massive sulfide, semi-massive sulfide, and host intrusive bodies. The result of this work was a pre-feasibility study.

Construction of the Eagle Mine commenced in 2010, and underground development began in September 2011. The Humboldt Mill was purchased by Rio Tinto in 2008. After several years of environmental reclamation and clean-up, refurbishment of Humboldt commenced in 2012 to prepare the facility to process its first ore in 2014.

Lundin Mining Corporation (LMC) acquired the Eagle Mine in 2013, and commercial production of nickel and copper concentrates was achieved in November 2014.

During 2015, exploration drilling discovered high-grade massive and semi-massive nickel-copper sulfide mineralization approximately 600 meters (m) beneath and 2 km east of the Eagle deposit. Referred to as Eagle East, this is a separate intrusion from the Eagle deposit. Eagle East Mineral Reserves were first disclosed in the

Technical Report prepared by Roscoe Postle Associates (RPA) at the effective date of December 31, 2016. The Eagle East deposit has been included in the Mine Plan since 2017.

The Mineral Resources and Mineral Reserves estimates for Eagle Mine were updated in 2022 and disclosed in the Technical Report prepared by WSP, effective December 31, 2022. This included the first Mineral Resource estimate disclosure for the Keel.

From the first commercial production in November 2014 to the end of 2025, Eagle Mine has produced approximately 195.0 thousand tonnes (kt) of nickel and 187.0 kt of copper. The nickel and copper concentrates are sold under long-term contracts directly to smelters or to traders in North America, Europe, and Asia.

Talon completed its transaction with Lundin Mining Corporation (LMC) on January 09, 2026, pursuant to which it acquired the producing Eagle Mine and associated Humboldt Mill.

1.3 Geology, Mineralization, and Exploration

The Eagle intrusion, Eagle East intrusion, and the Keel of Eagle East are all part of the same ultramafic intrusive system and all host high-grade primary magmatic Ni-Cu sulfide mineralization. These intrusions are related to the feeder system for the Keweenawan flood basalts, a Large Igneous Province (LIP) resulting from mantle-tapping extension during the Midcontinent Rift.

Mineralization styles are similar in Eagle and Eagle East, consisting of mineralized peridotite bodies with concentrations of semi-massive sulfide in the center of the intrusions and massive sulfides at the base. Massive sulfides can extend for short distances outwards beyond the contact of the peridotite, into the surrounding sedimentary country rocks as sills along bedding planes.

Exploration activities at Eagle have included geological mapping, geochemistry (indicator mineral sampling and Mobile Metal Ion (MMI) studies from basal tills, dike geochemistry, sulphur isotype studies, QEMSCAN studies), and geophysics (airborne, surface, and underground borehole electromagnetics, resistivity, and gravity). The main and most successful exploration tool has been diamond drilling in combination with a very robust and predictive conduit deposit model. The conduit has been traced eastward of Eagle East for approximately 1 km, at which point a gabbro intrusion occupies the intrusive plumbing system. This gabbro intrusion is approximately 350 m in width in the east-west direction and 225 m in the north-south direction and extends vertically to at least the drilled depth of 2,070 m below surface (1,550 m below the mineralized conduit). The hole defining this depth bottomed in gabbro, and the intrusion continues near vertically to an unknown depth. This gabbro intrusion frequently has a “rind” of pyroxenite, peridotite, or mineralized peridotite. This is interpreted as evidence that the gabbro has intruded and blocked the structural plumbing that was exploited by the mineralized peridotite intrusion.

The discovery and delineation of the Keel , at a shallower depth than Eagle East, has added to the mineral resource inventory of Eagle. There is currently no active exploration on the property.

The QP has conducted a review of the data collection processes, procedures, and data management records, with the following observations and conclusions:

- The drilling at Eagle, Eagle East, and the Keel has been conducted in a competent manner using appropriate equipment and techniques.
- Core handling, logging, and sampling have been carried out to a standard consistent with industry practice.
- Drill core and samples are stored and transported in a secure fashion.

- Assaying has been performed by accredited commercial laboratories using conventional methods commonly used in the industry.
- An adequate level of assay quality assurance/quality control (QA/QC) sampling has been carried out, and the results of this sampling have been used appropriately to ensure that the accuracy and precision of the analyses are within acceptable limits.
- The database is properly managed and validated in a secure manner.

1.4 Mineral Resources

The Mineral Resources estimate for the Eagle Mine is reported in accordance with NI 43-101 and has been estimated in conformity with generally accepted CIM Estimation of Mineral Resources and Mineral Reserves Best Practices guidelines.

The Mineral Resources estimate is reported at NSR cut-off values of $150.61/t for all deposits (Table 1.1). The Mineral Resources estimates are inclusive of Mineral Reserves but exclude mineralization within previously mined (depleted) areas.

Mineral Resources are not Mineral Reserves, and do not demonstrate economic viability. There is no certainty that all, or any part, of these Mineral Resources will be converted into Mineral Reserves. Inferred Mineral Resources are considered too speculative geologically to have economic considerations applied to them that would enable them to be categorized as Mineral Reserves.

Table 1.1: Eagle Mine Mineral Resources Estimate (Effective February 28, 2026)

Domain	Category	Tonnes (kt)	Ni (%)	Cu (%)	Co (%)	Au (g/t)	Ag (g/t)	Pt (g/t)	Pd (g/t)
Eagle	Measured (M)	39	1.21	1.40	0.03	0.20	7.35	0.38	0.24
Eagle East		-	-	-	-	-	-	-	-
Keel		-	-	-	-	-	-	-	-
Total Measured		**39**	**1.21**	**1.40**	**0.03**	**0.20**	**7.35**	**0.38**	**0.24**
Eagle	Indicated (I)	43	1.17	1.26	0.03	0.18	6.45	0.34	0.21
Eagle East		1,164	1.54	1.29	0.04	0.16	5.40	0.39	0.27
Keel		2,053	1.14	0.78	0.03	0.08	3.12	0.20	0.14
Total Indicated		**3,260**	**1.28**	**0.97**	**0.03**	**0.11**	**3.98**	**0.27**	**0.18**
Eagle	M&I	82	1.19	1.33	0.03	0.19	6.88	0.36	0.22
Eagle East		1,164	1.54	1.29	0.04	0.16	5.40	0.39	0.27
Keel		2,053	1.14	0.78	0.03	0.08	3.12	0.20	0.14
Total M&I	**M&I**	**3,299**	**1.28**	**0.97**	**0.03**	**0.11**	**4.02**	**0.27**	**0.19**
Eagle	Inferred	19	0.99	0.82	0.03	0.09	3.50	0.21	0.14
Eagle East		-	-	-	-	-	-	-	-
Keel		113	0.92	0.69	0.02	0.06	2.54	0.11	0.13
Total Inferred		**132**	**0.93**	**0.71**	**0.03**	**0.07**	**2.68**	**0.13**	**0.13**

Notes:

1. The updated MRE has been reported in-situ and has been prepared in accordance with the CIM Standards (2014) and follows Best Practices outlined by the CIM (2019).
2. Mineral resources that are not mineral reserves do not have demonstrated economic viability.
3. The QP (for purposes of National Instrument 43-101 – Standards of Disclosure for Mineral Projects ("NI 43-101")) for the updated MRE is Brian Thomas, P.Geo., an employee of WSP, and is "independent" of the Company within the meaning of Item 1.5 of NI 43-101.
4. The effective date of the MRE is February 28, 2026.
5. Mineral Resources are reported inclusive of Mineral Reserves at an NSR cut-off value of $150.61/t.
6. Metal Prices used: $9.37/lb Ni, $5.69/lb Cu, $20.00/lb Co, $3,825/oz Au, $44.50/oz Ag, $1,500/oz Pt, $1,205/oz Pd.
7. Rounding may result in apparent summation differences between tonnes, grade, and metal content.

1.4.1 Risks to Mineral Resources Estimates and Opportunities

Eagle Mine has been a producing mine since 2014 and has either mitigated or placed controls on many of the identified geological risks during that period. The following risks and opportunities associated with this Mineral Resources estimate are considered by the QP to be not material.

- Mineral domain models are interpreted from drill hole data and are subject to change with new information or re-interpretation at different cut-off values. Changes in modeling cut-offs could increase or decrease mineralized volumes.
- No mining has occurred in the Keel , and the nature of mineralization and grade continuity have yet to be confirmed.
- Some drill core intervals within the low-grade area of the Keel were not sampled and were assigned values of half detection limits during grade estimation.
- Different grade estimation methodologies can be used to support an MRE and variations in the approach, including estimation parameters and outlier controls used, can have a material impact on the resource estimate.
- Changes in metal prices and mining costs can vary significantly over short periods of time, which has the potential to materially impact the MRE.
- Further infill drilling could provide an opportunity to increase resource confidence and may support the conversion of remaining Inferred resources to the Indicated category.

1.5 Mineral Reserves

The mine design and scheduling for reserves estimates were prepared by the technical services department at Eagle Mine and verified by the QP responsible for these estimates.

The Mineral Reserves were estimated using the CIM 2019 Best Practices Guidelines and are classified using the 2014 CIM Definition Standards.

The Mineral Reserves estimation method consists of converting Measured and Indicated Mineral Resources to Proven and Probable Reserves by identifying material that exceeds the NSR cut-off values while conforming to the geometrical constraints determined by the mining method and applying modifying factors such as dilution and mining recovery.

Mineral Reserves are reported as diluted tonnes delivered to the process plant and have an effective date of February 28, 2026.

Table 1.2 shows the Eagle Mineral Reserves estimate, which is inclusive of dilution and mining loss, and is supported by a mine design, a detailed mine production schedule, and capital and operating cost estimates.

Table 1.2: Eagle Mine Mineral Reserves Estimate (Effective February 28, 2026)

			Grade							Contained Metal						
Domain	Category	(kt)	Ni	Cu	Au	Ag	Co	Pt	Pd	Ni	Cu	Au	Ag	Co	Pt	Pd
			(%)	(%)	(g/t)	(g/t)	(%)	(g/t)	(g/t)	(kt)	(kt)	(koz)	(koz)	(kt)	(koz)	(koz)
Eagle	Proven	27	1.16	1.36	0.18	6.94	0.03	0.35	0.22	0.31	0.36	0.15	5.92	0.01	0.30	0.19
	Probable	14	1.04	1.08	0.15	5.74	0.03	0.28	0.18	0.14	0.15	0.07	2.58	0.00	0.13	0.08
	Sub Total	41	1.12	1.27	0.17	6.52	0.03	0.32	0.20	0.45	0.51	0.22	8.50	0.01	0.42	0.27
Eagle East	Proven	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	Probable	1 155	1.31	1.09	0.13	4.62	0.03	0.33	0.23	15.15	12.61	4.99	171.7	0.40	12.2	8.36
	Sub Total	1 155	1.31	1.09	0.13	4.62	0.03	0.33	0.23	15.15	12.61	4.99	171.7	0.40	12.2	8.36
Keel	Proven	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	Probable	2 290	0.94	0.68	0.07	2.71	0.03	0.17	0.12	21.50	15.48	5.52	199.4	0.59	12.8	8.81
	Sub Total	2 290	0.94	0.68	0.07	2.71	0.03	0.17	0.12	21.50	15.48	5.52	199.4	0.59	12.8	8.81
Total	Proven	27	1.16	1.36	0.18	6.94	0.03	0.35	0.22	0.31	0.36	0.15	5.9	0.01	0.30	0.19
	Probable	3 459	1.06	0.82	0.09	3.36	0.03	0.23	0.16	36.79	28.25	10.57	373.6	0.99	25.2	17.3
	Total P&P	**3 486**	**1.06**	**0.82**	**0.09**	**3.39**	**0.03**	**0.23**	**0.16**	**37.10**	**28.61**	**10.73**	**379.6**	**1.00**	**25.5**	**17.4**

Notes:

1. The Mineral Reserves disclosed are classified as Proven and Probable and are based on the 2014 CIM Definition Standards and 2019 CIM Estimation of Mineral Resources and Mineral Reserves Best Practice Guidelines.
2. Mineral Reserves are estimated at a stope full cost NSR cut-off of $150.61/t, a stope marginal cost NSR cut-off of $107.29/t, and a development NSR cut-off of $52.30/t
3. Mineral Reserves are estimated using average long-term prices of $8.15/lb Ni, $4.95/lb Cu, $20/lb Co, $3825/oz Au, $44.50/oz Ag, $1500/oz Pt, $1205/oz Pd.
4. Bulk density interpolated in block model ranges from 2.98 t/m3 to 4.44 t/m3 and averages 4.11 t/m^3.
5. The reference point at which the Mineral Reserves are defined is where the ore is delivered to the process plant and therefore not inclusive of milling recoveries or payable metal deductions.
6. Contained Metal for Au, Ag, Pt and Pd is reported in Troy Ounces and calculated as follows:
   Contained Metal, (koz) = Tonnage (kt) * Grade (g/t) *0.032151
7. Numbers may not add due to rounding.
8. The QP is not aware of any environmental, permitting, legal, title, taxation, socio-economic, marketing, or political factors that might affect the estimate of Mineral Reserves, other than those specified in Section 15.10.

1.6 Mining

1.6.1 General

The Eagle Mine is an underground mine producing about 2,000 tonnes per day (tpd) of nickel-copper ore. The ore is hauled to the surface in diesel-powered trucks via the ramp and then trucked to the Humboldt Mill at a separate site. Underground workings are accessed via the main ramp, which has its portal entrance within the mine site industrial area. The mine has three active mineralized zones called Eagle, Eagle East, and the Keel. The Eagle Mine has Mineral Reserves to support production until 2030, when the mine is scheduled to close.

1.6.2 Geomechanics

The general rock quality in Eagle East and Eagle Main is classified as "Good to Excellent," according to the RQD system, "Good to Very Good," according to the RMR_{76} system, and "Fair to Good," according to the Q-system. The Eagle Main has post-mineralization faults within the intrusive near the footwall peridotite-siltstone contact. Eagle East has a post-mineralization fault, which has been intruded by a gabbro dike. An overcoring study using the Sigra biaxial deformation method indicated a higher horizontal in-situ stress occurring close to and within the Eagle ore zone.

Lithologic units within the Keel are similar to those in Eagle, except that the predominant waste rock is Feldspathic Peridotite. There has been no dedicated geotechnical drilling in the Keel, and some geotechnical data has instead been collected from resource drilling, suggesting “Good” ground characteristics (according to the Q-system) for most of the rock mass near and within the Keel. A review of the available drill hole data, core photographs of resource drilling within the Keel, past geotechnical characterization, and numerical modelling has been performed and is summarized in Section 16.3.

1.6.3 Hydrogeology

Eagle Mine is a relatively dry mine, and daily dewatering volumes are typically less than 10 gpm. The groundwater-inflow volume is calculated as the difference between the daily volume of water provided underground and the daily volume pumped to the surface. This volume is regularly monitored, as a sudden increase could indicate inflow from the crown pillar.

1.6.4 Ground Support

The primary ground support selection is based on the rock mass quality "Q" index, ranging from Type 1 support for Q ≥ 4 to Type 3 support for Q < 1. The ground support generally consists of 2.4 m (8 ft) inflatable or fully encapsulated resin rebar bolts installed on a 1.5 m by 1.8 m (5 ft by 6 ft) spacing with galvanized welded wire mesh and an overlapping "5-spot" pattern. Type 3 ground requires applying 5 cm (2 in) of shotcrete. Secondary support for intersections and other mine openings with a wide span consists of a pattern of 3.7 m (12 ft) inflatable bolts, 3.7 m (12 ft) fully encapsulated resin rebar, or 6 m (20 ft) cable bolts, depending on the purpose and longevity of the opening.

1.6.5 Mine Design

The Mineral Reserves estimate is based on a mine design and schedule that was prepared in Deswik software. The development parameters used for mine design and planning include the cross-sections of drifts and ramps and the advance rates for the diverse headings. The production parameters include mining methods, stope dimensions, and production rates.

The Eagle Mine uses the Modified Stability Graph Method to predict stability and determine stope dimensions.

1.6.6 Backfill

Eagle Mine employs cemented (CRF) and uncemented rockfill (URF) to backfill stope voids. CRF is used to backfill the production areas in drift-and-fill mining (D&F) and the primary stopes in transverse sublevel open stoping (TSLOS). URF is used to backfill secondary stopes in TSLOS. The backfill is hauled to stopes by the same mine trucks that transport ore to the surface. All of the aggregate used in the backfill is planned to come from off-site sources. The remaining waste rock left at Eagle Mine will be used in secondary stopes throughout the mine.

Talon is currently investigating the utilization of paste backfill as the backfill method for the upper and middle sections of the Keel to reduce operating costs and improve project economics. To generate the paste backfill product, Eagle Mine will convert its operating cemented rockfill plant to produce a paste backfill. The process will involve feeding purchased sand into a continuous mixer where it is blended with cement and water to produce the paste backfill. The paste system is planned to become operational in Q2 2028.

1.6.7 Mine Access

The underground workings are accessed via the main ramp, which measures nominally 5.5 m wide by 5.5 m high and has typical grades of -13% to -14%. The mine's escapeway routes consist of the main ramp, a borehole raise extending to surface equipped with an Alimak elevator, the twin ramps connecting Eagle East to the Eagle, and borehole raises extending between sublevels equipped with Laddertube™ manways. In addition, the Keel will have two escape routes connecting with the mine’s main ramp.

1.6.8 Underground Infrastructure

A compressor plant situated on the surface at the mine site supplies the mine's compressed air. The underground mine's data and communications systems consist of a leaky feeder system for two-way radio communication,fiber-optic network, and a private LTE cellular network. Mining equipment is mainly serviced and repaired at the maintenance shop on the surface; however, there is an underground maintenance shop in the East Eagle. The dewatering system consists of pumping stations connected in series along the main decline such that the water is pumped upward from station to station and finally to the Surface Control Water Basin. Underground electrical power is supplied by two separate 13.8-kV distribution systems, one from the portal and the second down the fresh-air raise (FAR). The mine's two explosive magazines are in the underground mine.

1.6.9 Ventilation

Fresh air enters the mine via the portal of the main ramp and a FAR. The return air is exhausted via a return-air raise (RAR), with twin 522 kW fans installed at the collar. The portal is equipped with a 186-kW fan. The ventilation system has been extended via twin ramps from the Eagle to the Eagle East For the Keel, fresh air will be drawn to its upper level via a ventilation drift extending from the main ramp and a system of raises, and the return air will be exhausted via the spiral ramp and discharged to the main ramp.

1.6.10 Mining Methods

Eagle Mine uses three mining methods: transverse sublevel open stoping (TSLOS), longitudinal sublevel open stoping (LSLOS), and drift-and-fill mining (D&F). For TSLOS, the portion of the deposit between two sublevels is mined by dividing the ore into alternating primary and secondary stopes

pes, which extend in parallel from the footwall to the hangingwall. Longitudinal stopes are typically 6 m wide and are mined along strike in panels up to 45 m in length. D&F is similar to the overhand cut-and-fill method except that the lifts are mined one drift at a time rather than by excavating the ore from the footwall to the hangingwall.

1.6.11 Mining Equipment

The Eagle Mine is a mechanized mine with rubber-tired diesel equipment utilized for all phases of mining operations. The LHDs are equipped for radio remote control operation, which is required for mucking in TSLOS and LSLOS stopes. The mine trucks are equipped with both ejector and standard boxes. The ejector boxed trucks are able to dump CRF and URF directly into stopes, while the standard boxed trucks focus on ore and waste haulage to surface. The drilling fleet includes electric/hydraulic face drill jumbos, longhole blasthole drills, a cable bolter, and rock bolting rigs for ground support.

1.6.12 Mine Development

The LOM development plan calls for 9,026 m of lateral capital development, of which 14% is required for Eagle East, and 86% for the Keel. Eagle East still requires development for its uppermost sublevels. The Keel is a new mining zone that accounts for most of the planned capital development meters.

Operating lateral development totaled 6,515 meters: 51% in Eagle East, 48% in the Keel, and less than 1% in Eagle.

The entire 2,296 meters of vertical development will be carried out exclusively within the Keel, as part of its ventilation and escapeway system implementation.

1.6.13 LOM Production

Eagle is expected to produce 724,000 tonnes in 2026 and then ramp up to approximately 787,000 tonnes throughput per annum (tpa) of ore from 2027 to 2029, then reduce to approximately 497,000 tonnes in 2030, which is the last year of scheduled production.

Eagle East production output is expected to decline in 2027, and the Keel will provide the additional tonnes needed to reach the yearly production target.

Eagle stopes, given their proximity to the Alimak raise, are scheduled at the end of the mine life.

1.6.14 Mine Personnel

Staff personnel, including management and technical services, are Talon employees who generally work a four-day work week, ten hours daily. In Q1 2024, Eagle internalized mine operations and mobile maintenance roles,previously performed by mine contractors. Personnel in these groups typically work 12-hour shifts, seven days a week, on a one-week-on, one-week-off rotation schedule.

1.7 Mineral Processing

The Humboldt Mill processing facility operates at or near the metallurgical budget. The remaining reserves at Eagle and Eagle East are similar mineralogy to the material already processed, with the exception of the Keel, which is lower-grade material. The processing facility will have no issues treating future material as it maintains a consistent grade/performance relationship with other Eagle ore. Keel ore fell in the hard range of hardness and is more competent than Eagle East ore as per the SGS grindability test work. This may result in increased energy demand and/or lower throughput in the ball mill as compared to treating historical ores.

1.8 Infrastructure

The Eagle Mine is considered a mature operation, which has endeavored to add Mineral Reserves to the mine plan as a means of extending the mine life. The added Mineral Reserves have placed minimal burden on existing infrastructure, with investment limited to Sustaining Capital.

- The area is served by an extensive network of paved roads, rail service, excellent telecommunications facilities, national grid electricity, and an ample supply of water. All infrastructure to operate the mine is in place, and no significant investments are required for the balance of the mine life, aside from the water treatment plant, described below.
- There is no additional infrastructure required for the Keel. The Eagle Mine infrastructure will be used for the Keel , as it has been for Eagle East.
- The Humboldt Mill will be used to process Keel material, commingled with ore from Eagle and Eagle East, and it is anticipated that the existing unit operations of the process plant would remain largely unchanged.
- Tailings produced at the Humboldt Mill are deposited sub-aqueously into the Humboldt Tailings Disposal Facility (HTDF), which is a pit lake that formed in the open pit of a former iron ore mine. Tailings deposition locations are prescribed in the tailings deposition plan, which is updated periodically as needed (typically about once per year).
- HTDF inputs and outputs (i.e., water and tailings) must be carefully managed and monitored to help preserve the quality of the near-surface water and limit the potential for impacts to groundwater around the HTDF.
- The surveillance program for the HTDF involves inspecting and monitoring the operation, structural integrity, safety, and environmental performance of the facility. It includes routine visual observation, monitoring of tailings slurry and reclaim water flows, monitoring of the HTDF water level, monitoring of water chemistry in the HTDF, monitoring of groundwater quality around the HTDF, and semi-annual bathymetric surveys.

A well-established tailings deposition methodology exists at the HTDF, which is used for permanent disposal of tailings generated from the processing of ore from the Eagle Mine at the Humboldt Mill. An effective surveillance program is in place to inspect and monitor the facility's operation, structural integrity, safety, and environmental performance. The tailings deposition plan shows that sufficient capacity exists in the HTDF to dispose of tailings produced at the Humboldt Mill through the LOM with no tailings deposited above an elevation of 461.8 m (1,515 feet) above mean sea level (amsl), which is the maximum permitted tailings elevation. About 2.0 million cubic meters (2.6 million cubic yards) of capacity is available up to an elevation of 461.8 m (1,515 feet) amsl as of December 31, 2025, to accommodate an estimated in-place tailings volume of 1.7 million cubic meters (2.2 million cubic yards) from that date through the remaining LOM.

1.9 Environmental Studies, Permitting, and Social or Community Impacts

Eagle Mine has completed environmental studies and permitting and has managed potential social impacts at both the Eagle Mine site (Mine) and the Humboldt Mill site (Mill). A review of 12 environmental studies completed between 2023 and 2026 finds no environmental issues that could materially impact the issuer's ability to extract the Mineral Resources or Mineral Reserves.

During operations, waste rock generated at the Mine site is stored in the Temporary Development Rock Storage Area (TDRSA) prior to being placed underground as backfill. During operations at the Mill site, sulfidic tailings are sub-aqueously disposed in the HTDF below a 5-meter-thick (17-foot-thick) water cover.

Groundwater levels and quality are monitored using a series of wells at both the Mine and the Mill site. Additional surface water quality measurements and profiles of physicochemical parameters, along with water surface elevations, are regularly monitored within the HTDF.

During operations, water at the Mine site is treated at the Mine water treatment plant (WTP) before being discharged to the Quaternary aquifer via the Treated Water Irrigation System (TWIS). At closure, the Mine WTP will be discontinued once water quality in monitoring wells is demonstrated to meet groundwater discharge criteria.

During operations, water at the Mill site is treated at the Mill WTP before being discharged to the Middle Branch of the Escanaba River. At closure, the Mill WTP will be discontinued once water in the HTDF meets discharge criteria to the adjacent wetland.

Eagle holds permits that specify the water quality discharged to the TWIS at the Mine site and to the Middle Branch of the Escanaba River at the Mill site. Additional permits relate to mining, air quality, and sewage disposal. Eagle is awaiting feedback from the State of Michigan, Department of Environment, Great Lakes and Energy (EGLE) on revised/renewed permits for water discharge at both sites. Eagle has continuously held reclamation bonds since the start of operations, with the most recent bond amounts being approved by EGLE in early 2026.

Eagle has no social or community-related requirements during operations or closure. On account of their performance record, community opinion of mining has shifted from opposition to Eagle to conditional acceptance of Eagle operations. Eagle contributes to multiple programs in the local community related to small business development, education, and environmental monitoring.

Required closure at the Mine site involves flooding the underground mine, monitoring groundwater quality for 20 years, removing all buildings, and returning the surface to a productive forest. Total financial assurance is set at a minimum of $39,158,626 applied to Eagle Mine.

Required closure at the Mill site involves treating HTDF water until the water quality is acceptable for passive discharge to the adjacent wetland. Thereafter, the water treatment plant and associated infrastructure will be removed. The Mill and associated infrastructure will be retained for resale and future reuse. The total financial assurance for the Mill is set to a minimum of $16,076,480.

1.10 Capital and Operating Costs

All capital and operating costs are expressed in United States Dollars ($).

Currently, there are no expansion plans requiring project capital expenditures in the LOM plan.

The Eagle Mine is in operation and comprises three mining areas: Eagle, Eagle East, and the Keel (in development). Sustaining capital and operating costs are based on the mine plans prepared as part of the LOM workup and current operating experience.

Underground development cost is directly correlated with development meters, with unit rates for lateral and vertical development applied to the number of meters of mine development required in each year. Mine development is scheduled to be substantially complete by the end of the year 2028, with 184 meters remaining in the last two years of mine life. The current mine plan requires $69.9 million in sustaining capital for continuing underground mine development, mine other, mill, and other expenditures.

Table 1.3 summarizes the capital expenditures planned for the balance of the mine life. The QP has reviewed the planned annual expenditures and agrees with their reasonableness. The short remaining LOM does not necessitate significant new equipment purchases. Spending for the sustaining capital categories, Mine Other, Mill, and Other, will be completed by 2028 and show no expenditures in the final two years of the LOM.

Table 1.3: LOM Sustaining Capital Derivation

Item	Unit	2026*	2027	2028	2029	2030	Total
Mine Development Meters							
Vertical							
Drop Raise	m	81	154	210	-	-	445
Raisebore Ventilation	m	152	109	211	-	-	471
Raisebore with Escapeway	m	178	90	86	-	-	354
Paste Boreholes	**m**	-	416	610	-	-	1,026
Total Vertical	**m**	**412**	**769**	**1,116**	**-**	**-**	**2,297**
Lateral							
Eagle	m	0	0	0	0	20	20
Eagle East	m	484	487	219	78	14	1,281
Keel	m	2,071	2,754	2,828	40	32	7,724
Total Lateral	**m**	2,555	3,241	3,046	118	66	**9,026**
Waste Tonnes	t	230,568	297,718	272,399	15,810	12,596	829,091
Expenditures, $M							
Underground Development	$M	12.2	13.8	13.9	-	-	39.9
Mine Other	$M	2.9	3.5	3.5	-	-	10.0
Mill	$M	1.0	1.2	1.2	-	-	3.4
Other	$M	0.5	0.6	0.6	-	-	1.7
Paste Plant	$M	5.0	10.0	0	-	-	15.0
Total Sustaining Capital, $M	**$M**	**21.6**	**29.1**	**19.1**	**-**	**-**	**69.9**

Notes: Columns and rows may not sum precisely due to rounding. 2026 excludes January-February results.

The Keel is being established as an extension of the current mine and accordingly has no project capital. Its sustaining capital and operating costs are based on unit cost factors established with the mining of Eagle and Eagle East, which are then applied to the mining activities derived from the LOM plans for the Keel. No additional infrastructure will be required other than that normally installed with development headings – electrical stations, pump stations, secondary egress, etc. Ventilation for the Keel will be integrated into the existing mine ventilation system via additional raises, described in Section 16.6.

The QP considers the Eagle, Eagle East, and Keel capital and operating cost estimates to be appropriate.

Talon provided a cash flow model that shows the LOM operating cost for the Eagle Mine and Humboldt Mill, including General and Administrative (G&A) and ore transportation and is described in Section 22.0.

In addition to the Sustaining Capital, the mine plan includes $78.0 million in expenditures for closure activities to be initiated within the remaining five years of operation and continued in the two ensuing post-closure years with asset retirement obligation expenditures, followed by ongoing site monitoring until 2047.

Operating expenses at Eagle have been reviewed by the QP and found to be reasonable for a mechanized mine utilizing the drift-and-fill and bulk longhole mining methods. The plant has demonstrated typical operating costs for a facility of its size. The following tables summarize operating costs, segmented by major cost center - the Mine, the Processing Plant, and G&A.

Table 1.4 summarizes the total expected operating expense to mine and process the 3.58M tonnes of ore as defined by the LOM and the cashflow model.

Table 1.4: Projected Operating Costs

Cost Centre	LOM Cost, $M Total	Unit Cost, $/t Average
Mining	245.5	70.29
Ore Transport to Mill	48.7	13.96
Plant	134.3	38.50
G&A	74.0	21.20
Total Operating Costs	**502.1**	**144.00**

shows the operating costs by year as compared to the production plan by mining area.

Table 1.5: Projected Operating Costs by Year

Item	Unit	2026*	2027	2028	2029	2030	Totals
Ore Tonnes Mined							
Eagle	t	-	-	-	-	40,532	40,532
Eagle East	t	509,487	329,675	136,394	179,759	-	1,251,394
Keel	t	118,982	457,720	650,204	607,520	456,207	2,290,633
Total Ore Tonnes*	t	**628,469**	**787,396**	**786,598**	**787,279**	**496,739**	**3,582,560**
Cost Center							
Mining	$M	49.9	61.6	55.4	47.0	31.0	245.1
Ore Transport to Mill	$M	8.6	10.8	11.1	11.2	7.1	48.7
Plant	$M	26.4	29.5	29.2	29.6	19.6	134.3
G&A	$M	17.3	18.2	14.4	14.4	9.6	74.0
Total Operating Costs	$M	**102.2**	**120.2**	**110.1**	**102.2**	**67.3**	**502.1**
Total Cost per Total Tonne	$/t	163	153	140	130	135	144

Notes: Columns and rows may not sum precisely due to rounding. 2026 excludes January-February results.

Operating costs of the underground mine are estimated to be $245.5 million over the LOM, which averages to $70.29/tonne of processed material, itemized in Table 1.6.

Table 1.6: Mine Operating Cost Projection

Activity Related	LOM Cost, $M Total	Unit Cost, $/t Average
Mining Consumables	37.4	10.73
Mine Operations	58.7	16.85
Energy	24.7	7.07
Maintenance	102.1	29.29
Overhead and Services	22.2	6.36
Total Mine Opex	**245.1**	**70.29**

Operating costs of the processing plant are estimated to be $134.3 million over the LOM, or an average of $38.51/tonne, with major cost elements provided in Table 1.7.

Table 1.7: Processing Plant Operating Cost Projection

Cost Center	LOM Cost, $M Total	Unit Cost, $/t Average
Reagents / Grinding / Chemicals	14.5	4.16
Maintenance	25.5	7.31
Power	16.5	4.73
Contract Services	18.3	5.25
Salaries	57.9	16.60
Admin	1.6	0.46
Total Mill Opex	**134.3**	**38.51**

Current G&A costs, along with current Ore Transportation costs, have been carried forward for the LOM based on current costs. G&A is above the NSR baseline of $19.00 $/t for 2026 and 2027, with 2028 and 2029 in line with previous targets. The final year of the LOM is a partial year of five months duration, resulting in a cost of $9.6 million. G&A over the LOM totals $74.0 million, equating to an average over the LOM of $21.20/t processed.

Ore transportation from the mine to the mill averages $13.96 /t over the LOM, providing a total operating expense estimate of $48.7 million for the remaining LOM.

1.11 Economic Analysis

The economic analysis has been prepared on an annual basis, with the NPV calculated as of March 1, 2026. The cash flows and NPV exclude the residual value of the mill, salvage value of equipment and release of working capital at the end of operations.

The economic evaluation reflects a steady-state operating scenario based on the current mine plan from March 2026 to the second half of 2030, incorporating forecast production, operating costs, sustaining capital requirements, and analyst consensus metal price estimates as of December 2025.

All dollar amounts are in US dollars.

Table 1.8: Assumed Metal Prices Based on Analyst Consensus Estimates as of December 2025

		2026	2027	2028	2029	2030
Nickel	$/lb	7.50	7.70	8.15	8.15	8.15
Copper	$/lb	5.50	5.00	4.95	4.95	4.95
Cobalt	$/lb	19.00	20.00	20.00	20.00	20.00
Platinum	$/oz	1,500	1,500	1,500	1,500	1,500
Palladium	$/oz	1,245	1,205	1,205	1,205	1,205
Gold	$/oz	4,200	3,825	3,825	3,825	3,825
Silver	$/oz	50.25	44.50	44.50	44.50	44.50

The key financial and operating metrics of the Eagle mine's remaining mine life are summarized in Table 1.9.

Table 1.9: Key Financial and Operating Metrics of Eagle Mine's Remaining Mine Life

Financial Metrics		
After-tax net present value @ 8%	$ millions	$19.0 million
IRR	%	Not applicable[1]
Payback	Yr.	Not applicable[1]
Operating Metrics		
Mine life	Years	March 2026 to H2 2030 (approx. 4.4 years)
Total tonnes processed	Tonnes	3,486,481
Average annual throughput	Tonnes per annum	787,000
Daily throughput	Tonnes per day	2,156
Cash cost[2] (LOM net of credits)	$/lb of payable Ni	$5.13
All-in sustaining cost[3] (2026-2030 operational period net of credits)	$/lb of payable Ni	$6.55
All-in sustaining cost[4] (LOM net of credits)	$/lb of payable Ni	$8.05
Revenue breakdown over LOM	% of gross revenue	Nickel – 57% Copper – 37% Other[5] – 6%

1.11.1 Sensitivity Analysis – Nickel/Copper Price Pairings

An additional sensitivity analysis was carried out using constant nickel and copper price pairs over the forecast period. The range of nickel and copper price pairs were based on analyst consensus metal prices, current metal prices and market participant expectations. Metal prices for metals other than nickel and copper used analyst consensus prices for the 2026-2030 forecast period.

Sensitivity analyses were performed on:

a) After-tax NPV-8%; and
b) after-tax free cash flow during the 2026-2030 operational period of the mine.

The cash flows and NPV exclude the residual value of the mill, salvage value of equipment and release of working capital at the end of operations.

[1] IRR and payback calculations are not applicable and do not compute since this is an operating mine and does not have an initial capital investment.
[2] Cash cost includes mining, transportation, processing, G&A costs, royalties and treatment/refining costs offset by by-product credits from metals other than nickel
[3] All-in sustaining cost ("AISC") includes cash cost, sustaining CAPEX, royalty buy-down, exploration and closure costs incurred during operational period.
[4] All-in sustaining cost ("AISC") – LOM includes operating AISC as well as closure costs incurred after operational period.
[5] Other includes cobalt, platinum, palladium, gold and silver. Total may not add up to 100% due to rounding.

Table 1.10: Sensitivity Table In US$ Millions

After-tax NPV-8%		Nickel price (US$/lb)				
		$7.00	$8.00	$8.50	$9.00	$10.00
	$4.50	(43)	(2)	19	40	90
Copper	$5.00	(22)	19	40	61	111
price	$5.50	(2)	40	61	82	132
(US$/lb)	$6.00	19	61	82	103	153
	$6.50	40	82	103	124	174

A

After-tax free cash flow		Nickel price (US$/lb)				
Mar 2026-2030		$7.00	$8.00	$8.50	$9.00	$10.00
	$4.50	(4)	45	70	94	153
Copper	$5.00	21	70	94	118	177
price	$5.50	45	94	118	143	202
(US$/lb)	$6.00	70	118	143	167	226
	$6.50	94	143	167	192	250

B

Note: A) After-Tax NPV; and B) ,After-Tax Free Cash Flow During the Operational Period (2026-2030), At Various Nickel and Copper Price Pairs

1.12 Recommendations

1.12.1

loThe QP has the following recommendations for Talon, which are expected to be considered by operations management and, as such, have not been costed out individually.

- Sample and assay any available core that was not sampled within the Keel mineral domain volume and establish boundary limits for future drill programs to ensure that all potential mineralization, within areas of interest, is fully sampled.
- Future model updates are recommended to include sample data from the 7 holes acquired after the data cut-off date and to incorporate any new mapping and geological data from the Keel once mining begins.
- Additional infill drilling is recommended to improve geological understanding, increase confidence in grade continuity, and support upgrading remaining Inferred Material to Indicated Material (and potentially refine mineralized volumes).

1.12.2 Mineral Reserves

The QP has the following recommendations for Eagle Mine, which are expected to be considered for future Mineral Reserves estimates:

- The Mineral Reserves estimate reflects risk due to the significant proportion of Probable Reserves (99%) compared to Proven Mineral Reserves. It is recommended that Eagle Mine focus on underground infill drilling within key deposit areas to convert Probable Reserves to Proven Reserves.
- Consider revisiting the full-cost, marginal, and incremental NSR cut-off values for each zone, as both costs and mining methods vary across different zones.
- Evaluate the performance (dilution, recovery, stability) of the first Keel stopes and modify design parameters as necessary for subsequent stopes within the zone.

1.12.3 Geomechanics

For future study stages, the following is recommended:

- Reconcile existing geotechnical data within and near the Keel ore body, identify data gaps, and collect additional information to close existing parameter uncertainty (e.g., downhole televiewer data to reduce uncertainty regarding structural orientations).
- After data reconciliation (previous bullet), update and revise stability assessments (3D numerical model, backfill strength estimates, pillar stability estimates, footwall offset stability, etc.) based on the current LOM. Review the LOM layout (stope sizing, pillar dimensions, etc.) and sequence based upon the revised assessments.
- The location and orientation of some stope accesses should be reviewed to mitigate or remove challenges related to stability.
- Evaluate the typical overbreak and dilution experienced in Eagle East as a check on ELOS estimates assumed for the LOM stopes.

1.12.4 Mining

- If the results of the paste fill study are convincing, accelerate the implementation of the paste fill system to enable the mine to benefit from its advantages. Due to the nearly flat deposits in the upper Keel, it is essential to carefully plan the application of longhole methods, particularly with regard to sill positioning, sizing, and backfill placement.
- Conduct an economic evaluation of relevant areas and operational levels to ensure profitability is achieved.

1.12.5 Mineral Processing

- Because Keel ore is low grade and more competent, it is recommended that mill operations closely monitor its actual performance and throughput. This will allow comparison with historical production data and support trend forecasting.
- The high-pressure slurry ablation (HPSA) unit is presently in the commissioning phase. It is recommended to initiate HPSA operations to realize anticipated recovery improvements and to systematically monitor its actual performance benefits.

1.12.6 Economic Analysis

- Average grades are very close to the cut-off. Maintaining productivity is essential to achieving the cost forecast provided. As production ramps down and capital development is completed, assessing marginal and incremental ore opportunities may help improve economics. Additional refinement of fixed costs at the end of operation may also improve economics.

2. Introduction

2.1 Sources of Information and Data

This Technical Report is based on information made available to WSP by Talon and Eagle Mine LLC in an electronic data room, as well as on information collected during the site visits. Other information was obtained from the public domain.

The purpose of this report is to support the public disclosure of the Mineral Resource and Mineral Reserve estimates of the Eagle Mine. This Technical Report was prepared in accordance with National Instrument 43-101 Standards of Disclosure for Mineral Projects (NI 43-101).

This Technical Report is based on the following sources of information:

- Information provided by Talon and Eagle Mine LLC.
- Site visits conducted by the Qualified Persons listed in Table 2.1 during February 2026.
- Discussions with Talon and Eagle Mine personnel.
- Additional information from public domain sources.

The Qualified Persons have reviewed such technical information and have no reasons to doubt the reliability of the information provided by Talon Metals and Eagle Mine LLC and have determined it to be adequate for the purposes of this Technical Report. The Qualified Persons do not disclaim any responsibility for this information. The documentation reviewed and other sources of information are listed at the end of this Technical Report in Item 27, References.

2.2 Units of Measure

The units of measure used in this report are per the International System of Units (SI) or metric, except for Imperial units commonly used in industry (i.e., ounces (OZ) for precious metals mass and US gallons per minute (GPM) for water flow rates).

All dollar figures quoted in this report refer to United States Dollars, unless otherwise noted.

Frequently used abbreviations and acronyms are listed in Section 2.6.

This report includes information that required subsequent calculations to derive sub-totals, totals, and weighted averages. Such a calculation inherently involves a degree of rounding and consequently introduces a margin of error. Where these occur, the report QPs do not consider them to be material.

2.3 Qualifications of Consultants

The QPs who prepared this Report are specialists in the fields of geology, exploration, Mineral Resources and Mineral Reserves estimation and classification, mining, geotechnical, environmental, permitting, metallurgical testing, mineral processing, processing design, civil, mechanical, electrical, capital and operating, and cost estimation. The individuals listed in Table 2.1 are, by virtue of their education, experience, and professional association, considered QPs, as defined by NI 43-101.

Table 2.1: Qualified Person Responsibility

Qualified Person	Designation	QP Responsibility/Role	Report Sections/Subsections
Bill Bagnell	P.Eng (SK)	Engineering Manager/Technical Director Mine Engineering and Stability	1: Summary, 2: Introduction, 3: Reliance on Other Experts,16.5 Mine Infrastructure 18: Project Infrastructure,19: Market Studies and Contracts, 24: Other Relevant Data and Information, 25: Interpretation and Conclusions, 26: Recommendations, 27: References
Brian Thomas	P. Geo., (ON, NFLD)	Geology and Mineral Resource Estimate	1: Summary, 4: Property Description and Location, 5: Accessibility, Climate, Local Resources, Infrastructure and Physiography, 6: History, 7: Geological Setting and Mineralization, 8: Deposit Types, 9: Exploration, 10: Drilling, 11: Sample Preparation, Analyses and Security, 12: Data Verification, 14: Mineral Resource Estimates, 23: Adjacent Properties, Information, 25: Interpretation and Conclusions, 26: Recommendations, 27: References
Ibrahim Karajeh	P.Eng.(ON), MBA, PMP, CCP	Infrastructure	1. Summary, 18.2: Site Roads, 18.3: Power Supply, 18.4: Water, 18.5: Ancillary Facilities, 18.6: Concentrate Shipping
D Jin	P. Eng. (ON)	Metallurgy and Recovery Method	1: Summary, 12: Data Verification (12.3 only), 13: Mineral Processing and Metallurgical Testing, 17: Recovery Methods, 25: Interpretation and Conclusions (25.4 only), 26: Recommendations (26.3 only), 27: References
K Mounhir	P. Eng. (QC)	Mining and Mineral Reserves Estimate	1: Summary, 15: Mineral Reserves Estimates, 16: Mining Methods (16.1, 16.2, 16.4, 16.6, and 16.7), 25: Interpretation and Conclusions, 26: Recommendations, 27: References
James Smith	P.Eng. (ON)	Geomechanics	1: Summary, 16.3 Geomechanics, 25: Interpretation and Conclusions, 26: Recommendations, 27: References
Jason Obermeyer	P.E. (MI)	Tailings	1: Summary, 12: Data Verification (12.4.1 and 12.5.5), 18.1: Tailings Disposal, 25: Interpretation and Conclusions, 27: References
Devin Castendyk	P.G. (WY)	Environmental Studies, Permitting, and Social or Community Impact	1: Summary, 12: Data Verification (12.4.2, 12.4.3, 12.5.6, and 12.5.7), 20: Environmental Studies, Permitting and Social or Community Impact, 25: Interpretation and Conclusions, 27: References
Emilie Williams	P.Eng (ON, QC)	Operating and Capital Cost Estimates	1: Summary, 15.7, 15.8 Mineral Reserves Estimates 21: Capital and Operating Costs, 22: Economic Analysis, 25: Interpretation and Conclusions, 26: Recommendations, 27: References

2.4 Site Inspections by Qualified Persons

Site Inspections were conducted by those individuals identified on Table 2.1.

Table 2.2: Site Inspection

Name	Specialization	Role	Site Visited	Site Visit Dates
Brian Thomas	Geology	Geology, Exploration, Data Verification, Mineral Resources	Mine	Feb 16-17, 2026
James Smith	Geomechanics	Geomechanics	Mine	April 2024
Khalid Mounhir	Mine Engineering	Mineral Reserves	Mine	Feb 16-17, 2026
David Jin	Mineral Processing	Metallurgical Testing and Mineral Processing	Mill	Feb 16-17, 2026

2.5 WSP Declaration

This report and the opinions of Qualified Persons in the employ of WSP contained herein and effective March 31, 2026, are based on information collected throughout the course of investigations by the Qualified Persons. The information in turn reflects various technical and economic conditions at the time of writing the Technical Report. Given the nature of the mining business, these conditions can change significantly over relatively short periods of time. Consequently, actual results may be significantly more or less favorable.

This Technical Report may include technical information that requires subsequent calculations to derive subtotals, totals, and weighted averages. Such calculations inherently involve a degree of rounding and consequently introduce a margin of error. Where these occur, the Qualified Persons do not consider them to be material.

Neither WSP, nor the QPs responsible for this Technical Report, are insiders, associates, or affiliates of Talon or Eagle Mine LLC. The results of the technical review by the Qualified Persons are not dependent on any prior agreements concerning the conclusions to be reached, nor are there any undisclosed understandings concerning any future business dealings.

2.6 Forward-Looking Information and Non-GAAP Measures

2.6.1 Forward-Looking Information

This Technical Report contains “forward-looking information” and “forward-looking statements” within the meaning of applicable Canadian and United States securities legislation, which involve a number of risks and uncertainties. Forward-looking information and forward-looking statements include, but are not limited to, statements with respect to the future prices of nickel and copper, the estimation of Mineral Resources and Reserves, the realization of mineral estimates, the timing and amount of estimated future production, costs of production, capital expenditures, costs (including capital costs, operating costs and other costs) and timing of the LOM, rates of production, annual revenues, requirements for additional capital, government regulation of mining operations, environmental risks, unanticipated reclamation expenses, title disputes or claims, and limitations on insurance coverage.

Often, but not always, forward-looking statements can be identified by the use of words such as “plans”, “expects”, or “does not expect”, “is expected”, “budget”, “scheduled”, “estimates”, “forecasts”, “intends”, “anticipates”, or “does not anticipate”, or “believes”, or variations of such words and phrases or state that certain actions, events or results “may”, “could”, “would”, “might” or “will” be taken, occur, or be achieved.

Forward-looking statements are based on the opinions, estimates, and assumptions of contributors to this Technical Report. Certain key assumptions are discussed in more detail. Forward-looking statements involve known and unknown risks, uncertainties, and other factors which may cause the actual results, performance, or achievements of Talon to be materially different from any other future results, performance, or achievements expressed or implied by the forward-looking statements.

Such factors include, among others: the actual results of current development activities; conclusions of economic evaluations; changes in project parameters as plans continue to be refined; future prices of nickel and copper; possible variations in ore grade or recovery rates; failure of plant, equipment, or processes to operate as anticipated; accidents, labor disputes and other risks of the mining industry, delays in obtaining governmental approvals or financing, or in the completion of development or construction activities; shortages of labor and materials, the impact on the supply chain and other complications associated with pandemics, including the COVID-19 (coronavirus) pandemic; as well as those risk factors discussed or referred to in this Technical Report and in Talon’s documents filed from time to time with the securities regulatory authorities in Canada.

There may be other factors than those identified that could cause actual actions, events, or results to differ materially from those described in forward-looking statements, and there may be other factors that cause actions, events, or results not to be anticipated, estimated, or intended. There can be no assurance that forward-looking statements will prove to be accurate, as actual results and future events could differ materially from those anticipated in such statements. Accordingly, readers are cautioned not to place undue reliance on forward-looking statements. Unless required by securities laws, the authors undertake no obligation to update the forward-looking statements if circumstances or opinions should change.

2.7 Abbreviations

Abbreviations and acronyms used in this Technical Report are included in Table 2.3.

Table 2.3: Abbreviations and Acronyms

Abbreviation	Description
°	degree
°C	degrees Celsius
3D	three-dimensional
CAGR	compound annual growth rate
CCP	Cumulative probability plots
CIM	Canadian Institute of Mining, Metallurgy and Petroleum
cm	centimeter
CN	Canadian National Railway
COG	cut-off grade
COSA	Coarse ore storage area
CRF	Cemented rock fill
CV	Coefficients of Variation
D&F	Drift and Fill Mining
DDH	diamond drill holes
DI	de-ionized water
EGLE	Michigan Department of Environment, Great Lakes, and Energy (EGLE)
ESG	Environmental, social, and governance
E-W	east-west
EOR	Engineer of Record
FAR	Fresh Air Raise
g	gram
G&A	General and Administrative
GISTM	Global Industry Standard on Tailings Management
GOB	Uncemented rock fill (i.e., waste rock)
Golder	Golder Associates Ltd., a member of WSP
GPM	US gallons per minute
GPS	global positioning system
Ha	hectare
HCl	hydrochloric acid
HTDF	Humboldt Tailings Disposal Facility
Hwy	highway
ICP-MS	inductively coupled plasma mass spectrometry
IRR	internal rate of return
kg	kilogram
kg/m^3	kilograms per cubic meter
km	kilometer
kt	kilotonnes
ktpy	thousand tonnes per year
kVA	kilovolt amperes
LOM	life-of-mine
LSLOS	Longitudinal Sublevel Open Stoping
m	meter
M	million
M+I	Measured and Indicated
m^3	cubic meter
masl	meters above sea level
mg/L	milligrams per litre

Abbreviation	Description
mm	millimeter
MDEQ	State of Michigan Department of Environmental Quality
Mt	million tonnes
NI 43-101	National Instrument 43-101
NNC	Nearest Neighbor Corrected
NPC	Normal Portland cement
NPV	net present value
N-S	north-south
NSR	net smelter return
OK	Ordinary Kriging
P.Eng.	Professional Engineer
PEA	Preliminary Economic Assessment
PFS	Pre-feasibility Study
PPC	Preparedness, Prevention, and Contingency
ppm	parts per million
PPV	Peak particle velocity
QP	Qualified Person
RAR	Return Air Raise
RC	reverse circulation
RQD	rock quality designation
SEDAR	System for Electronic Document Analysis and Retrieval
Sedex	sedimentary exhalative
sg	specific gravity
SGA	Selling, general, and administration
SR	strip ratio
t	tonne
t/m^3	tonnes per cubic meter
tpd	tonnes per day
tph	Tonnes per hour
TARP	Trigger Action Response Plan
TMF	tailings management facility
tpy	tonnes per year
TR	Technical Report
TSLOS	Transverse Sublevel Open Stoping
$	United States Dollar

3. Reliance on Other Experts

The authors have followed standard professional procedures in preparing the contents of this Technical Report. Data used in this Technical Report have been verified, and the authors have no reason to believe information has been withheld that would affect the conclusions made herein. The QP opinions contained herein are based on information provided to the QPs by Talon throughout the course of the investigations. The QPs have taken reasonable measures to confirm the information provided by others and take responsibility for the information.

The QPs used their experience to determine if the information from previous reports was suitable for inclusion in this Technical Report and adjusted information that required amending. The QPs do not disclaim any responsibility with respect to the inclusion of the information from the previous reports.

The QPs relied on Talon for guidance on applicable taxes, royalties, and other government levies or interests applicable to revenue or income from the Eagle Mine. The QPs have not performed an independent verification of land title and tenure as summarized in Item 4.0 of this Technical Report. The QPs did not verify the legality of any underlying agreement(s) that may exist concerning the permits or other agreement(s) between third parties, but have relied on information provided by Talon and Eagle Mine LLC, as of February 28, 2026, for land title issues.

4. Property Description and Location

4.1 Location

The Eagle Mine property, measuring approximately 0.63 km^2, is located in the Upper Peninsula of Michigan, USA, at geographic co-ordinates 46° 45' north latitude by 87° 54' west longitude (UTM Zone 16N coordinates 5177557 m N, 432639 m E), in Michigamme Township, Marquette County. The Humboldt Mill property, measuring approximately 1.42 km^2, is located 61 km west of Marquette and approximately 105 km by road from the mine site. The center point of the Humboldt Mill area (including all ownership of land) is 46º 29' north latitude, 87º 54' west longitude (UTM Zone 16N Zone coordinates 5148824 m N, 430843 m E).

The property location is shown in Figure 4.1, and the locations within the Upper Peninsula are shown in Figure 4.2.

The first Eagle Mine leases were held by Kennecott Exploration Company (KEX) and were later assigned to Kennecott Eagle Minerals Company (KEMC). On October 4, 2012, the company's legal name was changed from KEMC to Rio Tinto Eagle Mine, LLC (RTEM). On July 17, 2013, LMC, through its indirect U.S. subsidiary Lundin Mining Delaware Ltd. (LMDL), acquired all of the membership interests of RTEM. Subsequently, on July 17, 2013, the name of RTEM was changed to Eagle Mine LLC. On January 9, 2026, Talon completed the acquisition of the U.S. subsidiaries of Lundin Mining US Ltd (LMUS) and LMDL, which included all of the membership interests of Eagle Mine LLC.

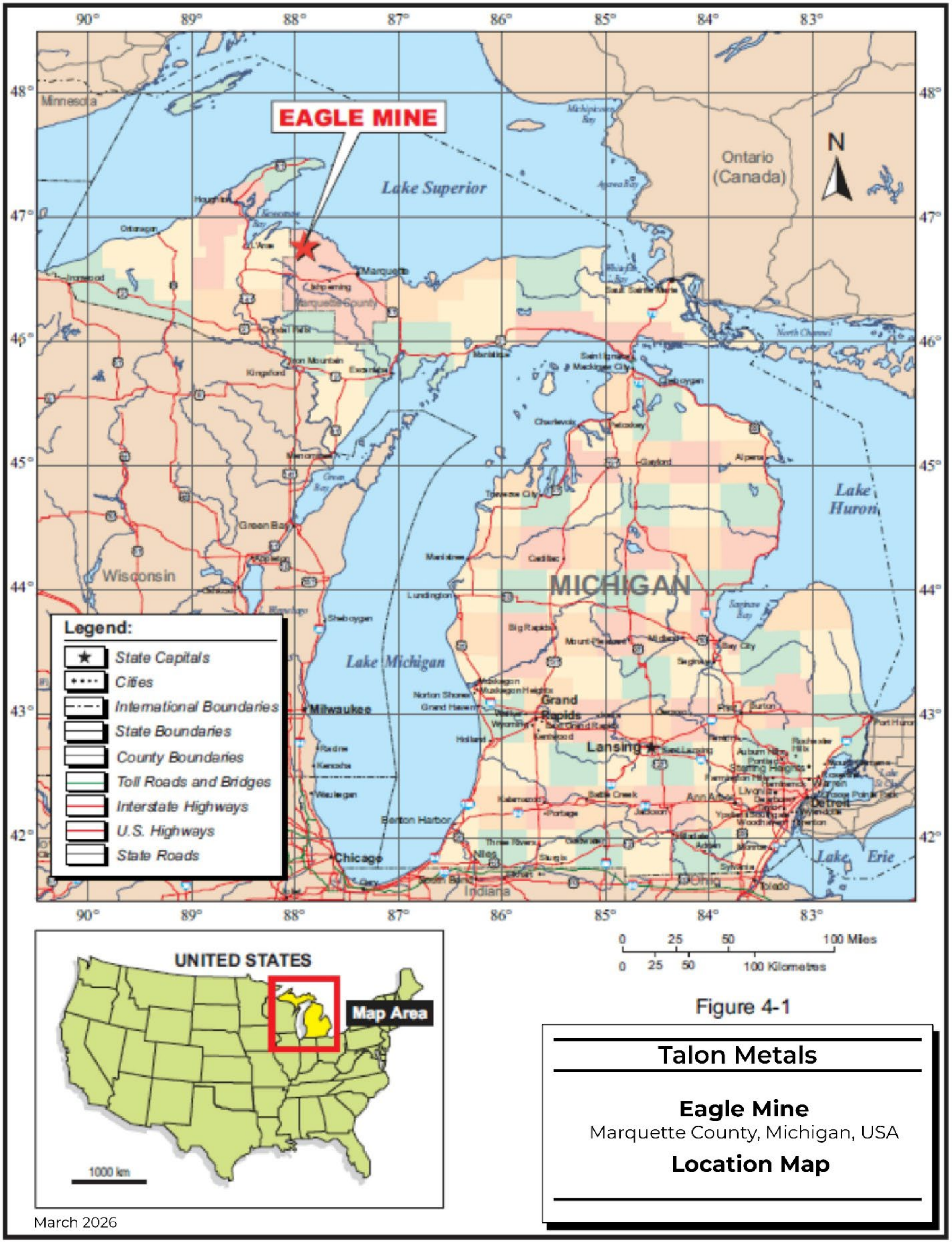


Figure 4.1: Eagle Mine Location Map (Talon Metals, 2026)

*Source: Lundin, 2023; Note: Each block = 1.61 km per side

Figure 4.2: Eagle Mine Location

4.2 Mineral Title and Land Ownership

Land ownership in Michigan allows for severed ownership, i.e., the owner of the surface rights may be different than the owner of the minerals beneath the same surface parcel. Where multiple people own minerals, they typically share an undivided interest for the entire parcel versus subsections of the property.

Lease payments are required for all parcels impacted by any decline, surface facility, or underground development, unless the parcel is wholly owned by Eagle Mine LLC. Agreements in place with private landowners related to the Eagle and Eagle East resource do not require an annual lease payment if production has begun on their property and the royalty payment is greater than their annual lease payment. The State of Michigan mineral properties, however, require an annual payment for mineral lease areas not included in a "mining operation area" (in 40-acre increments), i.e., the area without active production.

Surface and mineral rights in Michigan are held in units based on the Public Land Survey System. Townships comprise 6 by 6 arrays of 36 Sections, named according to distance and direction from a Principal Meridian and Baseline. Sections are generally one-mile squares, and can be divided into quarters, labeled NE, NW, SE, and SW. Each quarter may also be split into halves or quarters, which are labeled according to the side or corner of the quarter-section they encompass (e.g., NE quarter of the NW quarter).

4.2.1 Land Tenure

Eagle Mine LLC holds surface and mineral rights over Eagle Mine, Eagle East, Keel, and Humboldt Mill properties via a number of leases and agreements with the State of Michigan and private owners. In addition, Eagle Mine LLC owns some surface and mineral rights through previous purchases via various types of deeds. Separate agreements are in place with the owners of both the surface and mineral rights, as required.

4.2.2 Surface And Mineral Rights

Eagle Mine LLC holds surface and mineral rights over a wide district encompassing portions of Sections 4-9 and 16-18, Township 50N, Range 28W, and Sections 1-5 and 8-17, Township 50N, Range 29W. The overall footprint of land controlled by Eagle Mine LLC comprises leases, agreements, or ownership totaling approximately 5,049 ha of mineral rights and approximately 2,698 ha of surface rights.

Land blocks impacted by the operations of the Eagle Mine are listed in Table 4.1 and shown in Figure 4.3. Bounding vertices for each block, in UTM Zone 16N coordinates, are listed in Table 4.2. Figure 4.3 also shows the overall footprint of land controlled by Eagle Mine LLC (both mineral and surface rights), as well as the breakdown of mineral rights ownership.

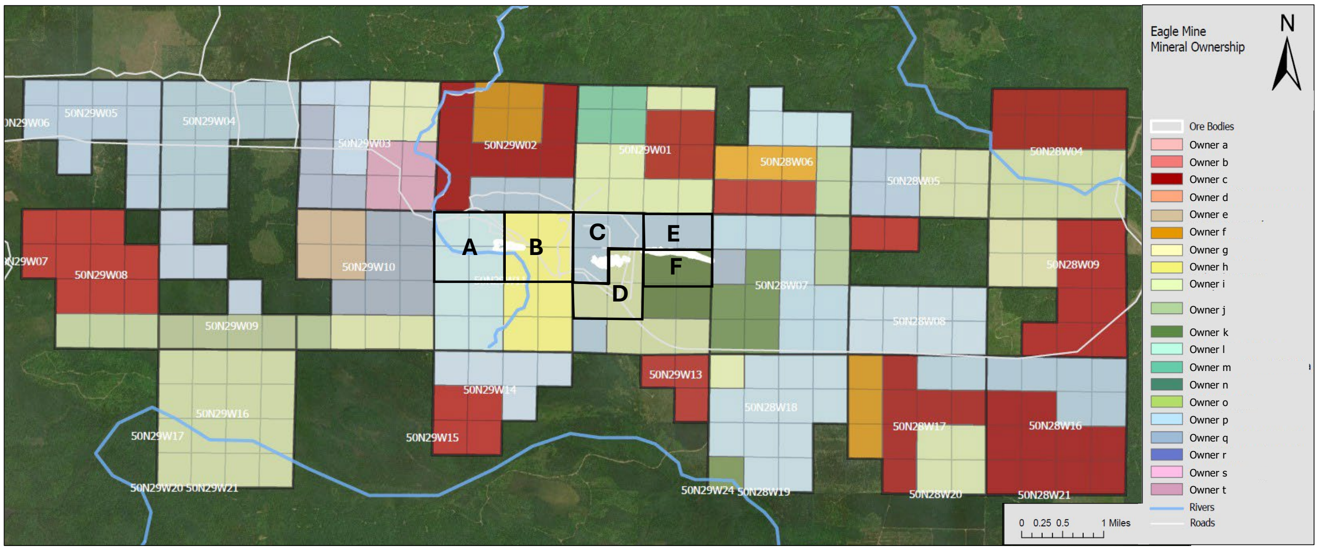
Table 4.1: Surface and Mineral Rights, Eagle Mine

Block	Description	Depicted Acres/km^2	Mineral Owner	Lease Origin Date	Primary Term Expiry	Surface Owner
A	Twp 50 N, Range 29 W, W ½ Section 11 (Block A on map)	320/1.29	State of Michigan, Leased to Eagle Mine LLC under M-00602	July 8, 1992	July 7, 2033, extendable by production	100% Eagle Mine LLC
B	Twp 50 N, Range 29 W, E ½ Section 11 (Block B on map)	320/1.29 (56.25%)	Three private owners with 56.25% ownership; leased to Eagle Mine LLC	November 15, 1995	November 14, 2015, but are extendable by continuation of payments and production	100% Eagle Mine LLC
B	Twp 50 N, Range 29 W, E ½ Section 11 (Block B on map)	320/1.29 (25%)	One private owner with 25% ownership; leased to Eagle Mine LLC	May 15, 2002	NA	100% Eagle Mine LLC
B	Twp 50 N, Range 29 W, E ½ Section 11 (Block B on map)	320/1.29 18.75%)	18.75% Eagle Mine LLC			100% Eagle Mine LLC
C	Twp 50 N, Range 29 W, N ½ of NW ¼ and SW ¼ of NW ¼, Section 12 (Block C on map)	120/0.49	State of Michigan, Leased to Eagle Mine LLC under M-00603	July 8, 1992	July 8, 2032, extendable by production	100% State of Michigan (See Table 4.3 below)
D	Twp 50 N, Range 29 W, SE ¼ of NW ¼ and N ½ of SW ¼, Section 12 (Block D on map)	120/0.49	100% ownership via 12 private owners under lease to Eagle Mine LLC or owned by Eagle Mine LLC	Multiple	Multiple – extendable by cross-mining and production from other properties.	100% Eagle Mine LLC
E	Twp 50 N, Range 29 W, N ½ of the NE ¼, Section 12 (Block E on map)	80/0.32	State of Michigan, Leased to Eagle Mine LLC under M-00603	July 8, 1992	July 7, 2032, extendable by production	100% State of Michigan
F	Twp 50 N, Range 29 W, S ½ of NE ¼, Section 12 (Block F on map)	80/0.32	One private owner with 100% ownership; leased to Eagle Mine LLC	May 25, 2005	May 25, 2055	100% State of Michigan

Table 4.2: Eagle Land Block Vertices

Vertex ID	Easting	Northing	Vertex ID	Easting	Northing
A1	430695.78	5177968.02	C7	432292.15	5177149.41
A2	431098.59	5177964.85	C8	432300.28	5177552.23
A3	431501.41	5177961.68	D1	432700.63	5177546.77
A4	431494.05	5177559.25	D2	433101.10	5177541.30
A5	431486.74	5177156.80	D3	433093.28	5177138.35
A6	431083.58	5177160.48	D4	433085.48	5176735.65
A7	430680.47	5177164.18	D5	432684.65	5176741.22
A8	430687.97	5177567.93	D6	432283.82	5176746.79
B1	431501.41	5177961.68	D7	432292.15	5177149.41
B2	431904.91	5177958.35	D8	432692.59	5177143.80
B3	432308.41	5177955.03	E1	433108.95	5177944.22
B4	432300.28	5177552.23	E2	433509.33	5177938.43
B5	432292.15	5177149.41	E3	433909.75	5177932.70
B6	431889.45	5177153.10	E4	433902.28	5177529.97
B7	431486.74	5177156.80	E5	433501.69	5177535.61
B8	431494.05	5177559.25	E6	433101.10	5177541.30
C1	432308.43	5177955.04	F1	433101.10	5177541.30
C2	432708.66	5177949.64	F2	433501.69	5177535.61
C3	433108.95	5177944.22	F3	433902.28	5177529.97
C4	433101.10	5177541.30	F4	433894.80	5177127.24
C5	432700.63	5177546.77	F5	433494.04	5177132.78
C6	432692.59	5177143.80	F6	433093.28	5177138.35

While the surface of the Eagle Mine is on Eagle Mine LLC property or property leased from the State of Michigan, the minerals comprising the Eagle Mine are either owned or leased from private owners or the State of Michigan. The state leases were renewed in 2022 for a period of 10 years. The private leases have various expiry dates that are extendable by continued payments or production. An annual lease payment is currently made, in addition to a royalty payment based on a percentage of the NSR, to the owners while the mine is in production.



Notes:

1. Lease payments would remain for the duration of mining at Eagle East, although royalty payments related to Eagle would cease when production from Eagle ends.
2. The Eagle deposit lies within the NW and NE quarters of Section 11, Township 50 North, Range 29 West. In the NW quarter (Block A), the deposit straddles the boundary between quarter-quarter NENW and SENW. Mineral rights for this area are leased from the State of Michigan. In the NE quarter of Section 11 (Block B), the surface is owned by Eagle Mine, LLC, and the mineral rights are held through lease agreements with individuals (81.25%) and ownership by Eagle Mine LLC (18.75%).
3. The Eagle East deposit lies against the northern border of the southern half of the northeastern quarter of Section 12 (Block F).

Source: Talon, 2026

Figure 4.3: Eagle Mine Land Blocks

The Keel deposit is a newly defined zone located on the East side of the mine between Eagle East and Eagle deposits. The deposit lies within the northern border of the southern half of the northwestern quarter of Section 12.

4.2.3 Surface Rights

Surface rights are owned by Eagle Mine LLC in Blocks A, B, and D. Block C is controlled by Eagle Mine LLC through a Surface Use Lease with the State of Michigan, while Blocks E and F are available for lease through the State of Michigan, if required.

The Eagle Mine surface rights are summarized in Table 4.3.

Table 4.3: Surface Land Tenure (production related), Eagle Mine

Description	Depicted Acres/km^2	Surface Owner	Lease Origin Date	Expiration Date
Twp 50 N, Range 29 W, N 1/4 Section 11 (Block B on map)	160/0.65	Eagle Mine LLC		None
Twp 50 N, Range 29 W, N ½ of NW ¼ and SW ¼ of NW ¼, Section 12 (Block B on map)	120/0.49	Three private owners with 56.25% ownership; leased to Eagle Mine LLC	July 8, 1992	July 8, 2032, extendable by production and reclamation/post closure monitoring requirements
Twp 50 N, Range 29 W, SE ¼ of the NW ¼ and the N ½ of the SW ¼, Section 12 (Block B on map)	40/0.26	Eagle Mine LLC		None

Note: Areas given in this table are only reflective of the areas depicted in Figure 4.3 and may not be indicative of the fully leased area.

A detailed description of blocks impacted by production at Eagle, as shown in Figure 4.3, is given below. Note that areas given in the descriptions below may not be representative of the entirety of ownership associated with the involved leases.

4.2.3.1 Block A

Eagle Mine LLC owns the surface with mineral rights from State of Michigan Metallic Minerals Lease M-00602 dated July 8, 1992, from the State of Michigan in favor of Terence W. Quigley, as lessee, as assigned to KEX pursuant to the Assignment of Metallic Minerals Leases dated August 27, 1993, and assigned to KEMC pursuant to the Assignment of Metallic Minerals Leases dated August 24, 2006. The primary term of this lease was extended to July 7, 2032, and is extendable by production. The area of interest for the purpose of this Technical Report is the 160 acres (64.7 ha) comprising the northwest ¼ of Section 11, Township 50 North, Range 29 West, as defined by the following coordinates (UTM Zone 16N) given in Table 4.3.

A sliding scale production royalty based on the Adjusted Sales Value per tonne of ore applies to this parcel.

4.2.3.2 Block B

Eagle Mine LLC has surface ownership with mineral rights leased from a total of four owners; three own a 3/16th undivided interest (18.75%) each, and a fourth owns the remaining 25%. Eagle Mine LLC owns 18.75%. Various NSR royalties are payable on each of the leased mineral estates.

Three owners own 56.25% of the gross mineral estate of, for the purpose of this Technical Report, 160 acres (64.7 ha), situated in the northeast ¼ of Section 11, Township 50 North, Range 29 West, as defined in Table 4.3. These three Mineral Lease Agreements, dated November 15, 1995, were executed in favor of KEX, as amended by the First Amendment to Mineral Lease dated June 25, 2001, by and between KEX, as assigned to KEMC pursuant to an unrecorded Assignment Agreement dated April 1, 2004. These leases are also subject to the

Second Amendment to Mineral Lease, dated March 1, 2014. The aforementioned leases each expired on November 14, 2015, and are extended by continuation of payments.

The additional 25% ownership is held by a single owner in a Mineral Lease Agreement, dated May 1, 2002, in favor of KEX, as assigned to KEMC pursuant to an unrecorded Assignment Agreement, dated April 1, 2004, expiring May 15, 2037, and extendable to May 15, 2054, by continuing payments, after which active mining must occur.

4.2.3.3 Block C

Surface ownership is by the State of Michigan through Surface Use Lease L-9742 (a/k/a SUL No. 11) dated July 8, 2008. Mineral rights, for the purpose of this Technical Report, comprise 120 acres (48.6 ha), being the north ½ of the northwest ¼ and the southwest ¼ of the northwest ¼ of Township 50 North, Range 29 West, Section 12 (as defined in Table 4.3), from State of Michigan Metallic Minerals Lease M-00603, dated July 8, 1992, from the State of Michigan in favor of Terence W. Quigley, as lessee, as assigned to KEX pursuant to the Assignment of Metallic Minerals Leases, dated August 27, 1993, as assigned to KEMC pursuant to the Assignment of Metallic Mineral Leases dated August 24, 2006. The primary term of M-00603 was extended to July 7, 2032, and is extendable by production. The expiration date of the Surface Use Lease coincides with the expiration dates of M-00602 and M-00603, July 8, 2022. These state leases were renewed in 2022 for a period of 10 years and are extendable by production or reclamation and closure activities.

4.2.3.4 Block D

Eagle Mine LLC owns the surface with 100% of mineral rights shared among 21 people and undivided ownership by Eagle Mine LLC. These leases have variable extents, expiration dates, proportional interests, execution dates, and extension provisions, as well as various amendments with variable dates. The area of interest for the purpose of this Technical Report is 120 acres (48.6 ha) composed of the Southeast ¼ of the Northwest ¼ and the North ½ of the Southwest ¼ of Section 12, Township 50 North, Range 29 West, as defined in Table 4.3.

4.2.3.5 Block E

Surface is owned by the State of Michigan with mineral rights from State of Michigan Metallic Minerals Lease M-00603 for lands in Township 50 North, Range 29 West, N ½ of the NE ¼, Section 12, dated July 8, 1992 from the State of Michigan in favor of Terence W. Quigley, as lessee, as assigned to KEX pursuant to the Assignment of Metallic Minerals Leases dated August 27, 1993, as assigned to KEMC pursuant to the Assignment of Metallic Mineral Leases dated August 24, 2006. The primary term of M-00603 was extended to July 7, 2032, and is extendable by production. The block is defined as listed in Table 4.3, containing 80 acres (32.4 ha) for the purpose of this Technical Report.

4.2.3.6 Block F

Surface is owned by the State of Michigan, with mineral rights held by a single owner and leased to Eagle Mine LLC for lands in Township 50 North, Range 29 West, S ½ of the NE ¼, Section 12, dated May 25, 2005, for a period of 30 years. The block is defined as listed in Table 4.3 and is subject to a sliding scale NSR royalty. The area of interest for the purpose of this Technical Report is 80 acres (32.4 ha).

4.2.4 Humboldt Mill

The Humboldt Mill property, measuring approximately 1.42 km^2, is located 61 km west of Marquette in Sections 2 and 11, Township 47 North-Range 29 West, Township of Humboldt, Marquette County, Michigan. The center point of the Humboldt Mill area (including all ownership of land) is 46º 29’ north latitude, 87º 54’ west longitude (UTM Zone 16N Zone coordinates 5148824 m N, 430843 m E). The land is held by both Humboldt Land LLC and Eagle Mine LLC through a series of deeds.

4.3 Royalties

4.3.1 Eagle Mine

Eagle Mine LLC is 100% owned by Talon Metals.

While the surface of the Eagle Mine is on Eagle Mine LLC property or leased from the State of Michigan, the minerals comprising the Eagle Mine are either owned or leased from private owners or the State of Michigan. Private interests and the 18.75% undivided interest owned by Eagle Mine LLC are in the northeast quarter of Section 11, Township 50 North, Range 29 West, while the State of Michigan owns minerals in the northwest quarter of the same section. The distribution of the Eagle Mine Mineral Resources is approximately 50:50 between the two quarters of the section. The leases have various expiry dates that are extendable by continued payments or production.

An annual lease payment is currently made, in addition to a payment based on a percentage of the NSR to the owners while in production. Royalty payments related to Eagle will cease when production from Eagle ceases. The QP has reviewed the confidential NSR rates, and in the QP’s opinion, they are within industry norms.

The QP is not aware of any other significant factors or risks that may affect access, title, or the right or ability to perform the proposed work program on the property.

4.3.2 Eagle East

Eagle East payments are based on a percentage of NSR to the owners while in production, which falls within the same range of royalty rates as Eagle. Lease payments will remain for the duration of mining at Eagle East. Eagle Mine LLC has all the required land access approvals to conduct the proposed work on the property.

Annual lease payments are currently made on the Keel, and any production within the Keel falls within the same range of royalty rates as Eagle and Eagle East on a percentage of NSR to the owners upon production.

4.4 Environmental Liabilities and Permitting

The property is subject to environmental liabilities typical of an operating underground mine and associated processing facility, including statutory reclamation and closure obligations for the Eagle Mine and Humboldt Mill, long-term post-closure groundwater and surface water monitoring requirements, and maintenance of financial assurance until regulatory release.

During Q3 2023 to Q4 2025, certain groundwater discharge permit limits were exceeded at the mine site. These exceedances were primarily related to administrative errors in the permit that require permit revisions, though Eagle is required to report the exceedances to the regulator in the meantime. A groundwater discharge permit application was submitted in January 2026.

No other material environmental liabilities are known at the time of writing. The QP has not identified additional factors that may impact the continued property tenure or operation of Eagle Mine LLC.

5. Accessibility, Climate, Local Resources, Infrastructure, and Physiography

5.1 Access

The closest full-service community to the Eagle Mine is Marquette, Michigan, 53 km away, a city with a population of approximately 21,000. Marquette has shipping and rail facilities, and daily air service to Detroit and Chicago from the Sawyer International Airport, which is located approximately 16 km to the south. Road access to the Eagle Mine property is excellent, with maintained loose surface and paved roads from the communities of Big Bay to the east, L'Anse to the west, and Marquette to the south. The closest community is Big Bay, 24 km from the property by road. Big Bay is primarily a cottage community with limited services.

The Humboldt Mill property, a former iron ore processing facility, occupying approximately 142 ha, is located approximately 61 km west of Marquette, close to the main US Highway 41. Ore from the Eagle Mine is trucked approximately 100 km to the Humboldt Mill for processing, starting from the mine, east on Triple A Road, northeast on County Road (CR) 510, south on CR 550, through the city of Marquette, and west on US Route 41.

There is no rail access at the Eagle Mine, but the Humboldt Mill is connected by rail to the CN Rail system at Ishpeming.

5.2 Local Resources

The region is served by an extensive network of paved roads, rail service, reliable telecommunications services, national grid electricity, and an ample supply of water. The property benefits from having access to an educated workforce.

Logging and mining have been a major part of land use activities for over 150 years. Copper and iron mining in the Marquette Range created many large open-pit mines and associated landforms. Logging is ongoing throughout the region. Agriculture is relatively limited, and there is minor commercial fishing for white fish and lake trout on Lake Superior. Urban development is concentrated around Marquette.

Recreation is an important land use, both along the shoreline and inland. The forested, hilly land with lakes and streams attracts hunters, fishermen, hikers, and other recreational users. The region is also very popular for snowmobiling in the winter. The mine is located 5 km east-northeast of the McCormack Tract, a Federal wilderness reserve.

Extensive third-party archeological studies revealed no Native American artifacts or evidence of areas of cultural significance. The Eagle Mine is located in the Ceded Territories, and the Keweenaw Bay Indian Community (KBIC) has claimed that the main outcrop of peridotite on State Mineral Lease M-00603 is of cultural significance. While there is no entry in the State historical records of any feature of Native American cultural significance, Eagle

Mine LLC has committed to protecting the rock outcrop from mining and offering access to the rock for cultural ceremonies.

5.3 Site Infrastructure

The surface and underground infrastructure at the Eagle Mine includes the following:

- Powerhouse
- Supply Storage Facility
- Water Treatment Plant
- Truck Wash
- Mine Services Building
- Mine Dry Facilities
- Three bay mobile maintenance shop
- Underground mobile maintenance shop
- Surface Sprung Maintenance workshop
- Contact Water Basins (CWB)
- Non-Contact Water Infiltration Basins (NCWIB)
- Coarse Ore Storage Area (COSA)
- Temporary Development Rock Storage Area (TDRSA)
- Crushed Aggregate Storage
- Concrete Backfill Batch Plant
- Mine portal connected by decline and levels to the Eagle, Eagle East, and Keel mining zones.
- Mine air heater and fresh air intake fan
- Surface Raise Site with exhaust fans
- Mine Security Gatehouse

There is no additional infrastructure required for the Keel deposit, as the existing Eagle Mine infrastructure would be used for the Keel Project. A paste plant is being considered by Talon for mining of the Keel.

At the time of QP's site visit, the infrastructure at the Humboldt Mill included the following:

- A 2,000-tpd flotation mill.
- Primary, secondary, and tertiary crushing circuits.
- Concentrate storage shed.

- Rail yard for rail car storage.
- Rail siding.
- Reclaim water system from tailings area.
- Tailings disposal to the HTDF.
- Water Treatment Plant.
- Mill Administration Building.
- Mill Services Building.
- Electrical power supply and distribution.
- SGS contract laboratory for mill and underground sample preparation and assaying.
- Coarse Ore Storage Area (COSA).
- Mill Security Gatehouse.

Eagle Exploration formerly maintained an office at the core handling/logging facility in Negaunee. This facility has now been converted into a training room and for core storage. Eagle Mine has an Information Center for visitors in Marquette.

5.4 Power

The mine site is serviced by grid power provided by the Alger Delta Electric Co-operative (ADEC). An agreement was signed between ADEC and KEMC on January 15, 2008, to provide power to the mine site. ADEC provides power from the city of Marquette to the town of Big Bay, and the overhead lines and associated substation were upgraded to provide 24.9/14.4 kV service to the mine site. The new line from the Big Bay line tap to the mine site is an underground line that supports the estimated 6.3 MVA requirement of the site. A powerhouse constructed at the mine site steps down the 24.9/14.4 kV utility power to 4.16 kV to support mine surface distribution and 13.8 kV to support mine portal, underground, and vent raise distribution. Emergency backup power is provided to portions of the mine by a 4.16 kV, 2,500-kVA diesel generator.

The Humboldt Mill site is predominantly serviced by the Upper Peninsula Power Company, with some power being supplied from WE Energies. The Upper Peninsula Power Company service is fed from a 69 kV American Transmission Company transmission line to an on-site, utility-owned substation. The substation steps down the incoming 69 kV power to 13.8 kV through two 10.5 MVA transformers situated in two redundant banks. This 13.8 kV is fed into the main concentrator building's 13.8 kV switchgear. This switchgear feeds 13.8 kV distribution to the reclaim water area for the mill, as well as pad-mounted transformers that step down the voltage to 4.16 kV and 480 V to support the mill process in a fully redundant design.

5.5 Water

An existing non-potable well, in conjunction with a potable well, provides service and drinking water to the mine site. Each is capable of delivering 150 USgpm. There are two wells at the mill: a potable well and a non-potable industrial well. Each is capable of delivering 100 USgpm. Currently, mill operations are supplied by recycled water from the HTDF, but can utilize the industrial well as needed. Hydrology studies at both sites indicate viable long-term aquifers. Both the mine and mill sites utilize septic systems.

5.6 Climate

The climate of northern Michigan is typical for the Great Lakes region, with warm summers and long, cold winters. The Eagle Mine and Humboldt Mill sites are located in a temperate region. The area's weather is characterized by variable weather patterns and large seasonal temperature variations. Summers are often warm and humid, and winters can be very cold with frequent snow showers and significant snow cover.

Mean high and low temperatures in Marquette range from -12.6ºC (9.4ºF) in January to a maximum of 25.3ºC (77.5ºF) in July. Mean daily temperatures vary from -8.9ºC (15.9ºF) in January to 19.3ºC (66.8ºF) in July. Snowfall in the region can be high; from 2010 to 2025, the average annual snowfall was 327.4 cm (128.9 in.). Mean annual precipitation for the same period was 894 mm (35.2 in.).

Lake Superior causes an identifiable lake effect on the area's climate during much of the year, increasing cloudiness and snowfall during the autumn and winter. This aspect, combined with the higher surface elevation, yields much higher snowfall amounts at the Eagle Mine and Humboldt Mill than recorded at the city of Marquette.

Exploration and mining activity can be carried out throughout the year.

5.7 Physiography

The Eagle Mine is on the watershed divide of the Yellow Dog River and Salmon Trout River. The Eagle Mine is located on the Yellow Dog Plains, where two hillocks of peridotite resistant to erosion protrude through the sandy glacial outwash till. The area is covered principally by boreal forest and wetlands with limited outcrop exposure. Lakes, rivers, and smaller streams are numerous in the area. Most of the streams have steep gradients, and many have waterfalls near Lake Superior. The Eagle Mine is at approximately 440 masl, and there is little relief in the surrounding area. Elevations drop to 200 masl at Marquette and rise again to approximately 500 masl at the Humboldt Mill.

Primary land use in the area of the Eagle Mine is logging, and much of the timber in the area has been logged and replanted. There are no operating metal mines in the immediate vicinity of the Eagle deposit. No permanent residences exist in the immediate area, although a handful of seasonal recreational cabins are within a few kilometers of the mine site.

6. History

6.1 Prior Ownership

Kennecott Exploration (KEX) started working in the region in 1991. In 2004, the project was transferred to Kennecott Minerals (Rio Tinto Copper Group) under the name Kennecott Eagle Minerals Company (KEMC). KEMC began construction of the Eagle Mine in April 2010 and began underground development in September 2011. On October 4, 2012, the company's legal name was changed from KEMC to Rio Tinto Eagle Mine LLC (RTEM). On July 17, 2013, LMC, through its indirect US subsidiary LMDL, acquired all of the membership interests of RTEM. Subsequently, the name of RTEM was changed to Eagle Mine LLC.

LMC operated the Eagle Mine and Humboldt Mill through January 9, 2026, when it was publicly announced that Talon had completed the acquisition of the mine and mill as first announced by Talon on December 18, 2025.

6.2 Previous Exploration and Development

The Baraga Basin region has, until recently, been subject to only sporadic exploration efforts. The earliest historical accounts of exploration in the basin date back to the mid-1800s when a group of investors tried to develop slate quarries along the Slate River. Little documented exploration work took place in the Baraga basin between 1910 and 1950. During the 1950s, Jones and Laughlin conducted an exploration program along the northern portion of the east branch of the Huron River, investigating uranium-silver-mercury mineralization associated with a graphitic shear exposed in the river. During the 1960s and 1970s, various interests conducted exploration programs on Ford Motor Company mineral lands in the Baraga Basin and the western portion of the Marquette Trough. The programs were primarily focused on uranium and zinc. The U.S. Department of Energy provided funding to drill a number of deep holes in the Baraga Basin during the 1970s, presumably to provide stratigraphic information for the uranium exploration effort.

Concurrently, the U.S. Geological Survey (USGS) began a bedrock-mapping program of the basin, focusing primarily on exposures in rivers, which produced an open-file outcrop map with little interpretation and no report. In 1976, Michigan Technological University drilled a 31 m hole on the east end of the Yellow Dog (Eagle East) outcrop. The hole bottomed in coarse-grained peridotite with only traces of sulfides. In 1979, the Michigan Department of Natural Resources (DNR), in conjunction with the USGS, published a report on the Yellow Dog peridotite describing the results of geochemical, petrographic, and geophysical studies of the peridotite (Klasner, et al., 1979). The authors concluded that the anomalous sulphur and copper contents of the outcropping peridotite indicated potential for a copper-nickel deposit. KEX started working in the region in 1991 and actively explored for sedimentary exhalative (Sedex) zinc deposits through 1994. During the course of mapping, float boulders of peridotite with sulfides were discovered that indicated the potential for magmatic sulfide mineralization. KEX partially shifted to magmatic nickel exploration in 1995 and drilled four holes to test the Yellow Dog peridotite (Eagle East). One hole (YD95-2) intersected 10 m of moderate to heavy disseminated sulfide mineralization along the southern contact. Two more angle holes (YD95-3 and YD95-4) collared on the east end of the Yellow Dog East outcrop demonstrated that the peridotite widened to the east but only intersected a meter or two of weak sulfide mineralization along the north and south contacts.

The more recent nickel exploration program started late in 2000. Drilling at the neighboring Eagle East target in July 2001 intersected 30 m of disseminated, semi-massive, and massive sulfides averaging 1.03% Ni and 0.75% Cu (YD01-01), and one of three holes on the east end of Eagle intersected 85 m of disseminated sulfides averaging 0.6% Ni and 0.5% Cu (YD01-06). In 2002, drilling at Eagle targeted the center of a magnetic anomaly defined by ground surveys in 2001. The first hole, YD02-02, intersected 84.2 m of massive pyrrhotite-pentlandite-chalcopyrite averaging 6.3% Ni and 4.0% Cu, firmly establishing the presence of economic-grade and width mineralization at Eagle. Subsequent definition drilling continued through the summer and autumn of 2002 and resumed in 2003. By the end of 2003, two separate high-grade sulfide zones were identified at Eagle. The lower zone was defined by 15 drill intercepts and the upper zone by six drill intercepts. This formed the basis of an order-of-magnitude study that was completed in early 2004. Upon Rio Tinto's acceptance of the order of magnitude study in early 2004, ownership of the Eagle project was transferred from KEX to KEMC for additional evaluation. KEMC conducted an extensive resource and geotechnical drill program in 2004, supplying the data to connect the former upper and lower zones and better establish the geometries of the massive sulfide, semi-massive sulfide, and host intrusive bodies. The result of this work was the completion of a pre-feasibility study.

Construction of the Eagle Mine commenced in April 2010, and underground development began in September 2011. The Humboldt Mill was refurbished, and the Eagle Mine achieved commercial production in November 2014.

From 2002 to 2008, Rio Tinto drilled more than 50 holes in the Eagle East intrusion, identifying uneconomic and largely disseminated mineralization. In June 2015, LMC announced the discovery of very high-grade magmatic nickel-copper mineralization similar in style to the Eagle deposit, located approximately two kilometers east of the Eagle Mine. The Eagle East deposit was discovered in an undrilled area approximately 960 m deep.

In 2016, LMC reported the initial Mineral Resources estimate for the Eagle East deposit, together with a positive PEA supporting further work on the deposit. Eagle Mine continued drilling from surface to delineate the deposit and undertook technical studies in support of the Eagle East Feasibility Study.

In 2019, the resource drilling was executed in the Keel, and a more detailed evaluation was completed. Although the Keel has been known since the early 2000s, the grades at that time were less attractive compared to the other zones and were not prioritized for further investigation. In 2022, the forecasted 5-year Nickel price made the zone more economically attractive, and the deposit was included in the 2023 Mineral Reserves and LOM plan.

6.3 Historical Mineral Resources and Reserves Estimates

In 2005, RPA was retained by Rio Tinto Technical Services (RTTS) to provide an independent audit of a Mineral Resource estimate for the Eagle Ni-Cu deposit. In a technical report, dated March 15, 2005, the Mineral Resource estimate was based on a total of 79 holes drilled on the Eagle deposit and a $25.00/t NSR cut-off value.

A number of internal and independent Mineral Resource estimates were prepared by and for RTEM (KMEC) between 2006 and 2012. To support LMC's purchase of Eagle in July 2013, an independent technical report was prepared by Wardell Armstrong International (WAI) (WAI, 2013). An independent NI 43-101 Mineral Resource estimate completed in accordance with NI 43-101 supporting the Eagle East mineralization was completed by RPA with an effective date of December 3, 2016.

WSP/Golder, along with Eagle personnel, updated the Mineral Resource estimates for the Eagle, Eagle East, and Keel deposits, effective December 31, 2022.

Talon is not treating any of the historical estimates as a current resource estimate. The QP has not completed sufficient work to consider the historical resource estimates as current, and they should no longer be relied upon. Refer to Item 14 of this Technical Report for the current MRE.

6.4 Historical Production

The historical production mined by Rio Tinto and LMC from the Eagle Mine is summarized in Table 6.1.

Table 6.1: Eagle Mine Production – Eagle Mine

Eagle Mine Production					
	Mill Feed	Feed Grade		Metal in Concentrates	
Year	(t)	Ni (%)	Cu (%)	Ni (t)	Cu (t)
2014	173,648	3.16	2.40	4,178	3,877
2015	746,466	4.31	3.36	27,167	24,331
2016	748,485	3.82	3.21	24,114	23,417
2017	754,096	3.44	2.88	22,081	21,303
2018	753,751	2.80	2.46	17,573	17,974
2019	747,061	2.20	1.99	13,494	14,297
2020	761,093	2.62	2.54	16,718	18,663
2021	699,134	3.12	2.71	18,353	18,419
2022	717,706	2.81	2.27	17,475	15,895
2023	717,705	2.62	1.96	16,429	13,600
2024	487,368	1.87	1.37	7,486	6,366
2025	685,546	1.73	1.36	9,907	8,906
Total	**7,992,060**	**2.90**	**2.41**	**194,976**	**187,049**

Copper in concentrates includes copper contained in copper and nickel concentrates.

7. Geological Setting and Mineralization

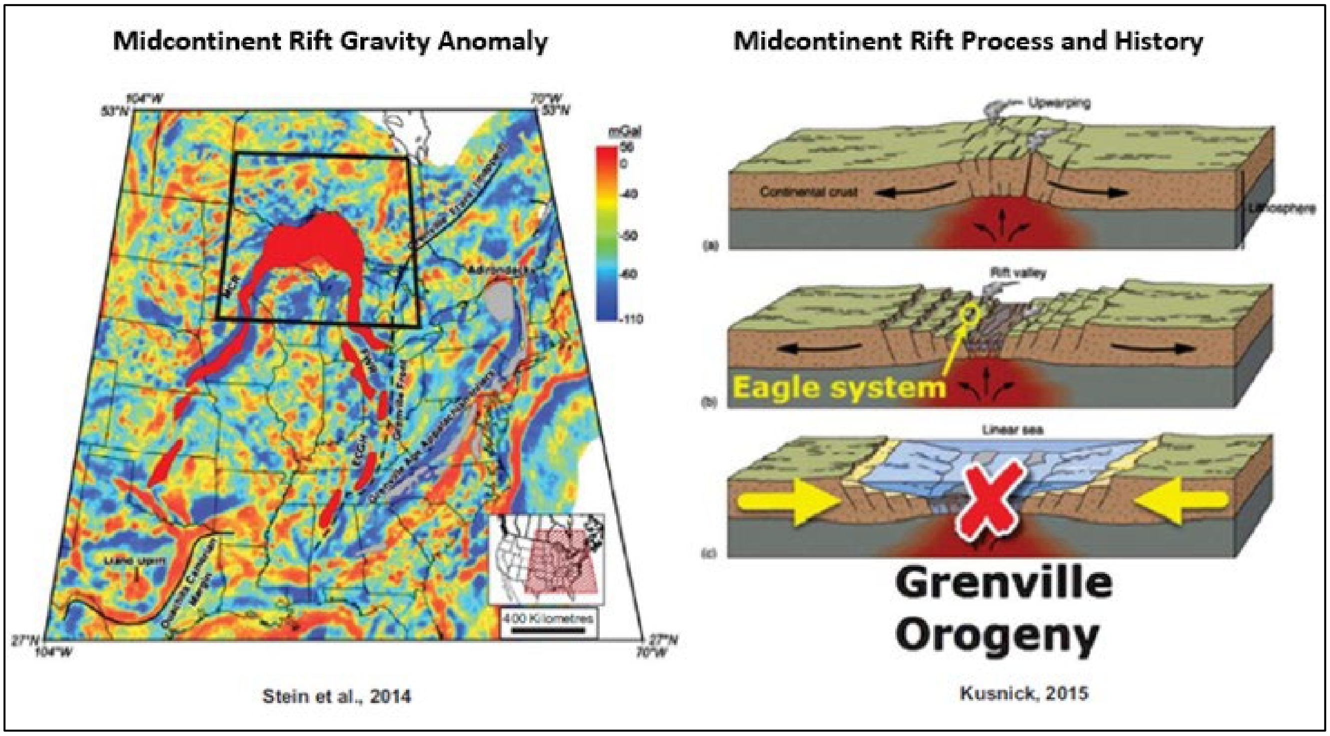
The Eagle intrusion, Eagle East intrusion, and the Keel are all part of the same ultramafic intrusive system and all host high-grade primary magmatic Ni-Cu sulfide mineralization. These intrusions are related to the feeder system for the Keweenawan flood basalts, a Large Igneous Province (LIP) resulting from mantle-tapping extension during the Midcontinent Rift.

Mineralization styles are similar in Eagle and Eagle East, consisting of mineralized peridotite bodies with concentrations of semi-massive sulfide in the center of the intrusions and massive sulfides at the base. Massive sulfides can extend for short distances outward beyond the contact of the peridotite, into the surrounding sedimentary country rocks as sills along bedding planes.

7.1 Geological Setting

The Midcontinent Rift formed when the North American continent began to split apart 1.1 billion years ago, resulting from the upward impact of a mantle plume. Rifting continued for 15 to 22 million years, at which point the rift failed. The rifting process consists of three main stages: mantle plume impact and upwelling, initial extension and flood basalt volcanism, and ongoing passive extension resulting in ocean basin formation.

In the first stage, upwelling occurs from the buoyant mantle plume underplating the crust. This results in the formation of tension cracks above the upwelling zone, which are often injected by magma, resulting in dike swarms. At the onset of rift extension, the crust thins as the crust on either side of the mantle plume begins to move apart, and the blocks bounded by tension cracks begin to subside into the rift depression. This results in normal fault movement, which accommodates the extension (Figure 7.1).



*Source: Lundin, 2023

Figure 7.1: Midcontinent Rift Gravity Anomaly and Midcontinent Rift Process and History

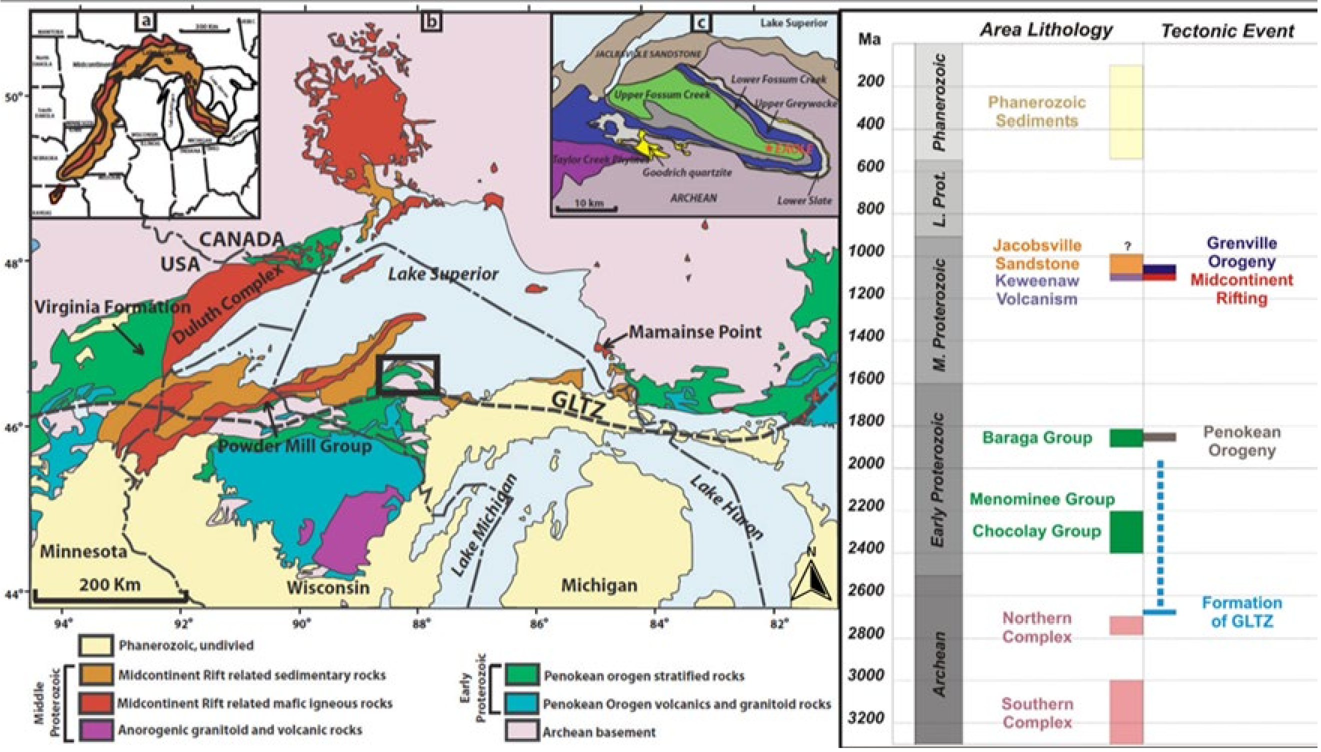
During the second phase, significant partial melting of the underlying mantle and lower crust occurs, resulting in volcanic eruptions and the formation of a flood basalt province. These large eruptions are often associated with the venting of large quantities of gas, including SO_2, which is important in the mineralization forming process, as magmas must be driven to sulphur saturation before sulfide droplets can form. Eagle and Eagle East are more mafic than the flood basalts and are likely related to partial melting of the mantle in the feeder zone to the flood basalts. These magmas migrate from deep staging chambers upward to episodic small volcanic vents along the edge of the main flood basalt province. These small, hot, low viscosity magmas exploit small, dilated spaces resulting from movement along faults, and can erupt vertically if the magma pressure overcomes the lithostatic pressure. This results in a structurally controlled but unpredictable magma conduit path to the surface. In conduit style systems, sulfide droplets settle out from sulphur-saturated magma wherever the velocity of the magma slows down due to a significant change in direction or change in conduit size, such as a small conduit entering a larger chamber or a conduit turning horizontal.

In the third stage of rifting, the rift is fully formed, and a passive crustal spreading center is formed on the ocean floor, similar to the mid-Atlantic ridge. Ongoing volcanism at the spreading center can form other types of deposits, such as VMS-style mineralization.

Further active volcanism can build islands such as Iceland, which continues to be a well-studied analog for Eagle-like volcanism. In the case of the Midcontinent, rifting halted prior to the influx of seawater into the basin.

7.2 Regional Geology

The Eagle Mine property is located in the Baraga Basin on the south side of Lake Superior (Figure 7.2). Three depositional periods are well represented in the region. These occurred in the Archean, Early Proterozoic, and Middle Proterozoic and are separated by pronounced unconformities related to major regional tectonic events.



*Source: Eagle Mine, 2023

Figure 7.2: Regional Geology and Geological History

7.2.1 Archean

The Archean basement rocks consist of two terranes separated by an ancient crustal suture zone known as the Great Lakes Tectonic Zone (GLTZ). The terranes consist of gneiss and granitoid to the north and migmatite to the south.

7.2.2 Paleoproterozoic

The Marquette Range Supergroup (MRS) consists of a package of sediments that unconformably overlie the Archean basement. The base of the MRS is a package of quartzite and chert carbonate (Goodrich Quartzite), which forms a distinct marker bed and strong seismic reflector. This is overlain by a package of barren sulfide-bearing black slates and greywackes which comprise the Baraga Basin. The Baraga Basin sediments are the country rock in which the Eagle Mine intrusions reside.

7.2.3 Mesoproterozoic

The Keweenaw Flood Basalt province represents the exposed portion of the Midcontinent Rift system in the Lake Superior region (Figure 7.2, left). The Midcontinent Rift forms a prominent gravity anomaly (Midcontinent gravity high) that can be traced southwest from the Lake Superior region into central Kansas and southeastward into southern Michigan. The total length of this geophysical feature is in excess of 2,000 km (Hinze et al., 1997). Seismic data indicate the rift below Lake Superior is filled with more than 25 km of volcanics buried beneath a total thickness of up to 8 km of rift filling sediments (Bornhorst et al., 1994).

The estimated volume of magmatic rocks associated with the rift is greater than two million km^3 (Cannon, 1992).

The Midcontinent Rift was previously thought to have failed because of regional compression associated with the Grenville Orogeny. New age dating suggests that the compressional event, which inverted the basin, postdates the Grenville Orogeny (Malone et al., 2016).

The Eagle deposit is located in the northern portion of the Mesoproterozoic Baraga-Marquette dike swarm. The Baraga-Marquette dike swarm comprises more than 150 primarily east-west trending dikes (Green et al., 1987). Although most dikes in the swarm are less than 30 m thick, individual dikes are up to 185 m thick and can be traced on magnetic maps for up to 59 km (Green et al., 1987). Compositionally, the dikes and associated intrusions of the Baraga-Marquette dike swarm can be broadly categorized into two groups, gabbroic and picritic. Gabbroic dikes are generally quartz-normative tholeiites with relatively low Al_2O_3 contents, similar to early-phase basalts of the Midcontinent rift. The picritic intrusions comprise elongate plugs, with maximum dimensions of a few hundred meters, and discontinuous dikes that range in thickness from less than a meter to over 70 m.

The picritic intrusions are typically more altered than the gabbroic intrusions. In some places, the picritic intrusions have been incorporated into later breccia dikes. Age dating of the dikes of the Eagle intrusive yielded an age of 1,107.2 ± 5.7 million years (Ma), and the gabbro that occupies the intrusive plumbing system below and east of the Eagle East deposit has a U-Pb baddeleyite date of 1103.4 ± 1.2 Ma. A gabbroic dike north of Eagle was dated at 1,120 Ma, which represents the start of rift-related intrusive activity.

7.2.4 Paleozoic

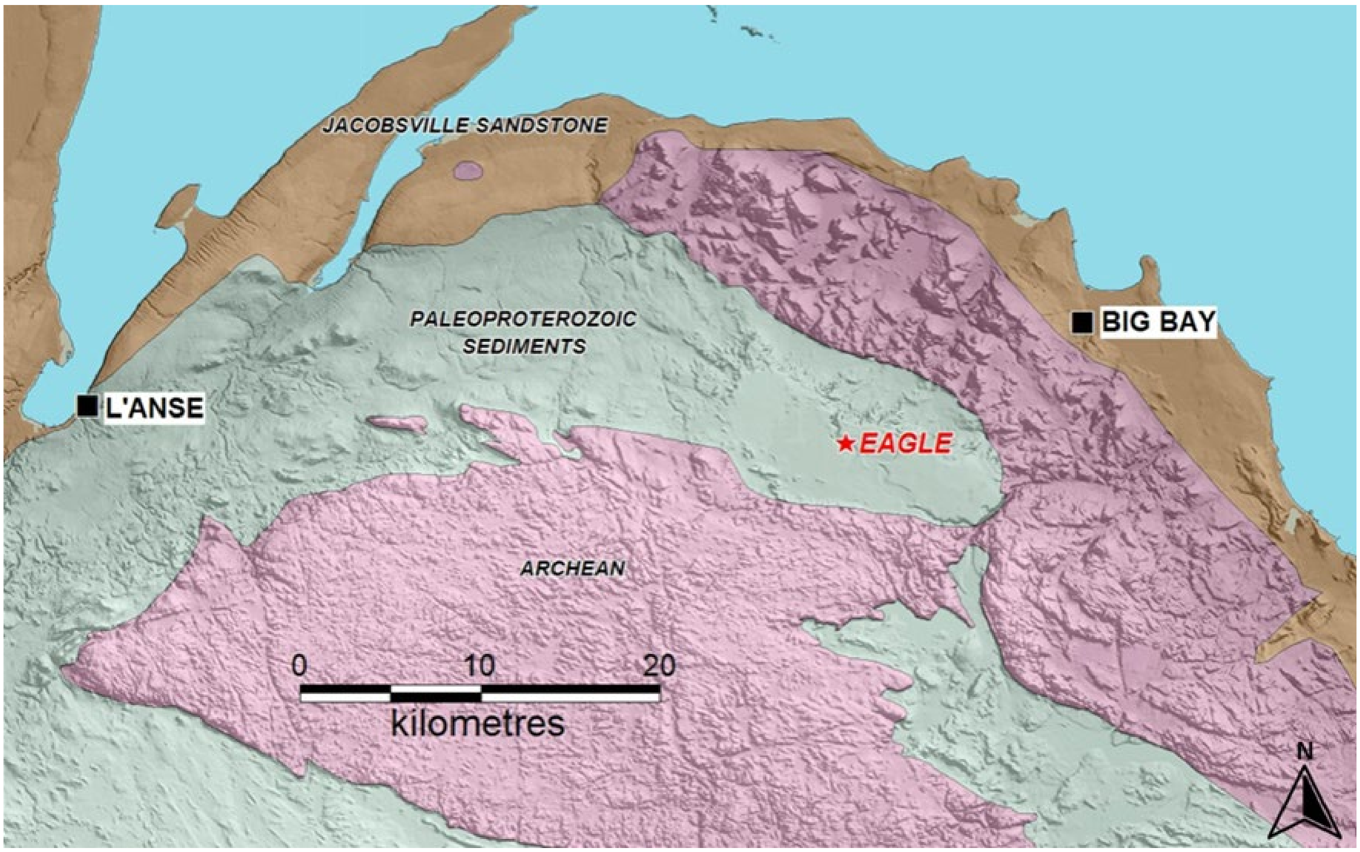
Paleozoic sediments in the eastern half of the Upper Peninsula cover the Precambrian basement. These gently south-southeast dipping sediments form the northern edge of the large Michigan Sedimentary Basin.

The entire Yellow Dog Plains area is covered by sandy till deposited in an outwash plain. Till thickness ranges from nil at the peridotite outcrop to greater than 100 m. Drilling in the wetland area directly above the Eagle peridotite indicates a till thickness of 10 m to 12 m. Till thickness increases to the east and is over 100 m thick above the Eagle East conduit zone. The till was locally reworked by later fluvial action into broad meandering stream channels.

7.3 Local and Project Geology

The Eagle deposit is located at the east end of the Baraga Basin, the northernmost basin of Paleoproterozoic sediments in Michigan (Figure 7.3). The host intrusions are part of the Mesoproterozoic Baraga-Marquette dike swarm.

The Eagle and Eagle East conduit zones are hosted in two peridotite intrusions. The Eagle East intrusion forms a prominent outcrop (historically known as the Yellow Dog Peridotite) that rises above the Yellow Dog Plains and is the site of the Eagle Mine portal. The western intrusion, 650 m to the west and host to the Eagle deposit, is only poorly exposed in a small subcrop on the north side of Salmon Trout River and is the site of the Eagle Mine ventilation raise. The intrusions are characterized by very prominent magnetic highs relative to the surrounding sedimentary rocks.



*Source: Eagle Mine, 2023

Figure 7.3: Local Geological Map of the Baraga Basin Area

The Eagle and Eagle East peridotite intrusions are hosted in Paleoproterozoic metasediments of the Baraga Basin, which rest unconformably on the Archean basement rocks. These sediments are assigned to the Upper Fossum Creek Unit and are mainly composed of an upper siltstone sequence with fine-grained turbiditic greywacke sandstone interbeds, which comprises the main sedimentary lithology found in Eagle Mine. A lower sequence of dark grey to black thin laminated slates and shales, medium grey thin-bedded siltstone, and rare fine-grained turbiditic sandstone is seen deeper and lateral to the intrusive rocks.

The Eagle East deposit is located deeper than the Eagle deposit, between -370 m and -550 m elevations (810 m to 990 m below surface). The host sediments encountered in the surroundings of the Eagle East mineralized zone are mainly siltstones with low proportions of sandstone interbeds. The assignment of these deeper sediments to the Lower Fossum Formation is not yet evaluated. Bedding and foliation are the main structural features present in the sediments and represent the weakest planar orientation found. All of these features are seen both in the Eagle and Eagle East drill core. Generally, the sediments exhibit hornfels within 10 cm to 20 m of the intrusive contact as a result of metasomatism. The presence of these can be confirmed around the Eagle intrusive, though the hornfels unit rarely exceeds 10 m in width.

The main intrusive types encountered in Eagle East are peridotites and pyroxenites, similar to those encountered in the Eagle Mine, with minor intrusives/dikes of mafic (mainly gabbroic) composition. All these mafic dikes are grouped together as they are not related to the mineralization.

7.3.1 Lithology

A summary of lithological, mineralization, and zone abbreviations is shown in Table 7.1. A summary of the major lithological units is also presented.

Table 7.1: Summary of Geological Domains – Eagle Mine

Domain	Abbreviation
Overburden	OB
Sediments	SLST
Mafic Dikes	PRX
Gabbro Intrusive	GAB
Peridotite (0-25% Sulfide)	PER
Semi-massive (25-85% Sulfide)	SMSU
Massive (85-100% Sulfide)	MSU

7.3.2 Sedimentary Units

The peridotites intrude siltstone assigned to the Upper Fossum Creek unit. The upper parts of the siltstone sequence are competent, light to medium grey and mostly thick-bedded, with minor fine-grained turbiditic greywacke sandstone interbeds (up to a few meters thick). Minor soft-sediment deformation features such as flame structures, slumping, and rip-ups are common, including infrequent thin laminated horizons or interbeds. Syngenetic sulfide is typically pyrite with minor pyrrhotite as thin laminae. Foliation in the sedimentary sequence is a dominant feature that forms the weakest planar orientation. Near the hanging wall contact to the Eagle peridotite (within 10 m to 20 m), foliation in the rock is not visible, and the rock becomes weakly hornfels altered. More proximal to the contact (0 m to 5 m), hornfels alteration is fairly strong, although the protolith can usually still be identified. Small-scale folds are both post-foliation (though possibly pre-mineral) and syn-foliation. Other notable features in the upper siltstone are one to two thin 10 cm to 20 cm banded quartz-silica beds that are useful as markers within the Eagle deposit area.

The sediments are upright and slightly tilted, dipping 10° to 25° to the east-northeast. A lower sequence (seen deeper and lateral to the intrusions) is defined by a dominance of dark grey to nearly black thin laminated slates/shales, syngenetic sulfide laminae (pyrite giving way to pyrrhotite+/-pyrite- chalcopyrite), medium grey thin-bedded siltstone, and rare fine-grained turbiditic sandstone. Subtle soft sediment structures are present in the lower sequence. Foliation, absent within 5-10 m of the peridotite contacts, is less obvious in the dark shales than in the upper grey siltstone, though visibly present. This sequence has been tentatively assigned to the Lower

Fossum Creek unit in some Eagle drill logs but is more likely a portion of the Upper Fossum Creek unit. The closest outcrop of sedimentary rocks is 10 km to the west of Eagle at the Huron River.

7.3.3 Peridotite

Medium to coarse-grained massive peridotite and feldspathic peridotite are the most common rock types and form the cores of both intrusions. The peridotite in the cores of the intrusions lacks obvious layering, banding, or foliation. The lack of penetrative, tectonic foliation is an important indication that the intrusions are not Paleoproterozoic in age. In hand sample, the peridotite is dark greenish grey on fresh surfaces. In core, feldspathic peridotite can have a mottled white and dark grey color (salt and pepper). In thin section, the peridotite comprises approximately 30% to 60% olivine. The olivine typically occurs as 2 mm to 5 mm round to ovoid grains, and is dominantly altered to serpentine. Textural evidence suggests that olivine is an early cumulate phase (Klasner et al., 1979). Chrome spinel occurs as inclusions in olivine, suggesting that it is also an early cumulus phase. Megacrystic and glomeroporphyritic olivine have also been noted, indicating that there might be multiple generations of olivine (Klasner et al., 1979). Pyroxene makes up 25% to 45% of the peridotite. Clinopyroxene is slightly more abundant than orthopyroxene in most samples. Both clinopyroxene and orthopyroxene are typically poikilitic or sub-poikilitic to olivine with pyroxene oikocrysts up to a centimeter across. USGS geologists in an early study (Klasner et al., 1979) described euhedral orthopyroxenes that could have also formed as an early cumulate phase. Anhedral plagioclase forms an intermediate to late intercumulus phase. In many places, the plagioclase is patchy, but over some significant intervals, it can average 25% to 30% (feldspathic peridotite). Other probable late intercumulus minerals include biotite, which can average up to a few percent, some possibly minor primary amphibole, Fe-Ti oxides, and sulfides. Early microprobe work on samples of unmineralized peridotite showed that olivine compositions ranged from Fo79 to Fo82 with NiO contents from 0.24% to 0.49% (Morris, 1977). A negative correlation between MgO and NiO contents in olivines could be an indication of subsolidus re-equilibration with co-existing sulfides. Clinopyroxenes have the compositions of low chrome diopside, with Cr_2O_3 contents ranging from 0.46% to 1.02%. Orthopyroxenes are compositionally enstatites. Plagioclase compositions range from An57-65 (Klasner et al., 1979).

7.3.4 Pyroxenite

In drill hole YD01-01 (Eagle East), near the lower contact, the core alternates rapidly between intervals of coarse-grained peridotite and a much finer-grained, less magnetic rock. Similar patterns of alternating intervals of coarse-grained peridotite and fine-grained rock were observed near the contacts in mineralized portions of Eagle. Subsequent drilling indicates that some, or possibly all, of the fine-grained intervals may be xenoliths of an earlier phase(s) of the intrusion that have been mechanically incorporated into the peridotite. A similar fine-grained rock has also been noted along the contacts with the surrounding sediments in both intrusions. Primary mineralogy is difficult to infer in these fine-grained intervals. Magnetic susceptibility was often used as an aid in estimating original primary olivine content. This assumes that the bulk of the magnetite formed during the serpentinization of primary olivine. When the primary mineralogy is not obvious, core with relatively low magnetic susceptibility is often assumed to be pyroxenite. In thin section, most primary silicates have been altered to secondary assemblages. Based on relict textures, estimated original olivine contents ranged from 3% to 10% (Jago, 2002). This is significantly less than the peridotites and consistent with their low magnetic susceptibility. Pyroxenes were the predominant primary mineral phase in these sections. In one sample, however, feldspar was estimated at 35% to 40%, indicating that possible compositions for pyroxenite might range from pyroxenite to olivine metagabbro. A number of thin dikes, ranging from less than a meter to a few meters in width, have been noted in drilling in close proximity to the Eagle intrusions. Little is known about the extent, orientation, or composition of these predominantly fine-grained dikes. One thin section, taken from a thin dike along the margin of the massive sulfide intersection in YD02-02, was described as being re-crystallized (hornfelsed) and comprises secondary minerals with no obvious primary mineralogy preserved (Jago, 2002). This suggests that at least some dikes predate the main stages of intrusion of the peridotite and massive sulfides. High chrome values (>500 parts per million [ppm]) for some of these dikes suggest that they are related to the other picritic dikes in the Baraga Basin. Thin dikes have been noted at the contacts of massive sulfide horizons peripheral to both Eagle intrusions. These dikes may have formed barriers, or zones of weakness, that played a role in localizing later massive sulfide mineralization external to the main intrusions. Drilling identified two larger gabbroic dikes to the immediate south of the Eagle intrusion. The dikes correspond with a paired, linear magnetic low and magnetic high that can be traced for several kilometers. The dikes have traces of pyrite and chalcopyrite, but very low values of chrome and nickel. They resemble other gabbroic dikes of the Baraga-Marquette dike swarm.

7.3.5 Structure

In general, there is no significant post-mineralization structural deformation affecting the Eagle and Eagle East systems. One post-mineralization fault has been identified at the west end of the Eagle East mineralized zone, and has been intruded by a gabbro dike. This dike/fault offsets the east side of the conduit approximately 20 m north and appears to spatially coincide with the western terminus of the massive sulfide zone. The structural deformation prior to the emplacement of the Eagle and Eagle East intrusions is relatively complex, resulting from multiple island arc accretion episodes during the Penokean Orogeny. This results in the sedimentary basin being folded into a gently eastward plunging syncline. The sediments have a strong foliation and local isoclinal folding, which results in significant deviation in drill holes. In general, the sedimentary rocks immediately adjacent to Eagle show a regular bedding orientation with an average strike of 340°, dipping 15° to the east. Foliation, like bedding, is consistent with an average orientation striking 100° and dipping 40° to 45° to the south, similar to the measurements from the rest of the Baraga Basin. Both open and closed joints show a broad range of orientations with no dominant set. Most open joints strike east-southeast parallel to the trend of the Eagle peridotite and have flat to moderate dips both north and south. A second preferred orientation strikes north-northeast, with very steep to vertical dips both east and west. Cemented joints are dominantly flat lying but show a similar, very broad range of orientations. Cemented joints (typically serpentinite) within massive sulfides preferentially strike at 065° and dip from 0° to 60° to the southeast. Within peridotite, they preferentially strike at approximately 280° and dip from 0° to 70° to the north.

7.3.6 Deformation Zone

A regionally consistent 1 m thick horizontal zone of mottled quartz veining is present throughout the drilled area of the Baraga Basin. This zone is not conformable with bedding and is likely related to ancient thrust faulting, although this interpretation is speculative.

7.3.7 Alteration

All samples of the two intrusions show evidence of significant but variable degrees of alteration. Alteration includes serpentinization of olivine, alteration of pyroxene to secondary amphibole, chloritization of amphibole, chloritization and saussuritization of plagioclase, and minor talc-carbonate alteration (Klasner et al., 1979). There is no hydrothermal alteration halo around the peridotite; however, there is a large bleaching zone above and lateral to the deep gabbro intrusive. Thermal alteration in the form of hornfelsed sediments occurs within ten meters of the intrusive units.

7.4 Mineralization

Eagle and Eagle East are part of the same ultramafic intrusive complex, and both host high-grade primary magmatic nickel-copper-sulfide mineralization. Mineralization styles are similar at Eagle and Eagle East, consisting of ovoid to pipe-like bodies of mineralized peridotite with concentrations of sulfide mineralization along the base of the intrusion, resulting in the accumulation of semi-massive sulfide, and a central core zone of massive sulfide. Two types of economic mineralization are found in Eagle and Eagle East: semi-massive sulfides and massive sulfides. Disseminated mineralization is also encountered in the peridotite intrusive, with some of the mineralized peridotite being potentially economic based on forecasted nickel and copper prices.

7.4.1 Eagle

The intrusion hosting Eagle is elongated east-west with a maximum length of 480 m and a maximum width of approximately 100 m near the surface. The intrusion narrows to approximately 10 m wide at the limit of drilling, 290 m below surface (145 m RL). The sulfide bodies within the intrusion comprise an irregular mass broadly aligned with the strike and dip of an ovoid dilatant zone occupied by the peridotite. The bodies subtend a volume measuring 330 m in strike length by 270 m vertically, abruptly terminating on the west and tapering to the east with a maximum thickness in the middle of approximately 135 m. At the east and west ends of this volume are two bodies of semi-massive sulfides (SMSU), termed SMSUE and SMSUW, respectively. The SMSUW is somewhat pipe-like in shape, oriented vertically within the peridotite. The SMSUE is more tabular in aspect, extending eastwards from the central core of the deposit, again, at roughly the same orientation as the host intrusion. Although these units are distinguished from one another for the purposes of geological interpretation and Mineral Resource estimation, the SMSU bodies do appear to be a single contiguous mass.

A single irregular body of massive sulfide (MSU) occupies the central portion of the deposit, more or less between the SMSUE and SMSUW. The MSU extends outside of the semi-massive bodies, and in many cases has intruded into the sedimentary rocks adjacent to the peridotite. This has resulted in several flat, sill-like protuberances at the margin of the deposit.

7.4.2 Eagle East and Keel

Eagle East has identified nickel and copper-rich massive and semi-massive sulfide mineralization concentrated along a horizontal conduit at the bottom of the main Eagle East intrusion. Prior to the exploration program initiated in 2013, no semi-massive sulfide had been found at Eagle East, and MSU lenses of only one to two meters have been found along the 45° plunging keel of the intrusion. The Eagle East intrusion can be categorized into two components: the funnel-shaped upper peridotite intrusion outlined prior to 2013, referred to as the Keel, and the sub-horizontal conduit zone defined since 2013.

The conduit zone contains massive sulfide and semi-massive sulfide similar to Eagle, whereas the main intrusion consists of barren peridotite with low-grade disseminated and thin massive sulfides which make up the Keel. The conduit exploration program has identified a 500 m long horizontal section of the Eagle East feeder conduit, where the peridotite conduit is cored by semi-massive sulfide with massive sulfide accumulations at its base, as well as massive sulfide sills into the sediments. The conduit is up to 30 m thick, and its vertical extent is in the order of 75 m.

The Keel host rock is peridotite, with mineralization occurring as disseminated sulfide blebs, measuring 1-20mm in diameter. Modal sulfide percentages increase as the lower contact is reached. In places, there is a basal massive sulfide along the intrusive/sedimentary contact, measuring 0.5 m to 1.5 m thick.

7.4.3 Mineralizing System

Sulfides are deposited as dense droplets in the primary magma due to decreased flow rate in the magma, or a change from laminar to turbulent flow due to changes in the conduit geometry. Multiple pulses likely occur in the same plumbing system, resulting in three discrete mineralization types, which typically have hard contacts. The mineralizing intrusion is Mineralized Peridotite (MPER), which transports sulfides within large volumes of magma, and in this way is able to transport significant quantities of dense sulfides upward through the crust in a diluted form. This results in the conduits between mineralized zones consisting of barren peridotite or weakly mineralized peridotite, such as in the subvertical throat where the primarily horizontal Eagle East deposit transitions into the Keel.

Typical mineralization zoning at both Eagle and Eagle East consists of a mineralized peridotite conduit with a core of SMSU and a base of crosscutting MSU that also sills out into the surrounding sediments (Figure 7.4). The massive sulfide remains liquid for a significant time, so it can crosscut other units after emplacement is complete.

7.4.4 Metal Distribution

Limited petrography and Quantitative Evaluation of Materials by Scanning Electron Microscopy (QEMSCAN) work indicates that most of the nickel is in pentlandite, with a small portion in millerite group minerals and secondary violarite. The majority of pentlandite occurs in granular form with less than 1% to 2% as flame or exsolution lamellae.

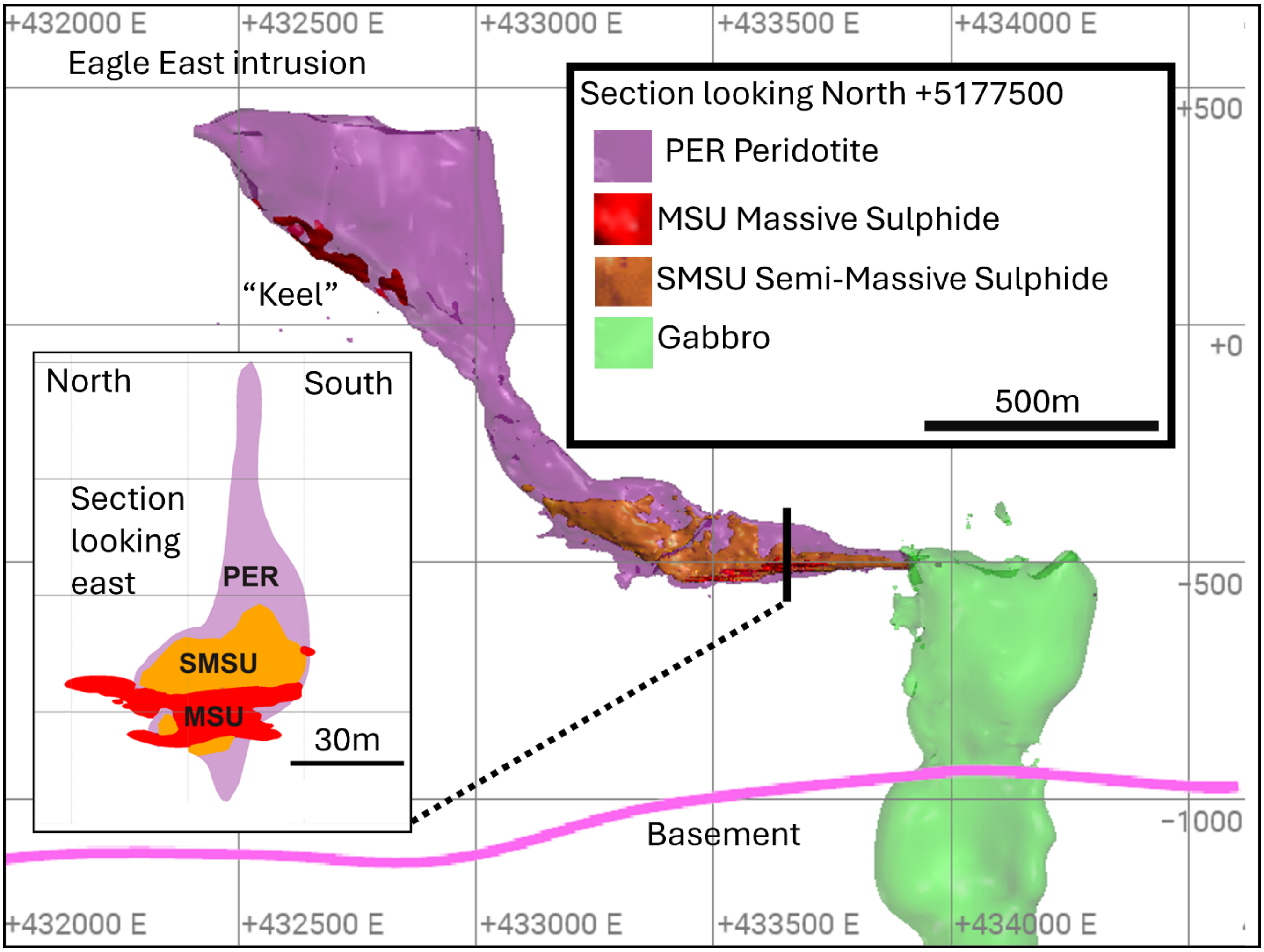
Copper is primarily in chalcopyrite with lesser secondary cubanite. Chalcopyrite occurs as anhedral inclusions in pyrrhotite and as coarse patches with granular pentlandite around pyrrhotite grains. Chalcopyrite also occurs as veins that locally crosscut SMSU and sedimentary units; however, these are volumetrically minor.

The distribution of platinum group metals (PGM), gold, and cobalt is still poorly understood, but assay and metallurgical test correlations indicate that the cobalt is associated with the pyrrhotite/pentlandite. PGMs and gold appear to be related to late-stage veining/intrusion and tend to be most abundant in areas with chalcopyrite enrichment.

Eagle East is observed to be significantly higher in grade for both precious and base metals than Eagle, with the exception of cobalt. Average nickel and copper grades are in the order of 60% higher at Eagle East compared to Eagle. Gold averages approximately 87% higher, while platinum and palladium are well over double. While silver is not reported in the Mineral Resource estimate for Eagle, silver is present at Eagle in roughly the same abundance as at Eagle East.

7.4.5 Peridotite (PER) And Mineralized Peridotite (MPER)

The mineralized intrusion is sulfur-saturated PER, which carries disseminated sulfide blebs in abundances ranging from trace to 25%. MPER (Figure 7.5) as a discrete lithological unit has never been economic at Eagle or Eagle East; however, the disseminated sulfide blebs are of very high metal tenor, which was an important factor in the decision to follow Eagle East to depth. The accumulation of high tenor droplets results in high-grade massive sulfide zones.



*Source: Eagle Mine, 2023

Figure 7.4: Typical Zoning of Peridotite Massive Sulfide, and Semi-Massive Sulfide

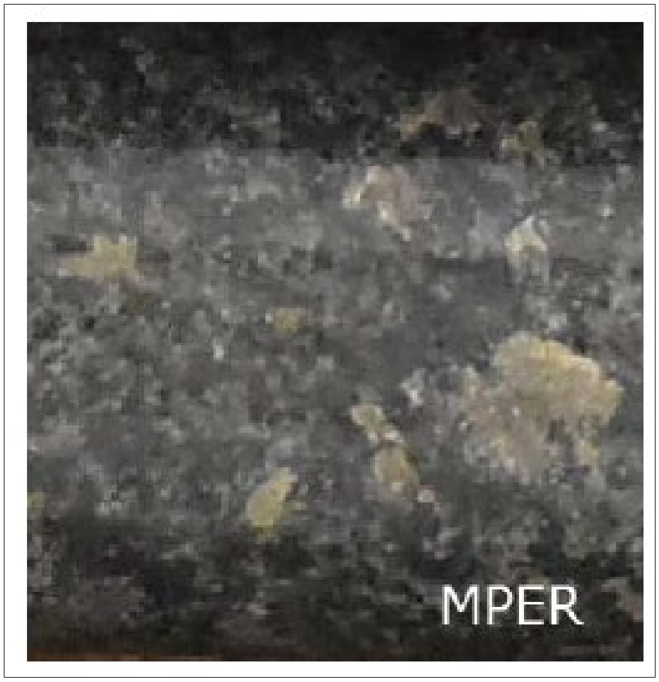


Figure 7.5: Mineralized Peridotite

Scattered blebs of sulfide are found throughout the peridotite sections of both Eagle intrusions. At Eagle, zones of abundant disseminated sulfide (3% to 15%) are localized along the margins of the intrusions, above and below the Upper Sulfide Zone and above the Lower Sulfide Zone. Cloud-like zones of low-grade, disseminated sulfides occur throughout the eastern portion of Eagle, concentrated on intrusion margins and commonly bordering possible rafts of fine-grained pyroxenite.

The transition from peridotite with only rare blebs of sulfide, to peridotite with several percent sulfides, typically happens over less than one meter. The geological control for this boundary is not obvious. The boundary of the disseminated mineralization, for modeling purposes, is based on metal value, not sulfide content.

7.4.6 Massive Sulfide (MSU)

MSU shows considerable variation in composition. Chalcopyrite content can vary from less than 10% to more than 50%. In most of the MSU (Figure 7.6), pyrrhotite is the dominant sulfide. Pyrrhotite occurs as coarse, anhedral grains with minor pentlandite and chalcopyrite.

Pentlandite typically occurs as discrete crystals up to five millimeters in diameter.

Chalcopyrite typically forms rings around the pyrrhotite crystals, except in the high copper massive sulfide zones where chalcopyrite is volumetrically dominant.

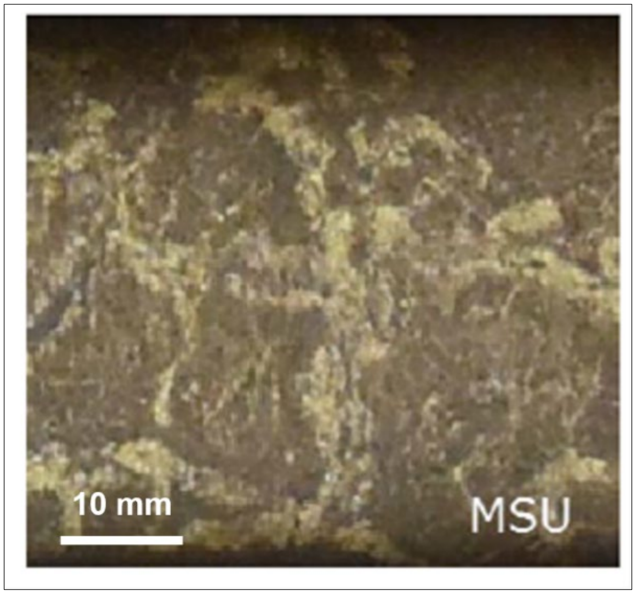


Figure 7.6: Massive Sulfide

7.4.7 Semi-Massive Sulfide (SMSU)

SMSU occurs throughout the core of the Eagle East conduit zone. The SMSU comprises zones of 30% to 50% sulfide that forms a net-textured matrix enclosing altered olivine and pyroxene.

Disseminated mineralization generally increases toward zones of SMSU (Figure 7.7). However, the transition between the disseminated mineralization and SMSU is typically abrupt, with sulfide contents increasing from 5% to 10% to over 40% over a distance of less than 1 m.

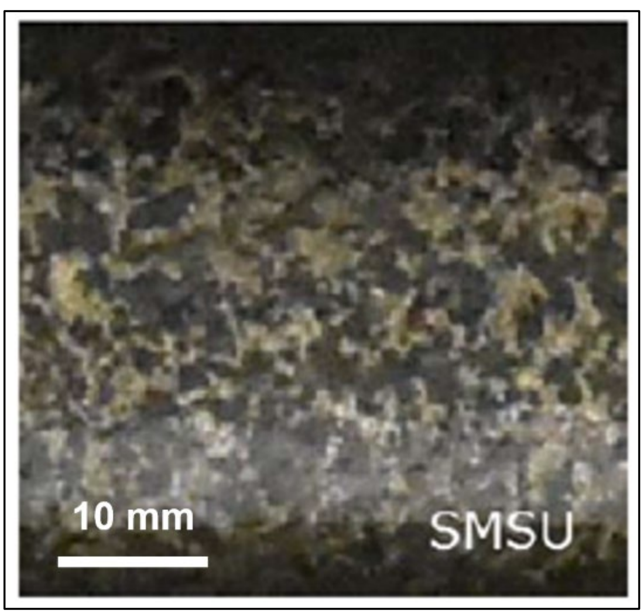


Figure 7.7: Semi-Massive Sulfide

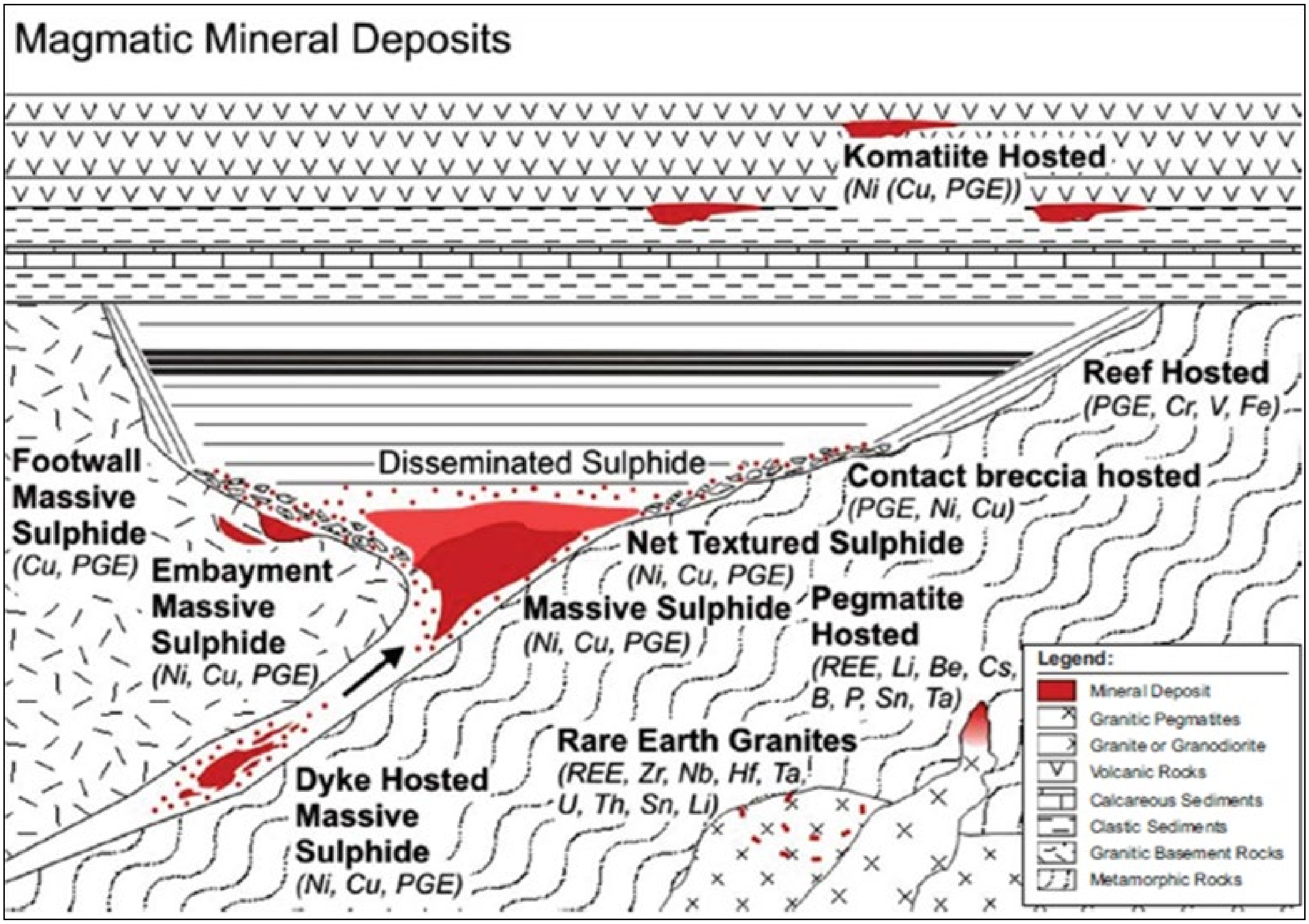
8. Deposit Types

Magmatic sulfide deposits containing nickel and copper, with or without PGMs, account for approximately 60% of the world's nickel production and are active exploration targets in the United States and elsewhere. On the basis of their principal metal production, magmatic sulfide deposits in mafic rocks can be divided into sulfide-rich and sulfide-poor. Sulfide-rich deposits typically have 10% to 90% sulfide minerals and have economic value primarily because of their nickel and copper contents. Sulfide-poor deposits typically contain 0.5% to 5% sulfide minerals and are exploited principally for Platinum Group Metals (PGM).

The Eagle and Eagle East deposits are sulfide-rich and high-grade magmatic sulfide accumulations containing nickel-copper mineralization and minor amounts of cobalt and PGMs. The economic minerals associated with these deposits are predominantly pentlandite and chalcopyrite.

The mineralization process common to all primary magmatic sulfide deposits consists of: 1) Metal-rich ultramafic magma intruding into the crust, typically in an extensional environment; 2) Sulphur saturation through geochemical contamination by crustal rocks resulting in primary sulfide droplets forming; 3) Metal enrichment of sulfides by interaction with large volumes of subsequent magma flow; and 4) Deposition of sulfides by density settling where magma flow slows due to structural traps or major changes in the geometry of the plumbing system (going from a small conduit to a large chamber, etc.).

Several varieties of this deposit type occur within the primary magmatic sulfide model, ranging from komatiite lava flow deposits like Raglan, to meteor impact-triggered partial melting like Sudbury, to conduit-style mineralization like Eagle and Voisey's Bay, and layered mafic complex mineralization like the Duluth complex. Figure 8.1 shows idealized representations of these deposit types.



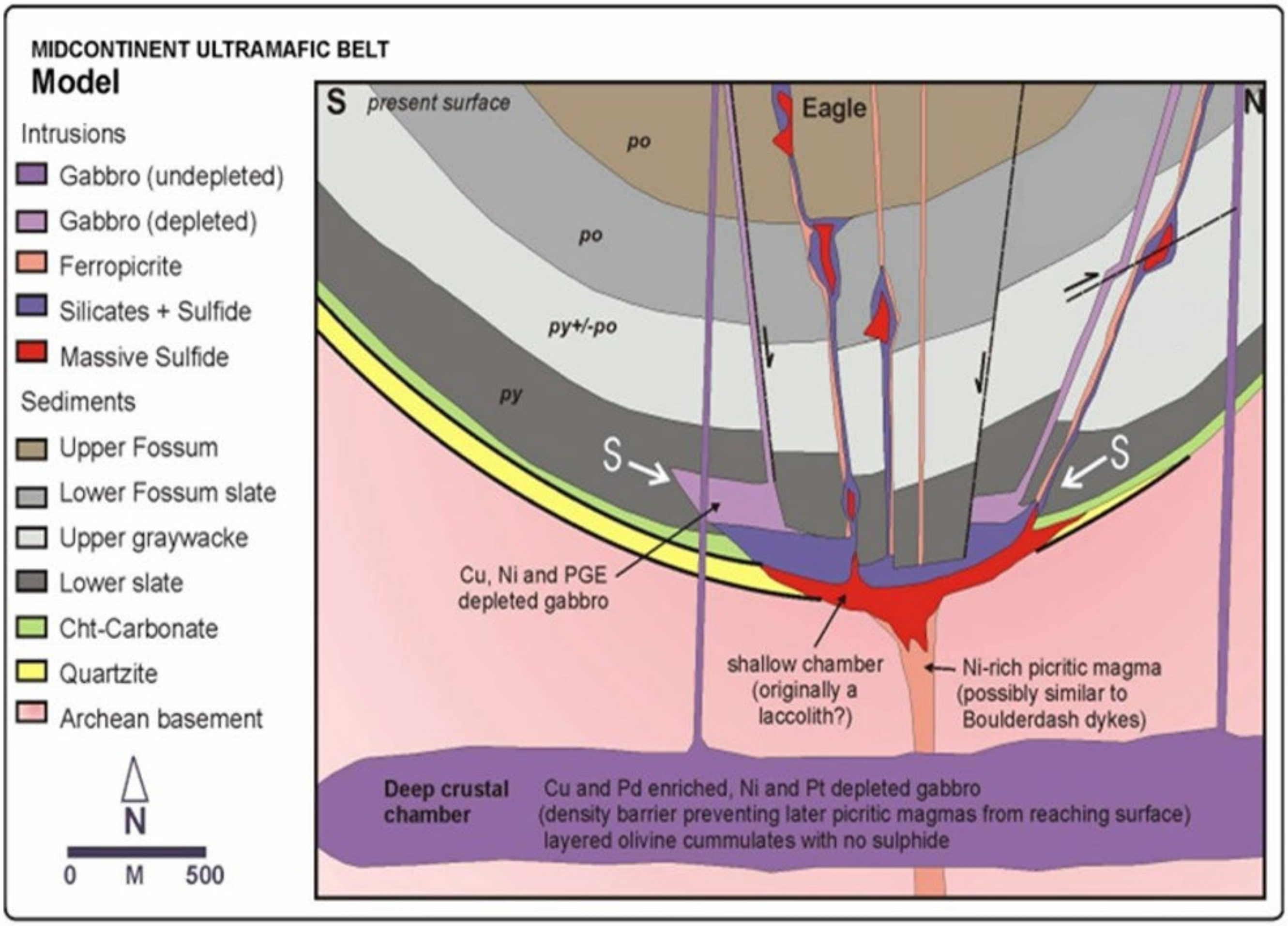
*Source:Eagle Mine, 2023

Figure 8.1: Types of Primary Magmatic Sulfide Deposits

The magmatic sulfide model focuses on deposits hosted by small to medium-sized mafic and/or ultramafic dikes, sills, and conduit-shaped “chonoliths” that are related to picrite and tholeiitic basalt magmatic systems generally emplaced in continental settings as a component of Large Igneous Provinces (LIPs). World-class examples (those containing greater than one million tonnes Ni) of this deposit type include deposits at Noril’sk-Talnakh (Russia), Jinchuan (China), Pechenga (Russia), Voisey’s Bay (Canada), and Kabanga (Tanzania).

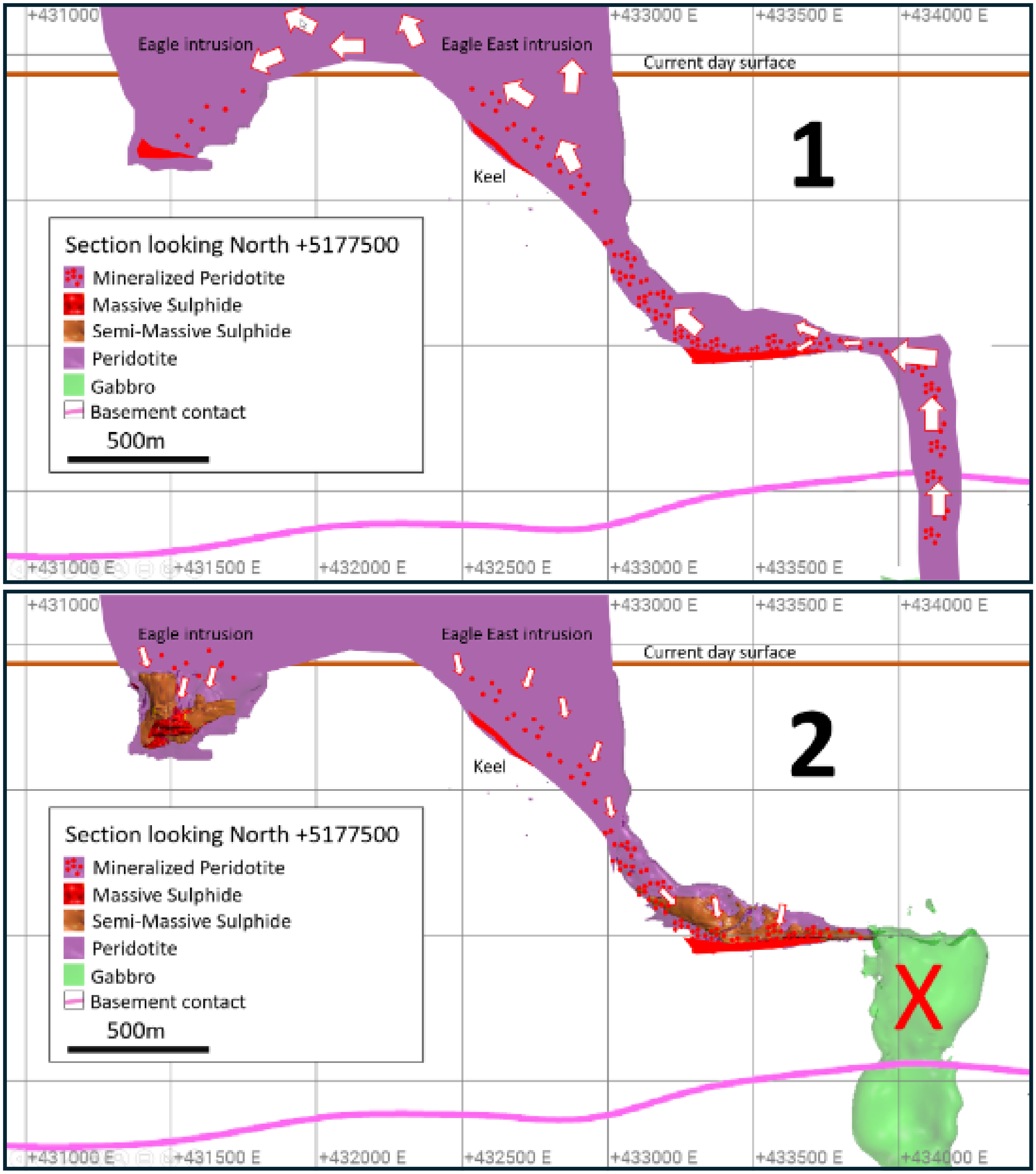
At Eagle, the conceptual model is that of a series of magma conduits connecting several larger magma chambers (Figure 8.2), and exploring for high grade deposits is reliant on tracing the conduits from one chamber to the next. The model has proven successful with the discovery of the Eagle East deposit, which was discovered as the result of directional drilling to follow the conduit from the much larger and lower-grade Eagle East peridotite. Drilling between 2016 and 2018 defined a large gabbroic intrusion that truncates the Eagle East peridotite at depth (marked with the red X in Figure 8.3) and is interpreted to be a younger intrusion that occupies the same structural plumbing as Eagle East, locally obliterating the peridotite intrusion.

The likely depositional process for the formation of the Eagle East deposit is that mineralized peridotite moving upward along a vertical intersection of mantle-tapping structures (now occupied by the gabbro intrusion) carried disseminated sulfide droplets in a high-volume magma flow, and the sulfides were dropped from the magma when they exited the small 90-degree bend in the magma conduit at the east end of Eagle East (Figure 8.3). This likely resulted in a significant pressure and velocity gradient, resulting in high velocity magma slowing down significantly in the horizontal portion of the conduit, dropping dense sulfides. Additionally, back-draining of sulfides from higher in the intrusion and ponding of sulfides in the horizontal section is likely to be a contributing factor to the formation of high-grade massive sulfide and semi-massive sulfide.



*Source: Eagle Mine, 2023

Figure 8.2: Genetic Model for Eagle Type Deposit Formation



*Source: Eagle Mine, 2023

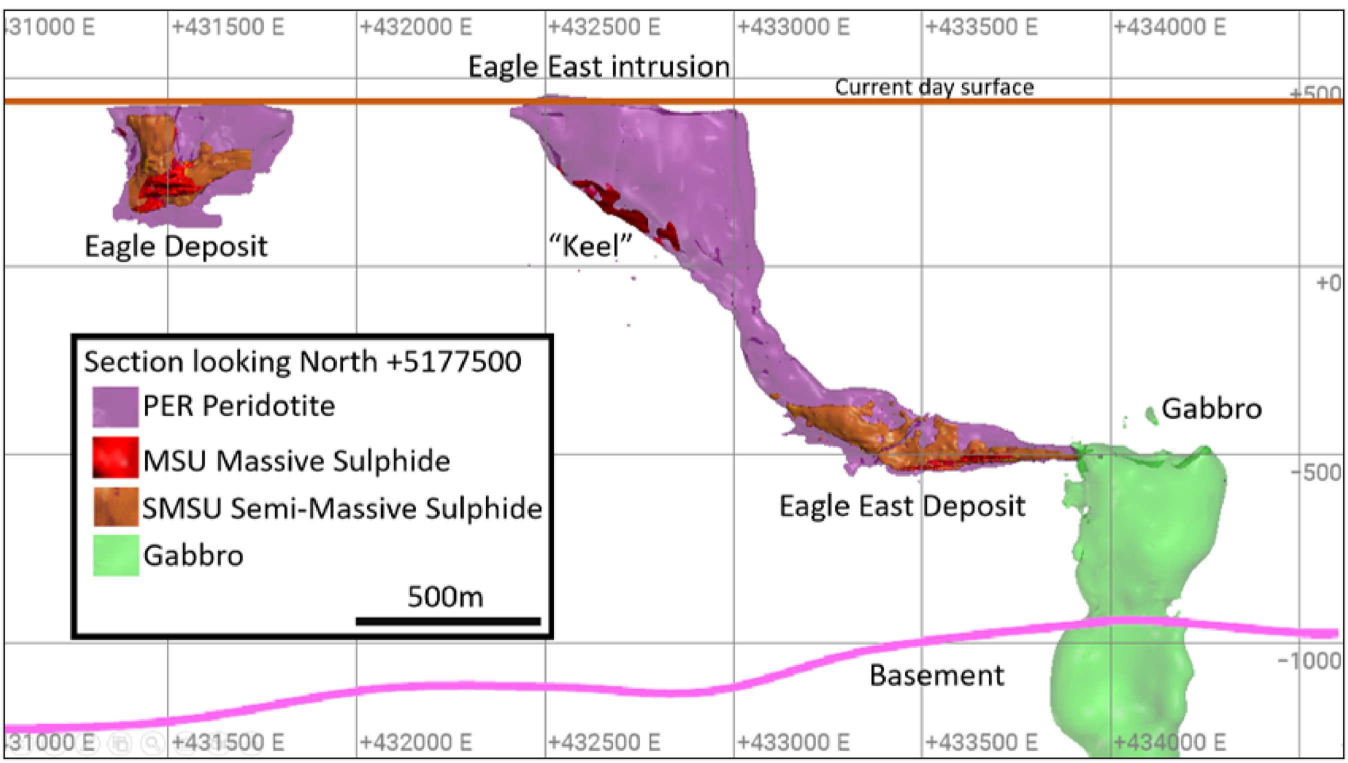
Figure 8.3: Eagle East Deposit Model

9. Exploration

Talon acquired Eagle Mine on January 9, 2026, and has not conducted any exploration programs since the acquisition.

Past exploration activities at Eagle have included geological mapping, geochemistry (indicator mineral sampling and Mobile Metal Ion (MMI) studies from basal tills, dike geochemistry, sulphur isotype studies, QEMSCAN studies), and geophysics (airborne, surface, and underground borehole electromagnetics, resistivity, and gravity). The main and most successful exploration tool has been diamond drilling in combination with a very robust and predictive deposit model (Figure 9.1).

Historical exploration conducted by Rio Tinto (KEX) is described in Section 6, History. LMC acquired Eagle in 2013 and subsequently completed construction and brought Eagle into production in 2014. Eagle Mine LLC continued with near mine exploration with a focus on extending mine life. Using the conduit model, the most direct and expedient exploration target was to follow the mineralized peridotite conduit at Eagle East to depth with directional drilling. With Eagle as a model, the Eagle East conduit was traced downward to a location where the conduit flattened to horizontal and high metal tenor sulfide droplets had settled to the base of the conduit, resulting in the discovery of the Eagle East deposit in 2015. Mineralization in Eagle East is terminated at depth to the east due to a large gabbro intrusion along the mineralized conduit.



*Source: Eagle Mine, 2023

Figure 9.1: Eagle and Eagle East Long Section (Facing North)

10. Drilling

All exploration and Mineral Resource definition drilling at Eagle and Eagle East has been conducted by diamond core drilling. Sonic drilling was historically conducted to test depth to bedrock and define lithologies at the paleo-bedrock surface. Since 2013, Eagle Mine LLC has carried out drilling at Eagle and Eagle East (including the Keel). Seven surface drill rigs were utilized in 2016 during the Eagle East resource drilling campaign, reducing to four surface rigs through August of 2019. The drilling was primarily to investigate controlling structures for the Eagle East mineralization and to look for extensions of the Eagle East conduit.

Total drilling at Eagle and Eagle East comprises 447,696 m from 1,516 total holes (surface and underground) drilled between 2001 and 2024. No drilling was conducted in 2025. Note that not all holes listed in Table 10.1 and Table 10.2 were included in the Mineral Resource estimates. A plan view in Figure 10.1 shows the locations of those holes that were used for modeling and resource estimation.

Table 10.1: Drilling Summary Eagle Mine

Table 10-1 DRILLING SUMMARY - EAGLE MINE
Eagle Mine

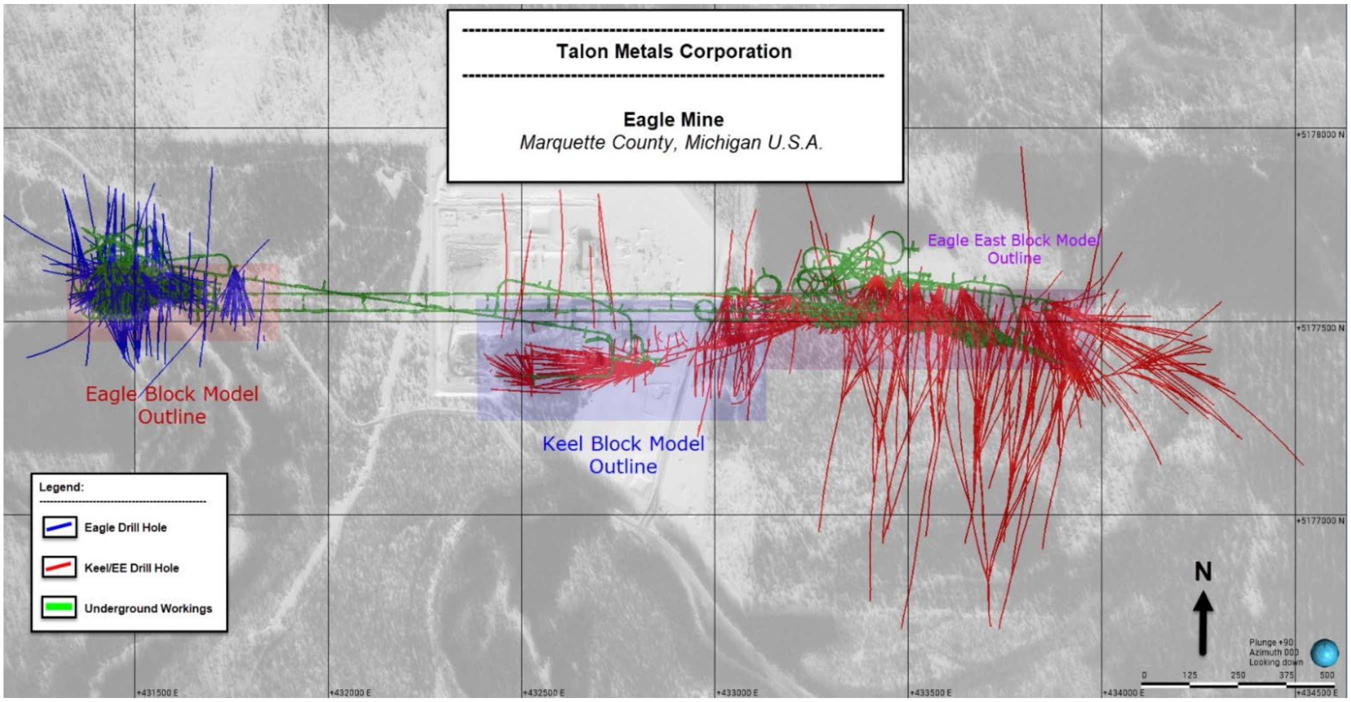
	Surface		Underground		Total	
Year	**Holes**	**Metres**	**Holes**	**Metres**	**Holes**	**Metres**
2001	4	667	-	-	4	667
2002	18	5,496	-	-	18	5,496
2003	14	3,781	-	-	14	3,781
2004	45	11,947	-	-	45	11,947
2005	17	4,262	-	-	17	4,262
2006	7	3,083	-	-	7	3,083
2007	20	7,911	-	-	20	7,911
2008	8	8,737	-	-	8	8,737
2010	3	1,049	-	-	3	1,049
2011	13	6,650	-	-	13	6,650
2012	74	40,586	7	1,337	81	41,923
2013	6	2,911	42	7,233	48	10,144
2014	2	567	56	5,269	58	5,836
2015	3	980	108	3,334	111	4,314
2016	10	5,677	89	5,505	99	11,182
2017	2	1,676	52	5,226	54	6,902
2018	16	13,279	5	420	21	13,699
2019	7	4,753	2	47	9	4,800
2021	-	-	25	1,484	25	1,484
2022			-	-	-	-
2023			26	3,929	26	3,929
2024			9	744	9	744
Total	**269**	**124,012**	**421**	**34,528**	**690**	**158,540**

Source: Talon, 2026

Table 10.2: Drilling Summary – Eagle East and Keel

Table 10-2 DRILLING SUMMARY - EAGLE EAST AND KEEL PROJECTS
Eagle Mine

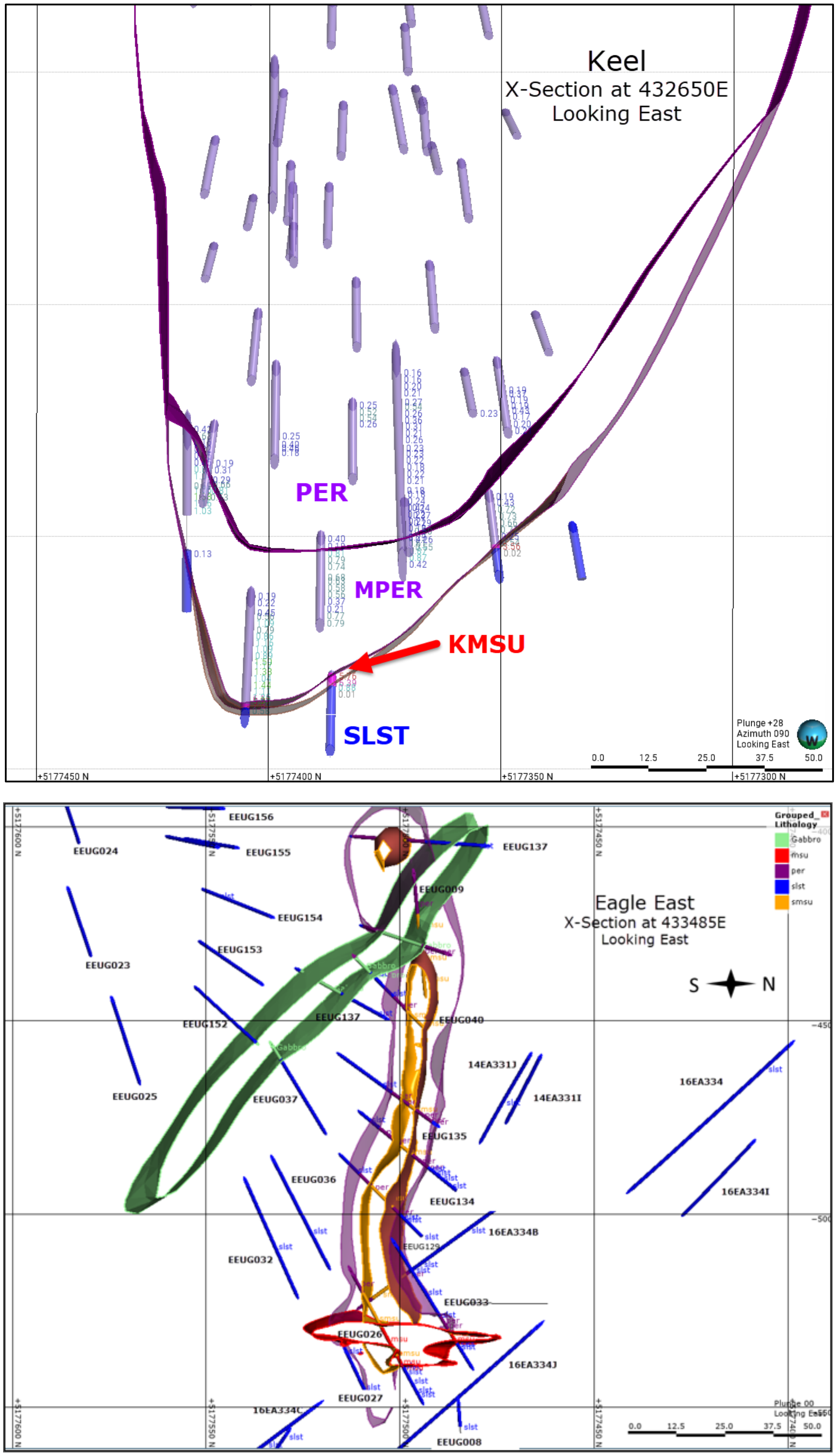
	Surface		Underground		Total	
Year	Holes	Metres	Holes	Metres	Holes	Metres
1995	4	894	-	-	4	894
2001	3	594	-	-	3	594
2002	10	3,540	-	-	10	3,540
2003	1	547	-	-	1	547
2004	3	1,598	-	-	3	1,598
2005	3	3,947	-	-	3	3,947
2006	30	9,337	-	-	30	9,337
2007	19	7,375	-	-	19	7,375
2008	29	16,997	-	-	29	16,997
2010	8	3,649	-	-	8	3,649
2011	14	8,302	-	-	14	8,302
2021	3	4,608		-	3	4,608
2013	3	1,175	-	-	3	1,175
2014	8	3,683	9	3,237	17	6,920
2015	27	12,513	-	-	27	12,513
2016	75	41,865	-	-	75	41,865
2017	49	39,457	-	-	49	39,457
2018	24	25,864	47	12,381	71	38,245
2019	4	1,556	206	39,156	210	40,712
2020	-	-	43	7,378	43	7,378
2021	-	-	30	8,501	30	8,501
2022	-	-	92	17,932	92	17,932
2023	-	-	35	4,868	35	4,868
2024	-	-	47	8,202	47	8,202
Total	**317**	**187,501**	**509**	**101,655**	**826**	**289,156**



*Source: Eagle Mine, 2026

Figure 10.1: Drill Hole Locations (showing only holes used for Mineral Resource Estimation)

See Figure 10.2 for section displaying drilling-associated geological interpretation.



*Source: Eagle Mine, 2023

Figure 10.2: Typical Diamond Drill Cross-Section Displaying Lithology in Eagle East

10.1 Diamond Drilling

At Eagle, the surface drilling was initially conducted on 25-m intervals with pierce-points at approximately 20 m to 25 m spacing along with drill hole fans on 25 m and 12 m centers. The overall drill hole spacing is not uniform owing to the orientation of the mineralized body and the environmental constraints (trees, boulders, water, etc.) on collar placement.

Underground preliminary development drilling, which began in 2012, is generally completed at a nominal 20 m spacing to achieve a Measured category for the resource model. Holes are not typically aligned along cross-section planes, owing to the necessity of fan holes from relatively few stations. The style of mineralization is such that it is not necessary for the drill holes to be rigorously oriented perpendicular to the overall trend of the mineralization. The deposit is traversed in a wide range of directions in such a fashion that the samples, taken as a whole, should be representative of the grades of the mineralization.

Both surface and underground drilling have been carried out by contract drillers. The most recent contractors have been Boart Longyear (surface) and First Drilling (underground). Surface drilling programs employed truck-mounted LF90 and LF230 rigs (Boart Longyear). Underground drilling is conducted using skid-mounted U8 rigs.

Drilling includes HQ (6.35 cm core diameter) and NQ (4.76 cm core diameter) sized core. Initially, limited wedge work and directional drilling were undertaken at Eagle to obtain twinned hole data and steer holes to desired target points. In 2013, directional drilling was used for precision drilling of a few small targets, and the use of directional drilling and wedging became routine practice as the precision requirements increased to follow the Eagle East conduit to depth. Directional drilling was routinely employed on all surface rigs between 2016 and 2019.

Directional drilling (using DeviDrill) has been utilized by a Norwegian contractor, Devico (who were permanently based on site), to drill deflection holes for multiple intersections out of a single hole. The Devico directional drilling tool was used to guide surface-drilled holes to targets and maintain even grid spacing. During the directional drilling process, parts of the hole are surveyed independently by the Devico sub-contractors, providing additional verification of the FLEXIT MultiSmart multi-shot tool survey data. All holes are gyro surveyed upon completion.

10.2 Core Recovery

Core recovery is recorded in the geotechnical logs. Generally, recovery is considered excellent at Eagle when advancing in bedrock. Recovery is poor to zero in the glacial tills during core drilling. Where till geology is required, drilling was completed using a sonic rig with a resulting recovery of close to 100%.

10.3 Surveys

10.3.1 Survey Grids

UTM coordinates based on the NAD83 (Zone 16N) datum are used at Eagle. The 0 RL elevation is based on mean sea level (MSL).

10.3.2 Diamond Drilling

Diamond drilling was planned by the exploration department using Vulcan 3D geological modeling software and Seequent Leapfrog 3D geological modeling software.

Surface collars were located initially by handheld GPS and oriented by a Brunton compass, then surveyed by contract surveyors. From 2003 to 2019, the collars were surveyed by a local registered land surveyor who also established several control points on the property.

KEMC reported that some of the 2002 collars were lost at the time of this survey. The onsite staff made their best estimate as to the locations of these collars. Accuracy for the surveyed locations of these collars is reported to be within two meters.

Underground diamond drill collars are initially marked by the Eagle Mine LLC Surveyors or Eagle Mine LLC geology personnel utilizing a Leica TS-14 total station. Foresight and backsight survey plugs are installed in the drift walls and marked with yellow paint, or the drill rig is directly sighted in with the total station. After completion of drilling, the hole collar location is surveyed.

Downhole surveys were carried out by a variety of instruments throughout the exploration history of the property. The survey methods and dates are listed below:

- 2001: Sperry Sun single-shot camera.
- 2001 and 2002: Sperry-Sun gyroscopic survey tool.
- 2002: Flexit MultiSmart multi-shot tool.
- 2003 to 2013: IDS gyroscopic survey tool and rate gyros plus Flexit surveys.
- 2014 to 2023: Reflex gyroscopic tool.
- 2024: Reflex gyroscopic tool and Veracio TruShot.

Downhole surveys are taken at three-meter intervals for underground drilling and three-meter intervals on average for surface drilling.

The collar and downhole surveys, as reported, have been carried out in a manner that is consistent with industry-standard methods.

10.4 Core Handling Protocols

Core boxes are labeled by the drillers with the box and hole number. The core is removed from the tube, washed, and placed in the box. Core boxes are waxed cardboard. Footage blocks are placed at the end of the run. Breaks are marked with an X with a red pencil. For oriented core, the driller is responsible for orienting the core to the EzyMark pins, recording the oriented core survey information, and marking a line on the pin block and the core. The pin block is placed in the core box. Alternatively, the ACT tool is used. In the case of the ACT tool, the driller is responsible for marking the ACT core orientation mark on the core and recording associated information.

Drill core is collected by Eagle Mine LLC personnel and delivered to the logging and sampling facility located at Eagle Mine. Core is stacked on pallets up to a maximum of 60 boxes per pallet. The drill core is in the custody of

Eagle Mine LLC personnel or the Company designates at all times. The drill sites and core storage areas are generally secure and supervised continuously.

10.5 Logging

For logging, the core is transferred to the logging tables. All data is captured via laptop computers and stored in an acQuire database. Footage blocks are converted to meters, and the core is inspected and re-oriented to fit together. Open and cemented joint data is recorded, and large-scale structures are logged. The core is photographed, both wet and dry, with a digital camera. Sample locations are marked for point load tests and density measurements. Point load tests are taken every five meters down the hole for the first 130 m, and every 15 m thereafter. Bulk density measurements are made every 15 m for the first 130 m, and every 20 m from there on. These specimens consist of a 15 cm length of whole core. The measurements are made by taking the ratio of the weight of a core specimen in air to the difference between the dry and submerged weights.

Other features deemed as “Not Required” in the protocol documentation may also be logged and include magnetic susceptibility, micro-defects, open fractures/joints, and cemented joints. Breaks in the core made by the drillers, and marked as such, are ignored. Joint angles to the core axis are recorded, as are the roughness, alteration, and infill material. Cemented joints must be at least one millimeter thick and cross the entire core axis to be included. Geotechnical data, comprising recovery, intact rock strength, number of joints (open and cemented), and number of joint sets, are logged for all intervals and entered into acQuire.

Major structures are defined as those encompassing a core length of at least 50 cm. The depth, interval length, and character (e.g., gouged, sheared, broken, or jointed) are recorded. Domain intervals for the geotechnical data are the run lengths, or major lithological or structural breaks. No oriented core was collected between 2016 and 2026.

Oriented core is placed in a v-rail, aligned to the marks, and a reference line is drawn longitudinally along the core. Angles of structural features to both the core axis and the reference line are then measured and recorded in the database. Historically, the geotechnical data was validated by plotting on strip logs and visually inspecting for missing intervals or unusual data. Errors were corrected by referring to the core photographs.

Geology logging includes the principal rock type, formation, texture, color, gross mineralogy, structures, and alteration. The data entry fields in the acQuire software are configured to restrict the entries to a specific set of codes for consistency in the logs.

Alteration is logged for both type and intensity, which is denoted by a scale from one (weak) to four (pervasive). Mineralization type is recorded, as are visual estimates of the average and maximum percent abundance. Since the structural information is captured in some detail during the geotechnical logging, the structural logging for the lithological table tends to be less rigorous.

Validation of the geological logging includes the following:

- Running acQuire validation scripts and reports on the data to check for missing and/or overlapping intervals.
- Load the data into Vulcan or Oasis and run the validation utilities in those packages.
- Compare to the geotechnical logs.

After logging and sampling, the core is stored in either the warehouse in Negaunee, Michigan, or in a warehouse in Sawyer, Michigan. Figure 10.3 depicts a core handling and logging flow sheet, as designed in 2012, which is nearly identical to the protocols employed at present. In the QP's opinion, the core logging protocols used at Eagle meet industry standards.

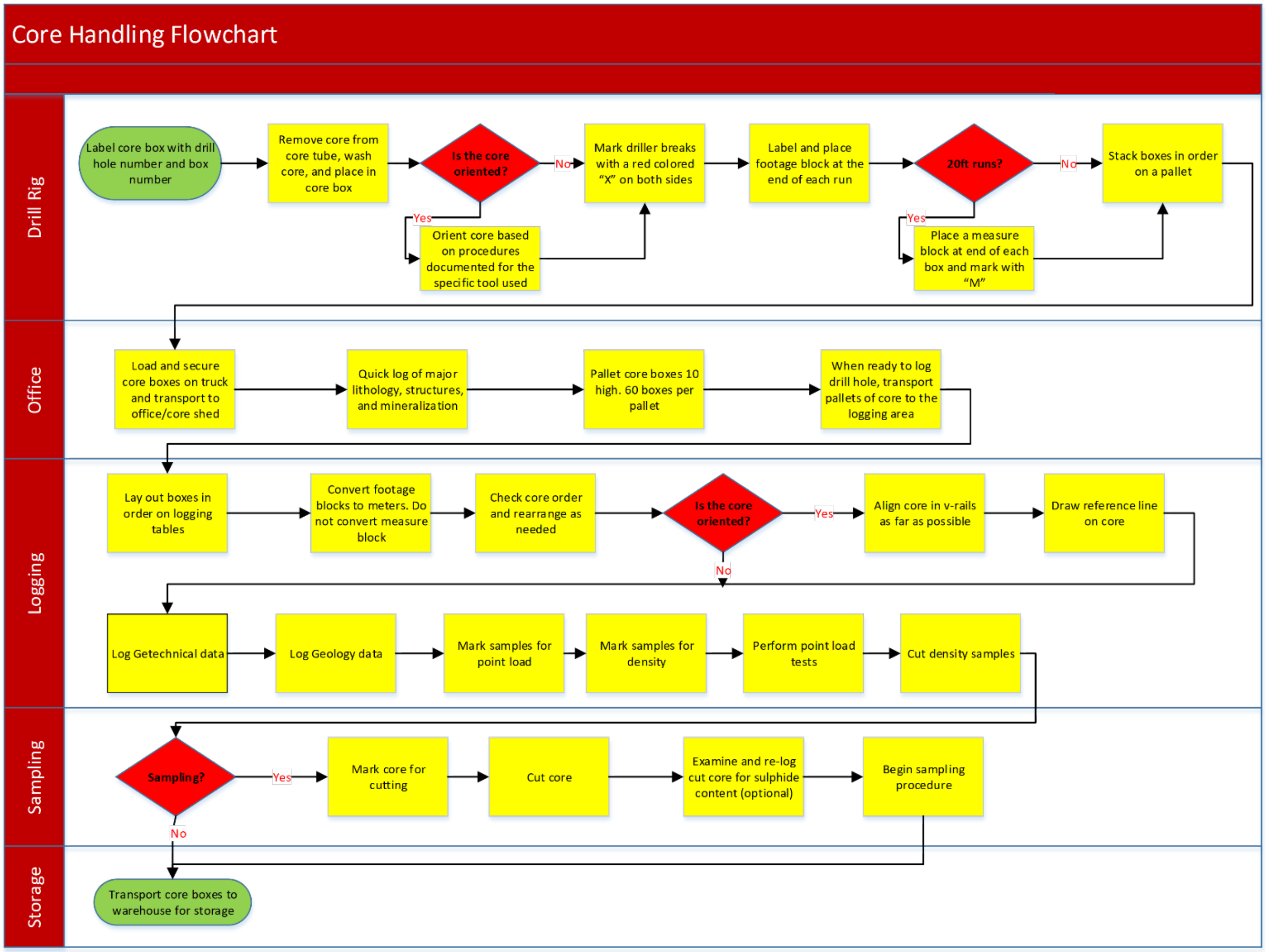


Figure 10.3: Eagle Core Handling Flowchart

11. Sample Preparation, Analyses, and Security

11.1 Historical Diamond Drill Sample Preparation and Analysis

11.1.1 Sampling

Between 2004 and 2025, the core samples comprised half-cores cut longitudinally using a diamond saw. Sampling was carried out with breaks for lithology or changes in mineralization type. Minimum sample size was 0.5 m, and most samples were 1.5 m or less.

All sampled intervals were selected, marked up, and inspected after sawing by the logging geologist prior to sampling. Intervals were tagged by the geologist by stapling a duplicate of the paper ID tag and the placement of a metal tag in the box for future reference. The core was also marked with an indelible pen or lumber crayon.

11.1.2 Sample Transport

Samples were placed in bags along with an identification tag; the bags were tied, labeled, and placed in plastic pails for shipment to ALS Chemex (ALS) in Thunder Bay, Ontario, or Reno, Nevada. Shipment descriptions, including sample numbers, were recorded on tracking sheets, which were faxed to the laboratory and to the Vancouver office at the time of shipping. Prior to 2004, samples were transported by KEMC personnel to Duluth, Minnesota, and placed in storage for pick-up by ALS. After 2004, samples were transported by commercial carrier directly to Thunder Bay. Sample pick-up was confirmed by electronic mail, and ALS was required to inspect the samples, note discrepancies, and scan and email a signed tracking sheet as a confirmation of the receipt of the samples.

11.1.3 Sample Preparation

Prior to 2003, drill core samples were shipped to ALS in Reno, Nevada, for crushing, splitting, and pulverization. From 2004 to 2015, samples were prepped for analysis at ALS in Thunder Bay, and from 2015 to 2019, some of the samples were sent to Minerals Processing Corporation (MPC), located in Carney, Michigan.

Prior to 2004, the entire sample was crushed to 70% minus 2 mm. Subsequently, the standard was set at ALS for the sample to be crushed to 90% minus 2 mm. A 1,000 gram (g) subsample was then riffle split out and pulverized using a ring mill to 85% passing a 75 micron (µm) screen. The entire pulp was then sent to ALS in Vancouver for analysis.

The current protocols employed by ALS for sample crushing and pulverizing are described in more detail below.

11.2 Current Diamond Drill Sample Preparation and Analysis

11.2.1 Sampling

Eagle has Standard Operating Procedures (SOPs) with respect to the geologic functions at the mine. The geology SOP focuses on the sampling procedures and sampling interface with the acQuire^{TM} database. The sampling takes place at the core logging facility at Eagle Mine. Filled core boxes are brought from the drill at the end of the shift and placed in a protected, marked location near the portal entrance. Eagle staff collect the core and transport it to the core shack, where it is placed on inspection (core) tables. The drill core is then remeasured and marked in metric with all Imperial distance/length blocks of the driller converted. The boxes are numbered, and the from-to lengths are written on the outside of the box. The core is then geologically logged, samples marked, and photographed. The majority of core sample lengths are 1.5 m or less with breaks for lithological contacts or changes in mineralization, such as a transition from SMSU to MSU. The minimum sample length is 0.5 m, and the maximum is 2.0 m. The core is then halved inside an automated core cutter, in approximately 40 cm lengths, whereupon both halves are returned to the core box. The core boxes, with split samples, are then returned to the table where the sampling procedure begins. Eagle generates its own bar-coded adhesive sample tags for use with the samples coordinated via the acQuire^{TM} database logging and sampling program. One is affixed to the core box at the beginning of a specific sample that matches the same depth in the geologic log, and the twin is affixed to a cloth sample bag with the corresponding half core. The bags are tied shut and placed in a reusable plastic pallet-sized transport bin.

Eagle Mine employs a QA/QC Standard Operating Procedure (SOP) with respect to the sampling of core. The current SOP indicates an insertion rate of one in ten QA/QC samples on a rotating basis between blanks, duplicates, and standards (each at a rate of one in thirty and at the discretion of the logging geologist). These are logged into the acQuire system as part of the regular logging and sampling of core. Sample dispatch and lab results are also integrated using the same acQuire system. There is a written procedure for taking the QA/QC sample results and inserting them into the appropriate spreadsheet for graphing error analysis. Except in cases of obvious errors, all re-assay triggering events are at the discretion of the Senior Geologist.

11.2.2 Sample Transport

Once the plastic pallet-sized transport bin has been filled with samples, a lid is placed on top, and colored, numbered seals are affixed to the outside, securing the lid to the bin. A dispatch of numbered samples, along with the color and lid seal numbers, is placed inside the container prior to being sealed as a check against possible tampering.

The sample container is picked up and transported by Line C transport to the ALS Prep Lab in Thunder Bay, Ontario, Canada. Representative pulps are sent to ALS Vancouver for final lithogeochemical analysis. ALS employs its own laboratory information management (LIMs) system; thus, each Eagle Sample received will get its own unique ALS LIM ID number. The corresponding number follows the sample through the preparatory and analysis process. Certified sample results with both corresponding sample ID numbers are sent to the Eagle Mine via email as an un-editable PDF file and as an XLS file. Sample rejects and pulps are returned to Eagle Mine and stored at the Talon secure warehouse facility in Negaunee, Michigan. Once the sampling and logging process is completed, the core boxes are palletized, wrapped in plastic, and transported to the core warehouse in Negaunee. The Negaunee warehouses are locked and located within a gated industrial property.

The QP finds that the sampling procedures and chain of custody meet industry standards. It is recommended that any pulps required for future analysis or metallurgical testing be stored in vacuum-sealed bags or refrigerated to prevent oxidation.

Figure 11.1 presents a flowchart for the Eagle diamond drill core sampling process.

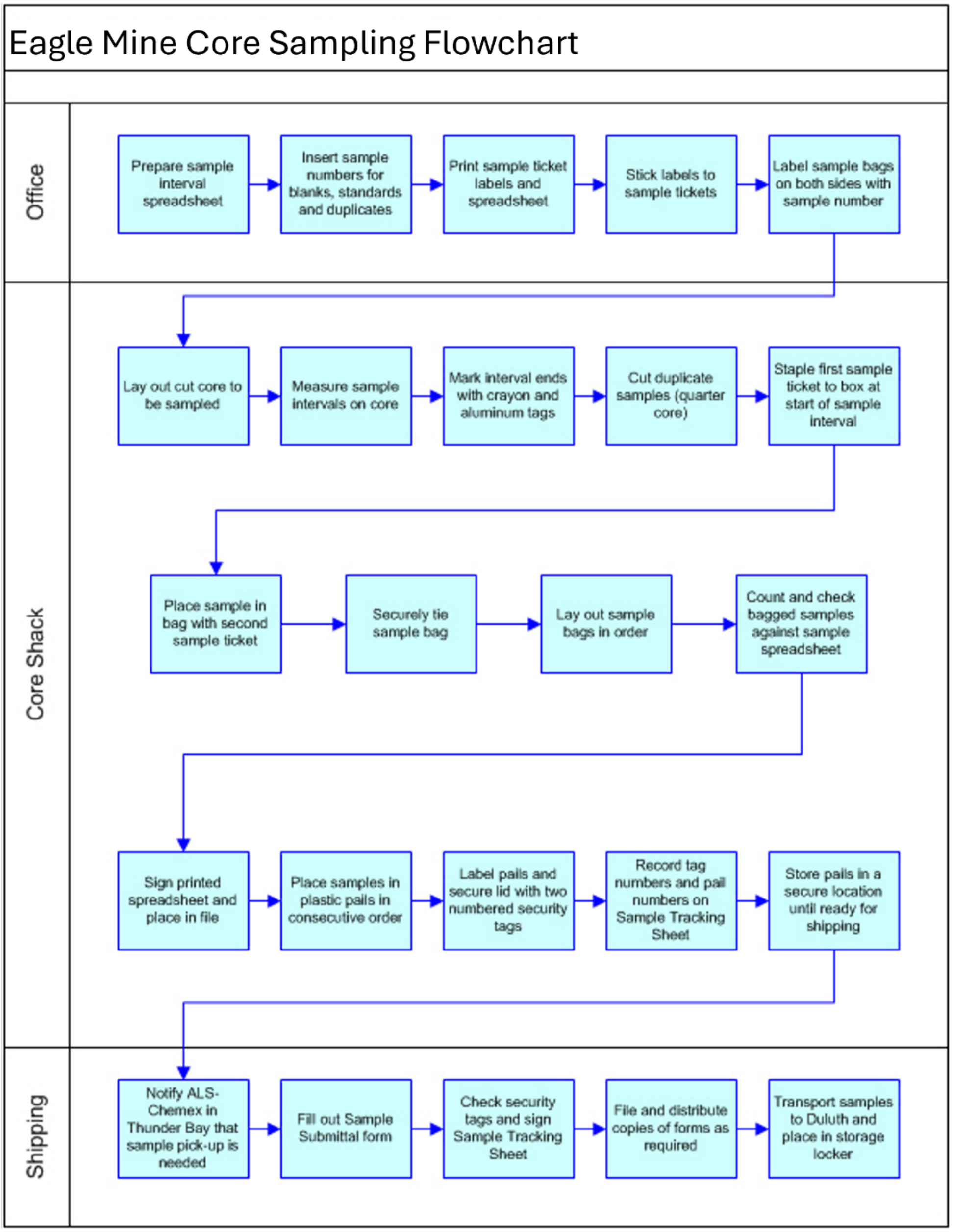


Figure 11.1: Eagle Core Sampling Flowchart

11.2.3 Sample Preparation

Samples are shipped to the ALS laboratory in Thunder Bay, Ontario, for preparation ahead of assaying.

ALS is an independent laboratory based in Thunder Bay Ontario.

The facility has standard procedures and quality controls for sample preparation to ensure compliance with industry and client standards. ALS has a digital Laboratory Information Management System (LIMS) and a web-based data retrieval system for customers to obtain assay results. The sample preparation procedures carried out on Eagle's diamond drill core samples at the Thunder Bay facility consisted of the following:

- Upon arrival, each sample is logged in the LIMS system, and a barcode label is attached.
- Drying of excessively wet samples in drying ovens.
- Fine crushing of samples to better than 70% of the sample passing two millimeters (CRU-31).
- Split sample using riffle splitter (SPL-21).
- A sample split of up to 250 g is pulverized to better than 85% of the sample passing 75 µm (PUL-31).

11.2.4 Analysis

Pulps are sent to the ALS laboratory in Vancouver for analysis. ALS Vancouver is an accredited laboratory in accordance with the International Standard ISO/IEC 17025:2017.

Samples are analyzed by a variety of methods for specific elements and mineralization types. The ALS assay codes and methods used include:

- **OA-GRA08** – Bulk density on whole core by water immersion method. Used as a check on the density measurements made by Talon personnel.
- **ME-ICP81** – Sodium peroxide fusion with inductively-coupled atomic emission spectroscopy (ICP-AES). Al, As, Ca, Co, Cr, Cu, Fe, K, Mg, Mn, Ni, Pb, S, Si, Ti, Zn.
- **ME-OG46** – Ag by aqua regia digestion with ICP-AES or atomic absorption spectroscopy (AAS). Triggered by over limits on As, Cd, Co, Cu, Fe, Mn, Ni, Pb, S, Zn.
- **Ag-OG46** – Ag by aqua regia digestion with ICP-AES or atomic absorption spectroscopy
- **PGM-ICP23** – Pt, Pd, and Au by fire assay with ICP-AES finish.

11.3 Quality Assurance/Quality Control

Quality Assurance (QA) consists of evidence to demonstrate that the assay data has precision and accuracy within generally accepted limits for the sampling and analytical method(s) used in order to have confidence in the Mineral Resource estimation. Quality Control (QC) consists of procedures used to ensure that an adequate level of quality is maintained in the process of sampling, preparing, and assaying the exploration drilling samples. In general, QA/QC programs are designed to prevent or detect contamination and allow analytical precision and accuracy to be quantified. In addition, a QA/QC program can disclose the overall sampling – assaying variability of the sampling method itself.

Accuracy is assessed by a review of assays of certified reference materials (CRMs), and by check assaying at outside accredited laboratories. Assay precision is assessed by reprocessing duplicate samples from each stage of the analytical process, from the primary stage of sample splitting, through sample preparation stages of crushing/splitting, pulverizing/splitting, and assaying.

Standardized protocols of QA/QC sample insertion using certified reference material, blanks, and duplicates have been used throughout the history of the Eagle project to monitor the quality of the sampling process and assay results. KEX initiated assay QA/QC protocols for the early exploration drilling at Eagle beginning in 2001. Initially, standards, blanks, and duplicates were inserted into the sample stream at an interval of one every ten samples. Currently, the insertion rate is one in thirty samples, consistent with mature mine protocols.

Blanks were also inserted following obvious high-grade samples. Over time, the QA/QC protocols have been modified to address specific concerns; however, the procedures used today are very similar to those used in past programs.

11.3.1 Blanks

The regular submission of blank material is used to assess contamination during sample preparation and to identify sample numbering errors. Blank material initially was derived from “barren” rocks from the area, but these were found to contain traces of mineralization, and therefore, deemed unsuitable. Since that time (post drill hole eewe007), industrial silica sand, purchased from a local source, has been used. Blanks are now inserted into the sample stream at a rate of one in thirty samples, or just after an obviously high-grade sample. The blanks are assayed for Au, Co, Cu, Ni, Pd, Pt, and S.

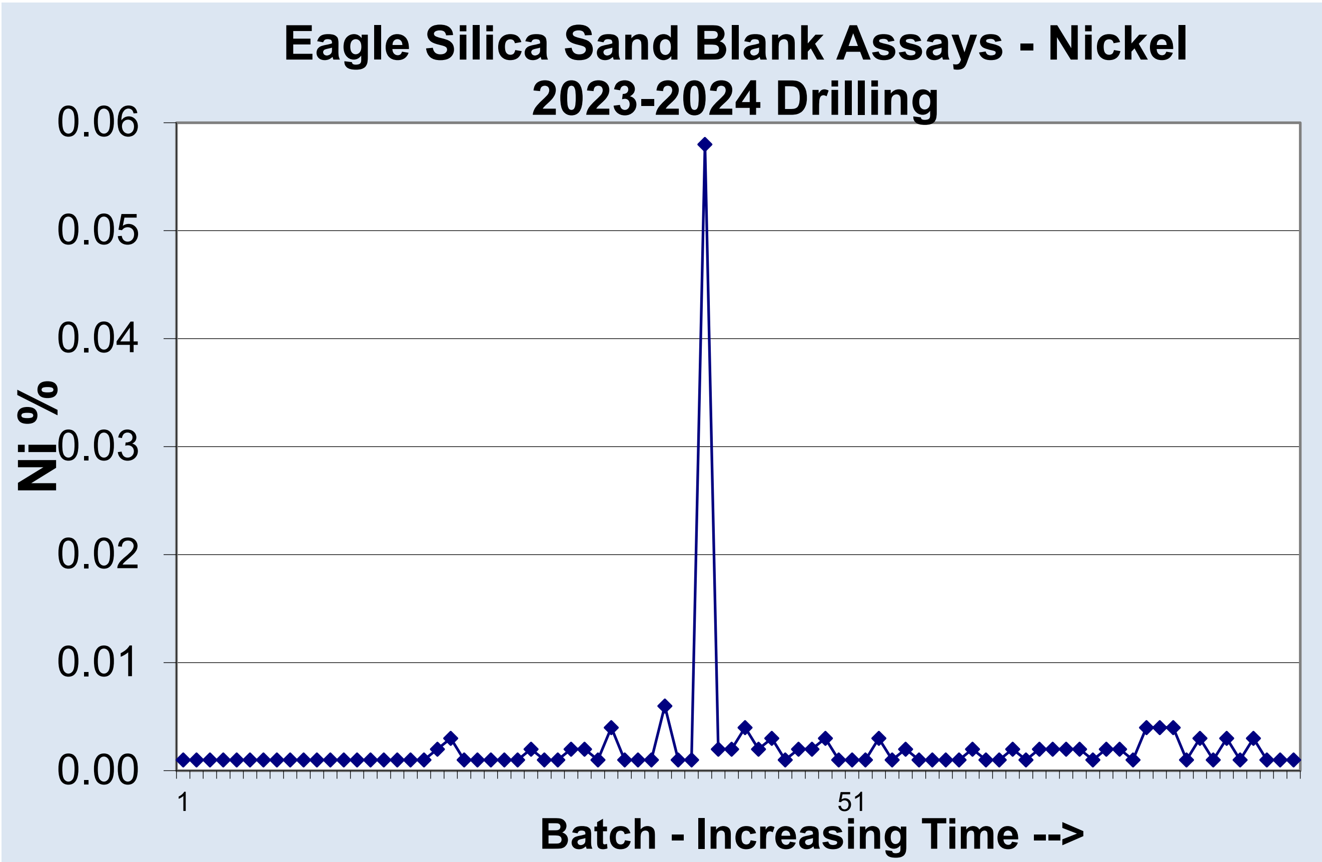


Figure 11.2: Eagle Silica Sand Blank Assays - Nickel

11.3.2 Duplicates

Duplicate samples are used to test for contamination in the laboratory and for overall consistency in performance. These duplicates can be made of the original sample material (termed field duplicates), the crushed reject material (reject), or the pulverized sample material (pulp). Each type of duplicate tests for inaccuracy at different stages in the sample preparation and assay.

Field duplicates at Eagle are quarter-core splits taken from the original half-core samples.

These are also taken at a rate of one in thirty but are offset from the standards and blanks by four or five samples. Splits of the rejects are made by ALS every 20th sample, and a pulp duplicate is taken approximately every 30th sample for the purposes of internal lab QA/QC. The acQuire database exports data to Excel, which produces scatter diagrams that compare the duplicate value with the original. Also plotted on these diagrams were regression lines to check for bias, as well as error limits.

The QP inspected the scatter diagrams up to 2024 field duplicates and noted that, while there are instances of significant differences between duplicate pairs, Au in particular displays a distinct nugget effect through all years but no bias.

The mill grade reconciliation with the block model is observed to be very good, and it does not appear to be an issue at this time.

The duplicates are assayed for Au, Co, Cu, Ni, Pd, Pt, and S.

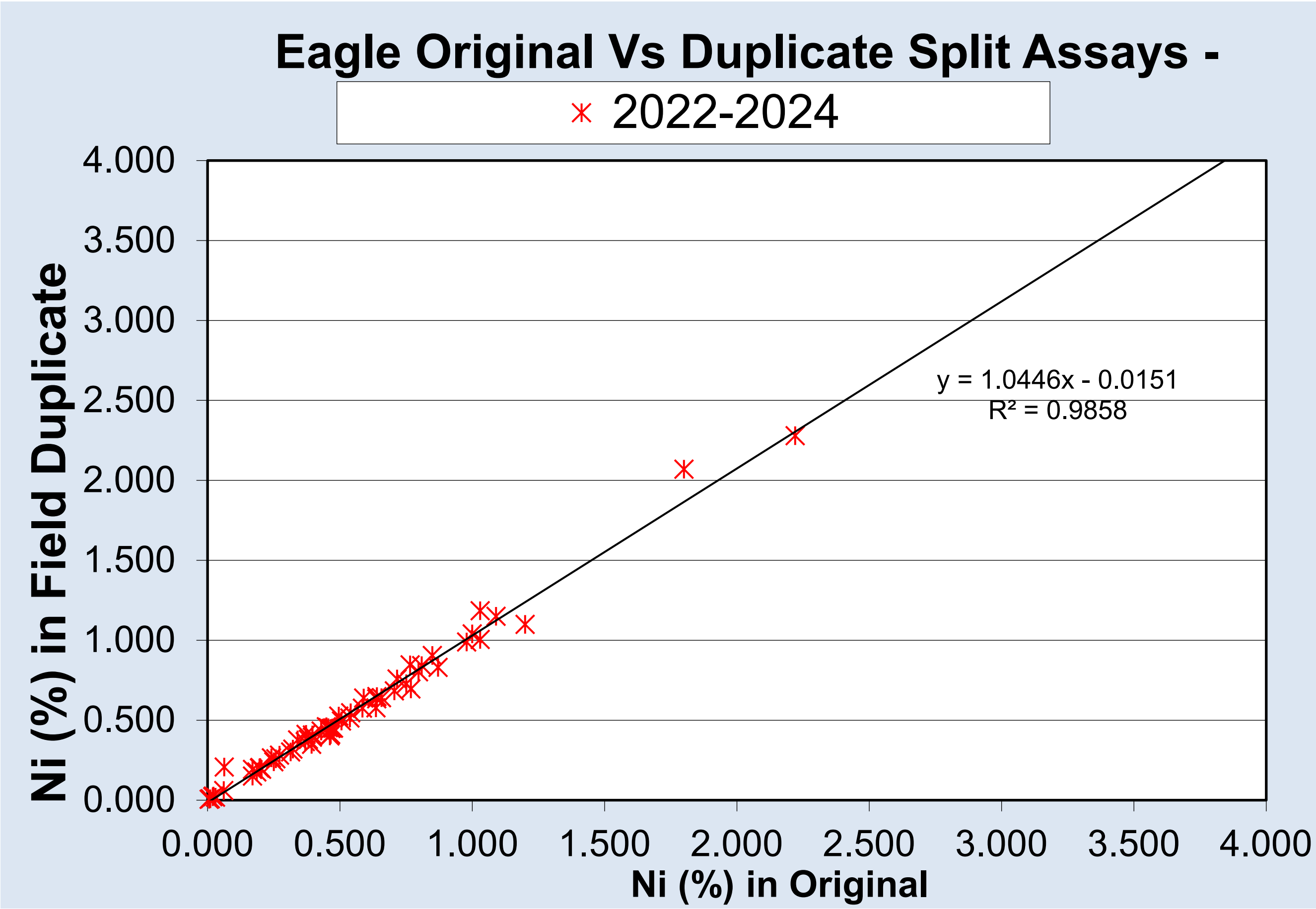


Figure 11.3: Eagle Original Versus Duplicate Split Assays

11.3.3 Certified Reference Material (Standards)

Results of the regular submission of certified reference materials (CRMs) are used to monitor analytical accuracy and to identify potential problems with specific batches. Specific pass/fail criteria are determined from the standard deviation (SD) provided for each CRM. The conventional approach for setting standard acceptance limits is to use the mean assay ± two SDs as a warning limit and ± three SD as a failure limit. Results falling outside of the ± three SD failure limit must be investigated to determine the source of the erratic result, either analytical or clerical. Eagle Mine uses a threshold of two standard deviations from the mean standard value on plots to gauge lab bias; however, it is at the discretion of the Senior Geologist to gauge whether it triggers a sample or batch re-assay.

Standards, consisting of 100 packets of material, are inserted every thirtieth sample in the same fashion as blanks. Only custom-made standards are currently applied, although a combination of commercial and custom (seven different ones) has been used in the past. The standards are assayed for Au, Co, Cu, Ni, Pd, Pt, and S. See Table 11.1 for the current CRMs used.

Table 11.1: Current Certified Reference Material at Eagle Mine

CRM	Expected Grades						
	Au (g/t)	Pt (g/t)	Pd (g/t)	Co (%)	Cu (%)	Ni (%)	S (%)
EA-01	0.050	0.073	0.054	0.020	0.429	0.517	2.750
EA-02	0.100	0.185	0.119	0.033	0.949	1.100	5.920
Ea-03	0.102	0.316	0.193	0.062	1.660	2.380	12.220
EA-S	0.171	0.503	0.289	0.065	1.771	2.308	12.368

Note: Smee and Associates conducted the certification.

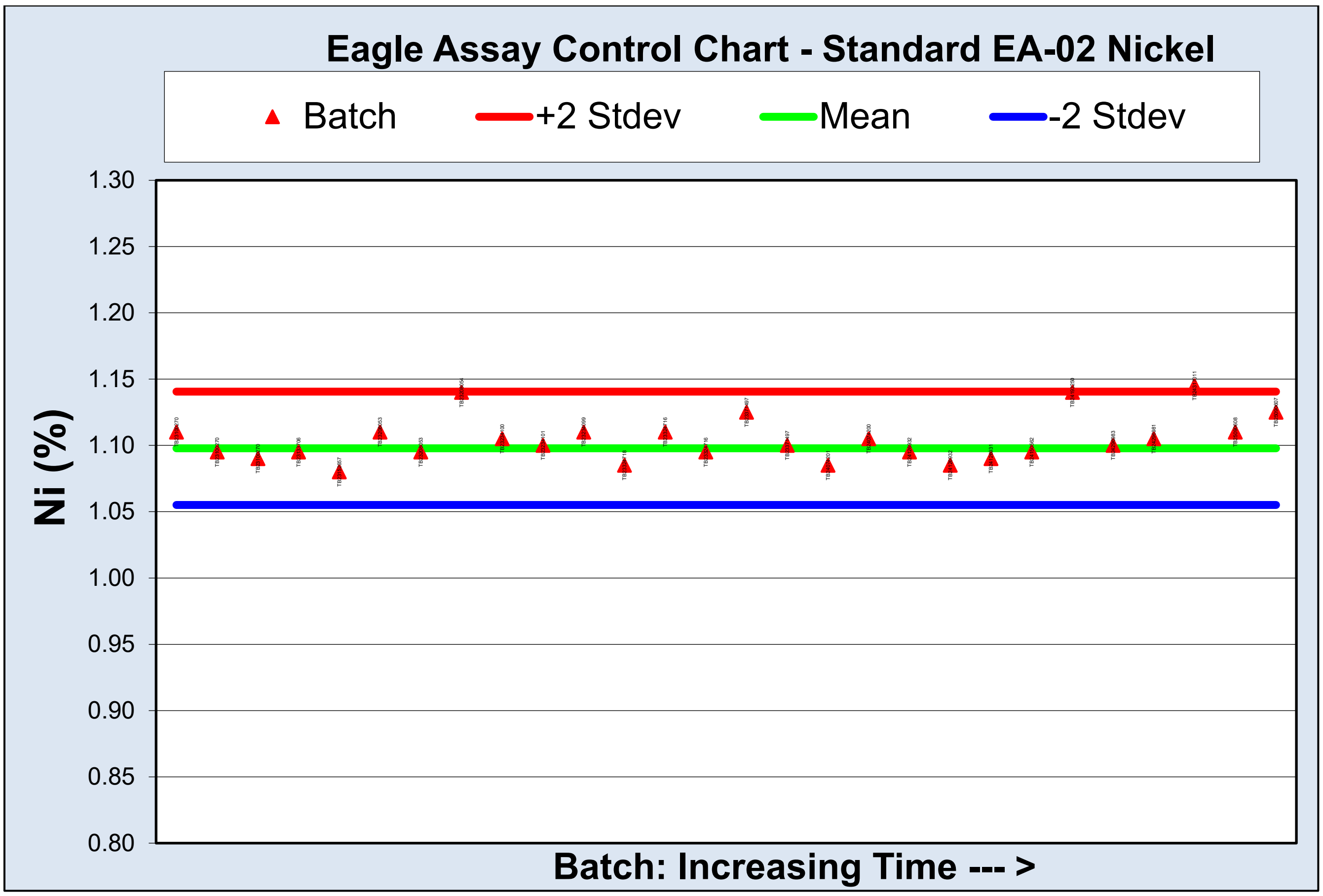


Figure 11.4: Eagle Assay Control Chart – Standard EA-02 Nickel

11.4 Underground Sampling

Muck samples are collected from underground sills and stopes for grade control, reporting, and monitoring purposes. They are not used for the estimation of Mineral Resources.

Underground sampling procedures aim to collect one sample per 150 to 200 tonnes of ore produced per month. Sampling protocols employed depend on the source of the ore.

11.4.1 Stope Sampling

Four samples are collected for each mucking event (by shift). The material is either collected from re-muck, from the loader actively mucking the stope, or from a haul truck as it is dumped in the COSA. Care is taken to ensure that all material types present in the muck pile are representatively added to the sample bag. Sample bags are filled to approximately half capacity (10 in x 17 in sample bag). Sample weights range from 10 lb to 30 lb, depending on mineralization type.

11.4.2 Sill Sampling

The number of samples collected is dependent on the width of the round shot. For six-meter primary and five-meter secondary rounds, four samples are collected. For four -meter primary rounds, two samples are collected. The sample is collected from either a fresh muck pile or remuck.

Sill samples can also be collected from a haul truck as it is dumped in the COSA. If a round was not sampled from these methods, rib samples may take the place of muck samples. Face samples are taken occasionally; however, the primary form of sample for reporting is from the muck pile. Due care is taken that all material types in the muck pile are representatively added to the sample bag. Sample weights range from 10 lb to 30 lb, depending on mineralization type.

11.4.3 Underground Sampling QA/QC

Muck samples are submitted to the assay laboratory at the Humboldt Mill on a daily basis.

Each submittal includes one sample for QA/QC: on a rotating basis, either a silica sand blank or one of two standards purchased from CDN Resource Laboratories, Canada. The standards are certified reference material in 60 g packets, which are sealed until submission to the mill laboratory.

11.4.4 Security

The QP is not aware of any major security issues at the Eagle Mine or the Negaunee Exploration Office/Warehouse. Access to these sites is restricted to authorized personnel, and they are staffed continuously. Drill and mine samples are handled and transported only by Talon personnel or contractors. Samples are picked up and transported to the laboratory by commercial carrier. Logging, sampling, and analytical data are captured in an acQuire database, which resides on the company's servers and is backed up daily. The integrity of this database is the responsibility of a Database Manager, who has exclusive access.

11.5 2QP Opinion

Eagle is an operating mine with a history of independent data reviews covering sampling, analytical, QA/QC, and chain of custody procedures. Past reviews include WSP/Golder in 2022, RPA in 2004, 2006, 2009, and 2016. In each case, there were no material concerns found that would preclude the use of the drill data in resource estimation.

On completion of the review of Eagle's procedures and the results of their QAQC and mining reconciliation, it is the QP's opinion that the procedures in use are consistent with standard industry practices and that the drill hole database is of suitable quality for use in the estimation of Mineral Resources.

The QP notes that there is a minor issue due to selective sampling procedures, based on visual estimates of sulfide mineralization, where some samples within a low-grade area of the interpreted Keel mineral domain wireframe were not sampled. It is recommended that this core be sampled if still available in storage and that any future infill drill programs establish boundary limits for sampling to ensure that all potential mineralization within the area of interest is fully sampled.

12. Data Verification

12.1 WSP 2026

Data verification conducted by the QP in 2026 consisted of a personal site inspection of the Eagle Mine, along with spot check comparisons of the assay data against the original laboratory certificates and independent QAQC checks of certified reference materials and pulp duplicate analysis.

During the site visit, reserves process estimation, mining design, and scheduling parameters were thoroughly reviewed and verified. Additionally, inspections were conducted on underground development headings, stopes, the ventilation system, and escape routes.

The QP has also reviewed the work and taken into consideration the assessment of the former WSP/Golder QP (James McDonald), who conducted a site visit and more thorough data verification in 2022, which has been included in its entirety in Item 12.2 of this Report.

12.1.1 Site Visit

The QP responsible for the MRE disclosed in Item 14 of this Report conducted a site inspection of Eagle mine between February 16 and 17, 2026. The site inspection included an underground tour of the mine, surface infrastructure tour, review of QAQC procedures, grade control procedures, and the block model and grade estimation methodology.

The underground tour included active production and development headings for the Eagle, Eagle East, and Keel deposits. Figure 12.1 provides an example of sulfide mineralization seen in Eagle East.

Figure 12.1: Sulfide Mineralization in Eagle East

There were no active drills present at the mine, and no core was available for inspection. Therefore, independent verification logging and sampling were not conducted.

12.1.2 Assay Data Verification

The verification activities for this report consisted of data spot check comparisons on assays generated by ALS Laboratories compared to Talon's drill hole sample database and independent QAQC analysis. These checks build upon the more rigorous independent verification, sampling, and QAQC review completed during the 2022 Site visit, which is described in Item 12.2.

For the 2023–2025 data, a series of digital and database-level verification checks focused on confirming the integrity of assay data transfers was carried out under the supervision of the QP. Talon assay data were constrained to the Eagle East and Keel mineralization (representing the majority of the remaining mineral resources) and compared to an independently compiled dataset of the original ALS Certificate of Assay values in .csv format. A randomized subset of samples (~10%) was further selected and compared to the original .pdf certificates from ALS.

Analytical results for Ni, Cu, Co, Au, Pt, Pd, and Ag were directly compared between the Talon assay database and the laboratory certificate values with no discrepancies identified. A summary of the data reviewed in Table 12.1.

Table 12.1: Assay Data Verification Checks against Lab Certificates

	Data Checks with Lab Certificate .csv File	Data Checks with Lab Certificate .pdf File
No. Drill holes	53	43
No. Samples	828	80
No. Certificates	13	13
Assay Date Range	May 2023 - Nov 2024	May 2023 - Nov 2024
Ni Min	0.04	0.12
Ni Max	6.4	5.58
Cu Min	0.01	0.023
Cu Ma	5.94	3.07
Co Min	0.001	0.01
Co Max	0.16	0.14
Au Min	0.0005	0.002
Au Max	0.38	0.28

	Data Checks with Lab Certificate .csv File	Data Checks with Lab Certificate .pdf File
Pt Min	0.002	0.01
Pt Max	0.89	0.89
Pd Min	0.001	0.003
Pd Max	0.66	0.42
Ag Min	0.5	0.5
Ag Max	23	8
No. Errors	0	0

Based on these checks, the QP is satisfied that the assay data for the 2023–2025 period is suitable for use in the current technical report. More detailed evaluation of analytical performance, including assessment of duplicates, blanks, and standards, is addressed separately in Section 12.1.3.

12.1.3 QAQC Review

As part of an independent assessment of the duplicates, blanks, and standards, the Eagle Mine QAQC was independently reviewed for a subset of samples related to the Eagle East and Keel mineralization and their associated lab batches.

12.1.4 Field Duplicates

Field duplicates were compared against original samples for six main elements (Ni, Cu, Co, Au, Pt, and Pd) and found to have reasonable correlation with each other (e.g., Table 12.2) with Au showing a distinct nugget effect, as expected.

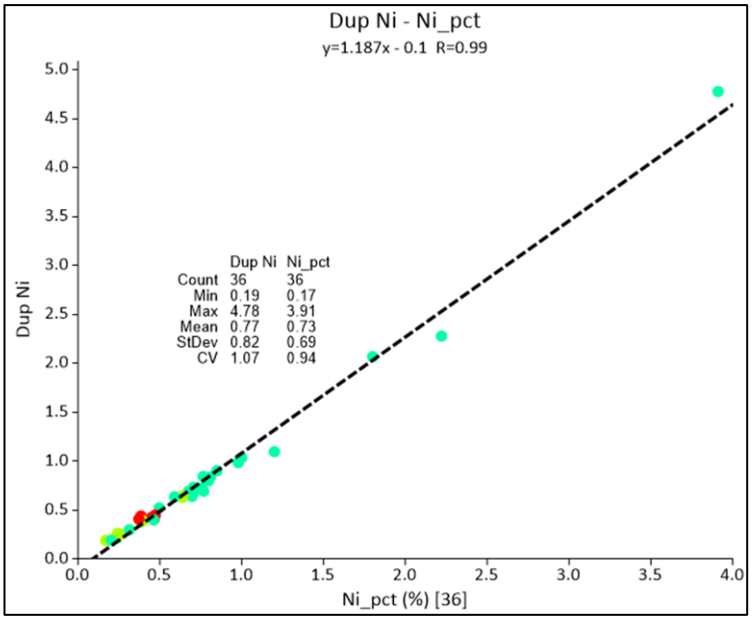


Figure 12.2: Nickel values of 2023-2024 Keel Field Duplicates

12.1.5 Blanks

A review of current blanks in 2023-2025 indicates that successful procedures were implemented during sample preparation. All analyses are well within defined tolerance levels. The previously identified concerns in historical data for Cr (pre- 2019) no longer continue to be an issue (Figure 12.3).

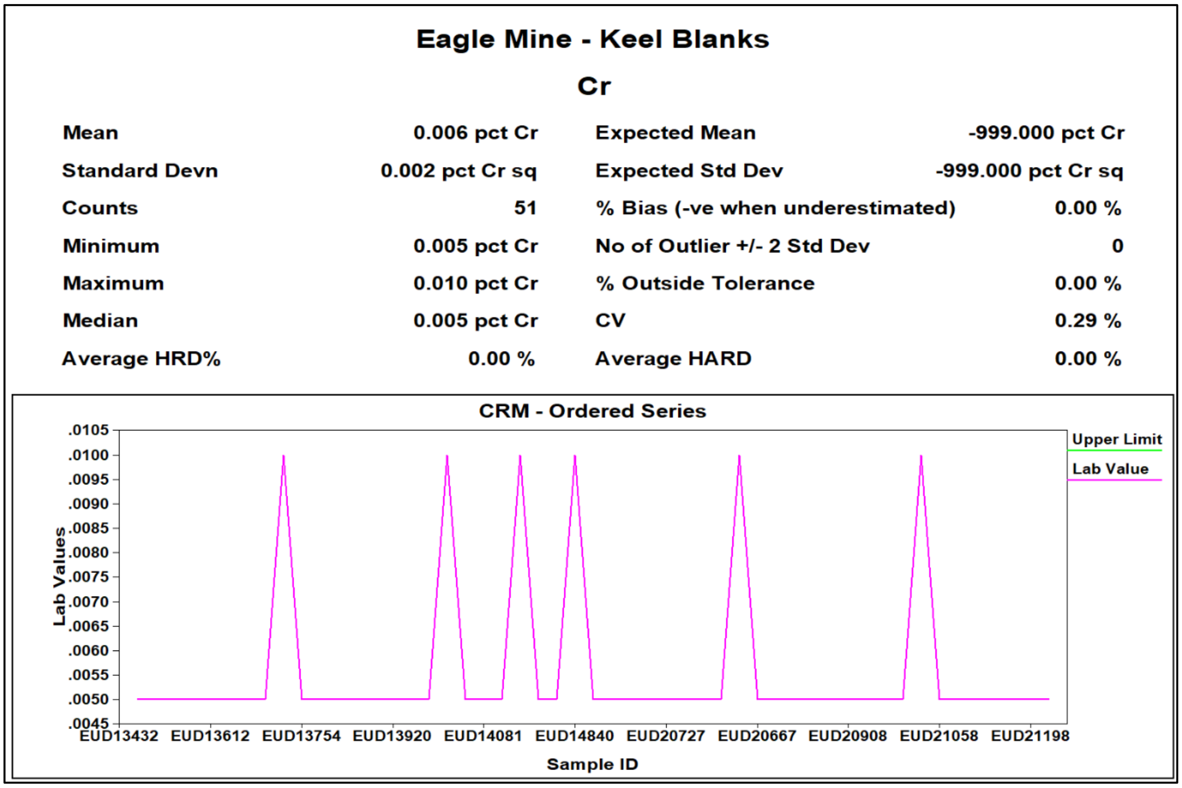


Figure 12.3: Chromium Values in 2023-2025 Blanks

12.1.6 Standards

The same four customized standards used in 2022 and prior are currently still in use. Assay results of these standards from between 2023 and 2025 were reviewed and plotted independently and compared against Talon's internal QAQC documents. Talon's documents were found to be set up correctly, and various plots were independently replicated. Overall, the standards are performing well and within 2 standard deviations of the certified reference material, with some outliers in Au. Figure 12.4 presents the recent standards for EA-3 within the Keel mineralization, between 2023 and 2024.

Keel Standard EA-03

Standard EA-03 - Cu

Mean	1.644 pct Cu	Expected Mean	1.661 pct Cu
Standard Devn	0.037 pct Cu sq	Expected Std Dev	0.093 pct Cu sq
Counts	11	% Bias (-ve when underestimated)	-1.02 %
Minimum	1.600 pct Cu	No of Outlier +/- 3 Std Dev	0
Maximum	1.715 pct Cu	% Outside Tolerance	0.00 %
Median	1.640 pct Cu	CV	0.02 %
Average HRD%	-0.52 %	Average HARD	1.08 %

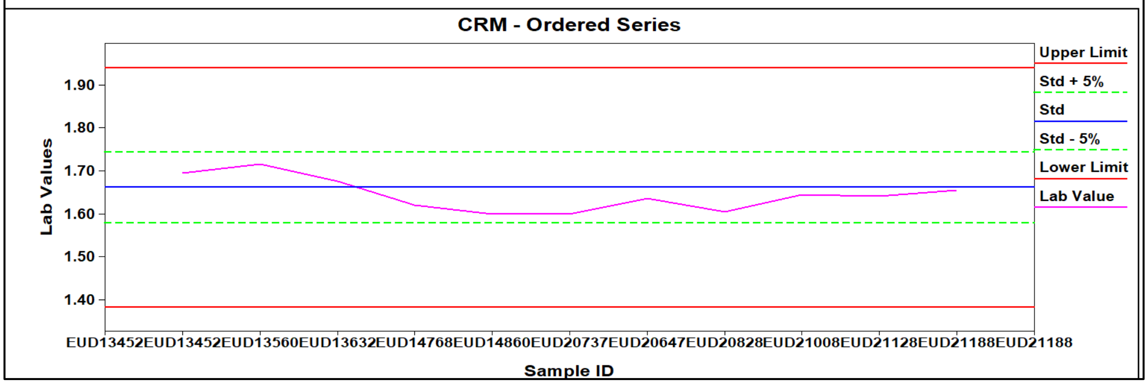


Figure 12.4 QAQC of Copper Values for Eagle Standard EA-3 within the Keel Mineralization

12.2 WSP/Golder 2022

In 2022, the WSP/Golder QP conducted several verification checks at Eagle Mine and the Negaunee core storage facility during a two-day site visit on May 10 and 11, 2022. The verification process included a review of:

- Confirmation core logging and independent assay verification on selected drill core samples
- Chain of custody of drill core samples and storage and security of historic drill core
- QA/QC performance of the assay database for the metal suite
- Data verification, including spot check comparisons of metal assays from the drill hole database against the original assay lab certificates
- Visiting underground mineralization contacts
- Drill collar inspections

Details of the Site visit and data verification are summarized in the subsequent sub-sections.

12.2.1 Independent Logging and Sample Verification

Prior to the site visit, the QP selected six individual samples, each from a unique hole representing the various mineralization domains and spatially spread out from the others in both the Eagle and Eagle East Deposits. During the Site Audit, each was logged, photographed, quarter sawn, and then sampled and tagged in a manner consistent with the SOP at Eagle Mine. These six samples, as well as one prepared standard (EA-2), were then submitted and analyzed at ALS laboratories in Sudbury (preparation) and Vancouver (lithogeochemical analysis). The analytical procedures for determining Ni, Cu, Co, and S are a Sodium Peroxide Fusion/ ICP finish (ALS methods **ME-ICP81**), for Au, Pt, Pd, a fire assay with ICP finish (ALS method **PGM-ICP23**), and for Ag, an Aqua Regia digestion/ICP finish (**ME-OG46**). Specific gravity tests were performed on all samples via the gravimetric process (**OA-GRA08**). The results compared to the original assays are summarized in Table 12.2. Figure 12.5 and Figure 12.6 provide a graphical comparison of the QP verification and Eagle mine assays for Ni and Cu, respectively. All the duplicate samples selected by the QP demonstrate acceptable precision and reproducibility consistent with the Eagle Mine database.

Table 12.2: Verification Sampling of Eagle Mine Assay Intervals

Drillhole	Sample ID	From	To	Length	Eagle Cu (wt. %)	Golder Cu (wt. %)	Eagle Ni (wt. %)	Golder Ni (wt. %)	Eagle Au (ppm)	Golder Au (ppm)	Eagle Pt (ppm)	Golder Pt (ppm)	Eagle Pd (ppm)	Golder Pd (ppm)	Eagle Co (wt. %)	Golder Co (wt. %)	Eagle S (wt. %)	Golder S (wt. %)
EEUG133	EUD20112	160.91	162.4	1.51	4.68	4.69	7.85	7.98	0.165	0.16	0.961	1.25	0.608	0.737	0.193	0.198	36.30	36.2
EEUG094	EUD19062	173.88	175.5	1.58	3.76	3.99	6	6.46	0.383	0.625	1.12	1.065	0.806	0.904	0.149	0.158	29.10	30.7
EAUG0285	EUD4933	95.65	97.15	1.5	2.55	2.86	6.12	6.8	0.047	0.031	0.18	0.203	0.146	0.169	0.181	0.206	36.00	36.9
EEUG0169	EUD11930	114.89	116.4	1.5	2.37	2.47	3.56	4.19	0.08	0.125	1.095	1.08	0.618	0.677	0.072	0.09	14.05	17.2
EEWE067	EUD9793	189.26	190.8	1.5	4.35	4.48	2.52	2.81	0.911	1.07	1.265	1.25	0.743	0.837	0.046	0.051	10.00	10.8
EAUG0191	EUD3861	81.64	83.14	1.5	1.225	1.275	1.5	1.595	0.097	0.1	0.29	0.335	0.22	0.224	0.043	0.043	7.77	8.09
EA-2					0.949	0.942	1.1	1.115	0.1	0.097	0.185	0.186	0.119	0.12	0.032	0.035	5.92	5.9

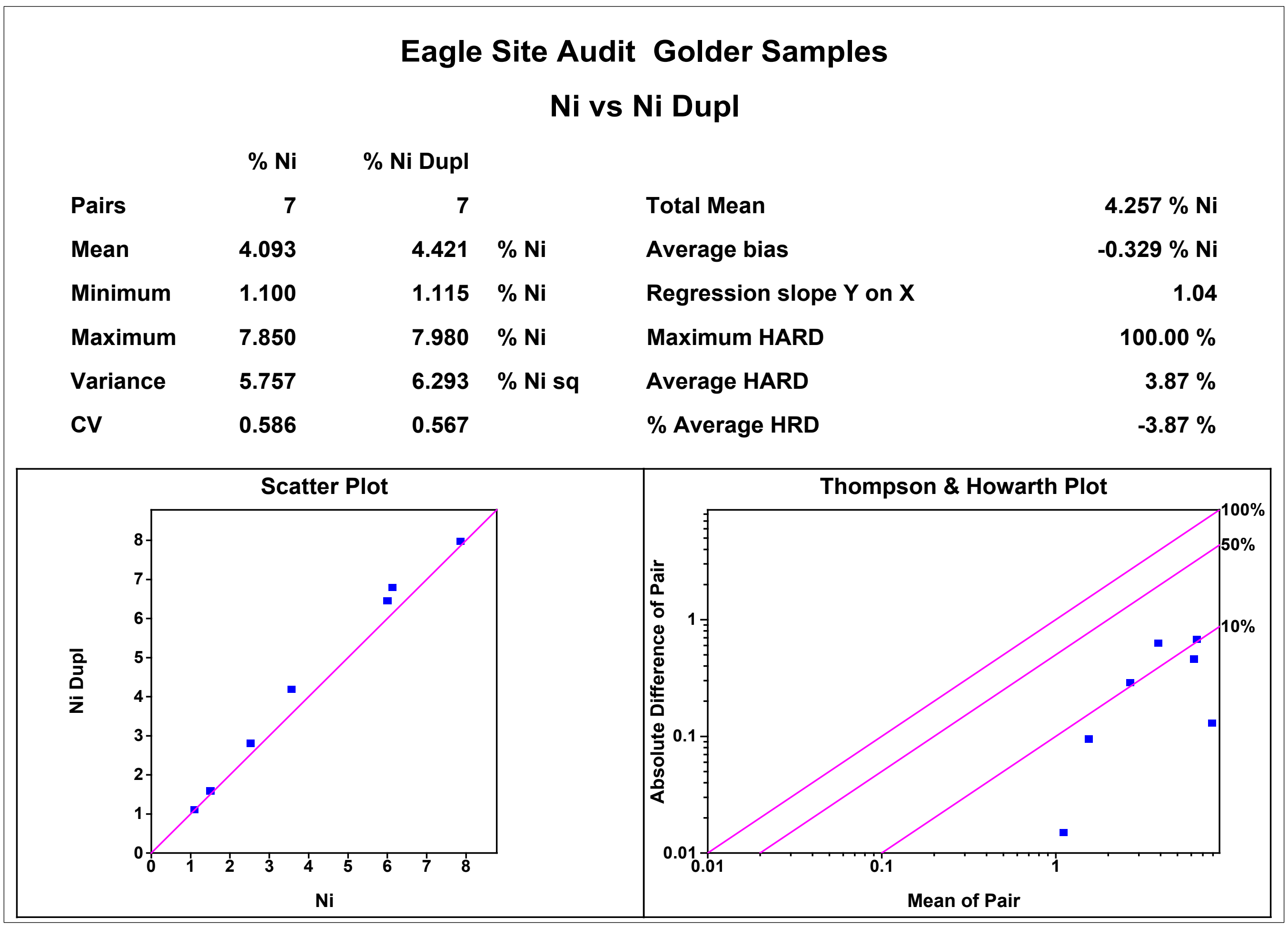


Figure 12.5: Comparison of Original Versus Verification Sampling Ni Values

Eagle Site Audit Golder Samples

Cu vs Cu Dupl

	% Cu	% Cu Dupl			
Pairs	7	7		Total Mean	2.899 % Cu
Mean	2.841	2.958	% Cu	Average bias	-0.118 % Cu
Minimum	0.949	0.942	% Cu	Regression slope Y on X	1.02
Maximum	4.680	4.690	% Cu	Maximum HARD	100.00 %
Variance	1.857	1.932	% Cu sq	Average HARD	2.10 %
CV	0.480	0.470		% Average HRD	-2.00 %

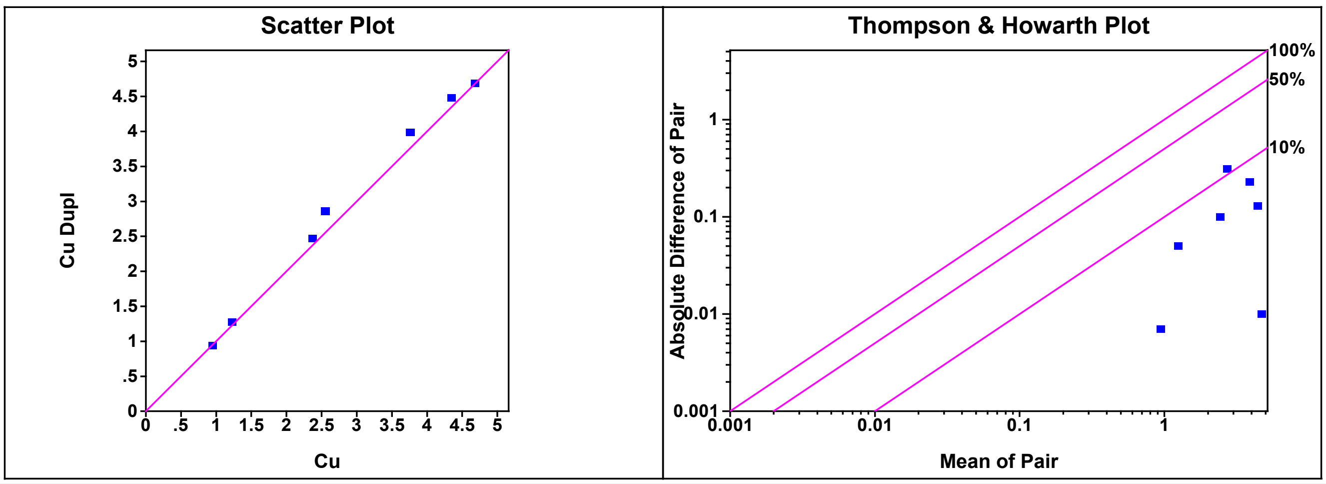


Figure 12.6: Comparison of Original Versus Verification Sampling Cu Values

12.2.2 Geological Data Verification

All logging and sampling data are captured and stored in an acQuire database.The database manager is responsible for importing the assay data via the internet directly from the laboratory, validating the data, compiling the QA/QC results, and resolving QA/QC failures. Much of the validation work is done using scripts and utilities run from within acQuire.The database manager also provides export files to downstream users for import into other software packages such as Vulcan or Leapfrog. The QP reviewed seven elements (Ni, Cu, Co, Au, Pt, Pd, Ag) of the original ALS Certificate of Assay values against the drill hole sample database. Records selected were primarily from drill holes that support the current resource in Eagle, Eagle East, and Eagle East Keel. The QP found no discrepancies between the original certificates and the database in the approximately 895 individual samples audited.

12.2.3 QA/QC Review

Eagle Mine employs a QA/QC Standard Operating Procedure (SOP) with respect to the sampling of core. The current SOP indicates an insertion rate of one in ten QA/QC samples on a rotating basis between blanks, duplicates, and standards (each at a rate of one in thirty). These are logged into the acQuire system as part of the regular logging and sampling of core. Sample dispatch and lab results are also integrated using the same acQuire system. There is a written procedure for taking the QA/QC sample results and inserting them into the appropriate spreadsheet for graphing error analysis. Except in cases of obvious errors, all re-assay triggering events are at the discretion of the Senior Geologist.

12.2.4 Field Duplicates

Quarter core field duplicates are currently inserted in the sample stream at a rate of one in thirty samples. Originally (during the initial years of the mine), field duplicates were inserted at a rate of one in twenty. A review of field duplicate analyses conducted by Eagle demonstrates a reasonable correlation to the original sample (Ni, Cu, Co, Pt, Pd, S, SG) except for Au, which showed a distinct nugget effect through all years. The QP considers an average HARD value (half absolute relative difference) between 10-20% to indicate marginal precision (See Figure 12.7).

Eagle Mine 2022 Audit

Ni vs Ni Dupl

	% Ni	% Ni Dupl			
Pairs	1709	1709		Total Mean	1.775 % Ni
Mean	1.772	1.778	% Ni	Average bias	-0.006 % Ni
Minimum	0.001	0.001	% Ni	Regression slope Y on X	1.00
Maximum	8.800	9.280	% Ni	Maximum HARD	100.00 %
Variance	4.889	4.922	% Ni sq	Average HARD	5.66 %
CV	1.248	1.248		% Average HRD	0.42 %

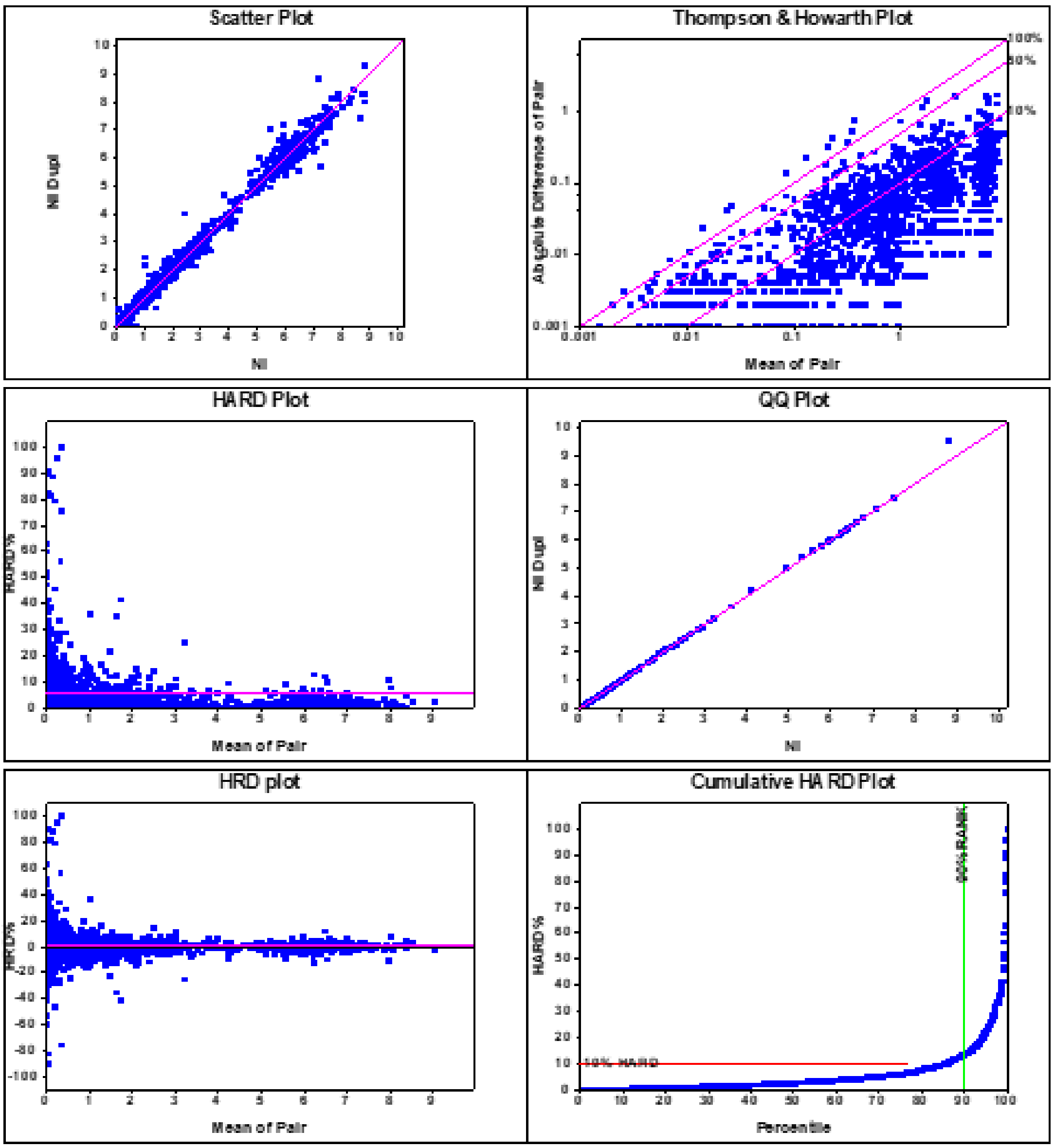


Figure 12.7: QA/QC Analysis of Eagle Ni Duplicates

12.2.5 Blanks

A review of the current blanks analyses conducted by Eagle indicates a fairly successful cleaning procedure by the prep lab; however, reviewing historical data, elevated Cr values in blank analyses did occur regularly up until hole eewe007 (September 2019). This seems to have been resolved with the Mine switching to a commercially produced pure silica sand instead of a locally sourced sandstone as their blank sample source (Figure 12.8). Early in the mine life, blank samples were inserted every ten samples or after an obvious high-grade sample. The current practice is to insert a blank at a rate of one in thirty samples or at the discretion of the logging geologist.

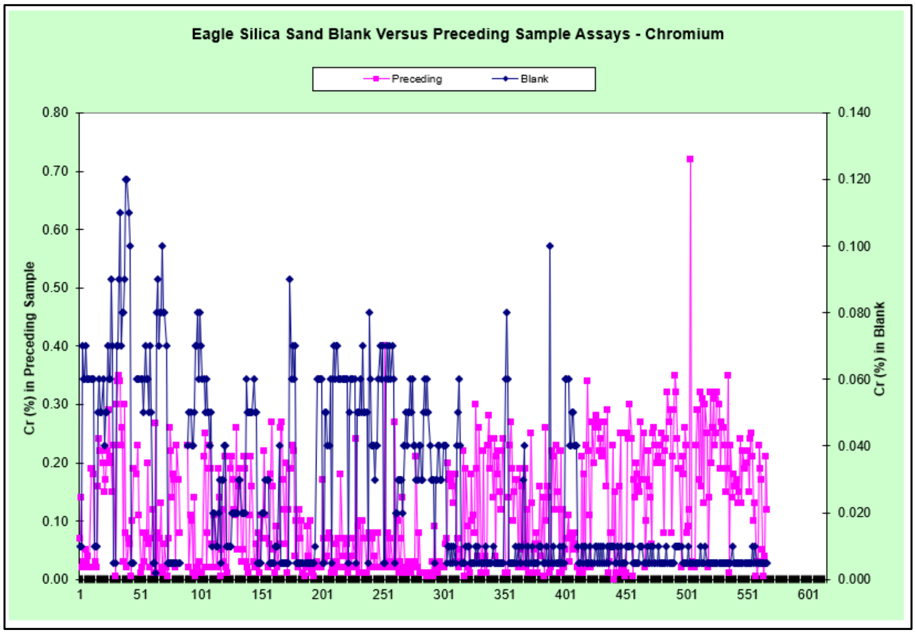


Figure 12.8: Cr Values in QA/QC Blanks

12.2.6 Standards

Eagle Mine has used up to seven different standards in the past, of which four are still used. The four were custom-made for the mine site and are shown in Table 12.3. Standards are inserted at a rate of one in thirty and correspond to rock types. It was noted that within the Eagle Mine Standards QA/QC spreadsheet, the mean value for Copper in EA-1 and Cobalt for EA-2 differed from the Certificate of Assay (COA) values produced by Smee and Associates for Eagle Mine. Eagle Mine uses a threshold of two standard deviations from the mean standard value on plots to gauge lab bias; however, as mentioned previously, it is at the discretion of the Senior Geologist to determine whether to trigger a sample or batch re-assay.

Figure 12.9 provides a graphical history of over 400 EA-2 standard samples assayed for nickel, and Figure 12.10 depicts the same QA/QC control graph for over 550 EA-1 standard samples assayed for gold.

Table 12.3: Summary of Mean Grades for Certified Reference Materials

CRM	Expected Grades						
	Au (g/t)	Pt (g/t)	Pd (g/t)	Co (%)	Cu (%)	Ni (%)	S (%)
EA-1	0.050	0.073	0.054	0.020	0.429	0.517	2.750
EA-2	0.100	0.185	0.119	0.033	0.949	1.100	5.920
EA-3	0.102	0.316	0.193	0.062	1.660	2.380	12.220
EA-S	0.171	0.503	0.289	0.065	1.771	2.308	12.368

COA: 2006 Smee & Associates

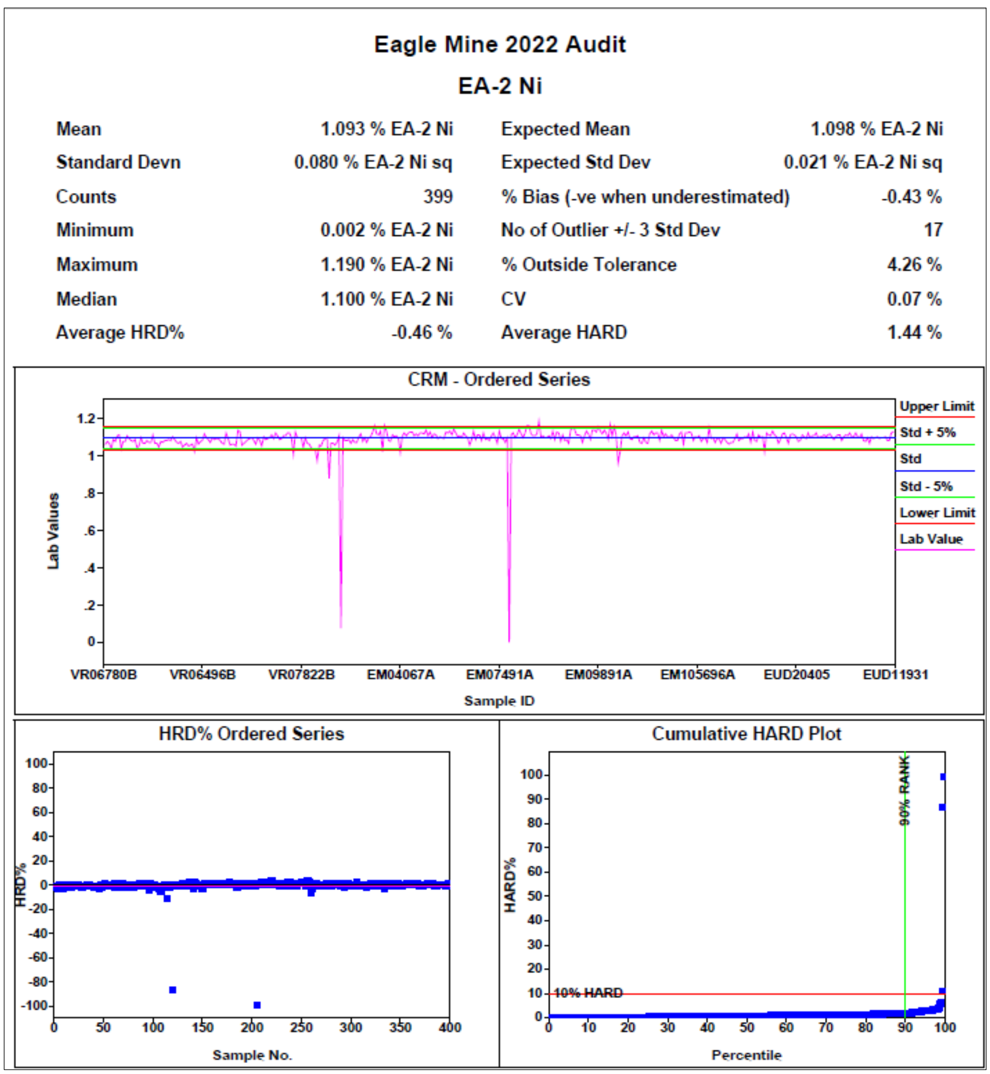


Figure 12.9: QA/QC Ni Values for Eagle Standard EA-2

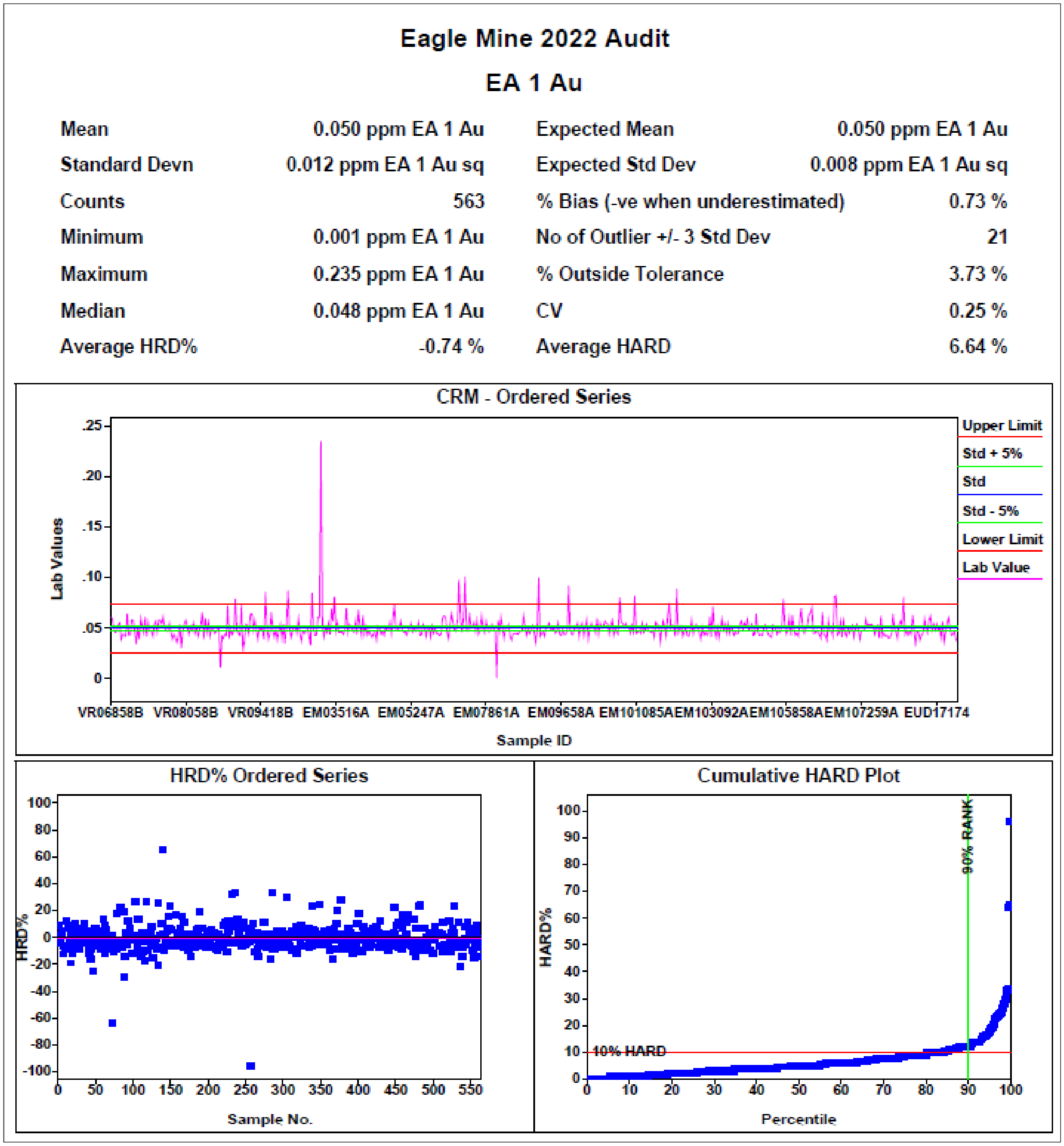


Figure 12.10: QA/QC Au values for Eagle Standard EA-1

The QA/QC insertion rate of one in thirty is consistent with industry standards for mature drilling programs. The QP finds the QA/QC program meets industry standards.

12.2.7 Drill Collar Inspection

At Eagle Mine, the last surface diamond drill hole was completed in 2019, with all subsequent drilling occurring from underground drill stations. Prior to 2019 and since, Eagle Mine has pursued diligent reclamation of most surface drill sites (See Figure 12.11) as part of its legislative requirements.

Figure 12.11: Current and Rehabilitated Former Drill Hole Collar Locations

Three surface drill hole collars were located and surveyed using a handheld Global Positioning System (GPS) unit (Garmin GPSMAP 62S). See Table 12.4 for a comparison of the results. Eagle Mine uses only UTM NAD 83 Zone 16 datum with mean sea level as 0 RL elevation.

Table 12.4: Comparison of Surface Drill Hole Collar Coordinates

	Hole ID	Easting	Northing	Elevation
Golder GPS	16EA341	433750.0	5176932.0	444.1
Eagle Mine Survey		433746.9	5176930.0	437.9
Difference		3.1	2.0	6.2
Golder GPS	15EA336	433444.0	5176963.0	444.4
Eagle Mine Survey		433446.7	5176963.0	435.1
Difference		-2.7	0.0	9.3
Golder GPS	15EA337	433544.0	5176943.0	445.9
Eagle Mine Survey		433545.0	5176944.3	437.6
Difference		-1.0	-1.3	8.4

GPSMap62
NAD 83 Zone 16

The results demonstrate a close validation of the mine survey collar coordinates. Handheld GPS elevation values are barometer-based and can be affected by changing weather fronts. The QP finds no issues with the mine surface collar coordinates.

12.2.8 Underground Geology

The QP traveled underground at Eagle to review the interpreted geology and mineralization. An active stope and drift and fill location in Eagle East were visited. The Keel was not visited due to mining activity. The observed geology and mineralization are consistent with the general interpretation of the mineral domains supporting the resource (Figure 12.12). The underground paper mapping was also referenced and judged to accurately represent the observed geology. Stope sampling, drift wall sampling, and muck pile sampling all occur to support short- and mid-term mine production. Samples taken during production mining are sent to an SGS contract laboratory located at the Humboldt Mill, for base metal analysis. No precious metals are analyzed. The underground samples are used strictly for grade control and are not used in the resources estimation. Eagle staff suggested that there is one sample for every two hundred tonnes of production.

Figure 12.12: Eagle East 515 Zone 3 Lift 2 MSU, Mineralized Peridotite, and Siltstone Contact

12.2.9 Mining

WSP Mining QP Khalid Mounhir completed a two-day site visit in February 2026. During the site visit, the Qualified Person (QP) completed both surface and underground inspections of the Eagle mine. The QP also reviewed the reserves estimation procedures with the long-term mining engineer and verified the design and planning data.

The underground tour included a visit to:

- A development face at the Upper Keel ramp,
- Both longitudinal and transverse stopes,
- The drift-and-fill face
- A stope in the CRF filling phase,
- The Escape Way and a portable refuge,
- Sections of the ventilation system.

During the surface site visit, the following was verified:

- UG mine portal location, including Eagle mine access and the active underground stoping operations
- Ore stockpile locations and truck loading facilities underground
- Potential for staged expansion and reclamation
- CRF plant and surface ventilation fans location

12.2.10 Geotechnical

The geotechnical QP has reviewed the available geotechnical data and design assessment work. The details and conclusions of the review are presented in Item 16.3.

12.3 Metallurgy and Mineral Processing

The WSP metallurgical Qualified Person (QP) reviewed testwork data, mill design documents, process plant performance, forecasts, and engineering studies for the mineral processing facility.

The QP visited the Humboldt Mill on February 26, inspecting the operational facilities from ore receiving through to concentrate production. The site visit also included a visit to the onsite laboratories, control rooms, water treatment facilities, and the tailings pond nearby, all of which were observed to be in normal working order. Additionally, a new High-Pressure Slurry Ablation (HPSA) unit was identified within the mill and is undergoing commissioning tests. During the visit, several key operations staff were interviewed and demonstrated both competence and substantial expertise.

12.4 Site Infrastructure

The QP, Ibrahim Karajeh, completed a general technical review of the background information related to site infrastructure. The review included a variety of engineering narratives that detail the design and configuration of the site infrastructure components. These narratives included site plans, layouts and general arrangement drawings, schematics and diagrams, and descriptive text. The scope of the review covered off-site infrastructure, including the site's access and proximity to transportation networks; grid electrical power; and water bodies for fresh water feed and excess discharge. The scope also covered on-site infrastructure including site grading, drainage, and surface water management; within-site transportation; electrical power distribution; water storage and distribution; fuel storage; and ancillary facilities, including water treatment, mine administration, dry, compressor house, truck shop, and truck wash.

The purpose of the review was to verify the adequacy of infrastructure to support and sustain the operation throughout the life of the mine. The Site Infrastructure QP has not participated in the site visit. However, observations collected by participants in the site visit were used to verify the data and information provided in the material that was subject to the desktop review.

12.4.1 Tailings

QP Jason Obermeyer's data verification focused on confirming that tailings management at the Mill site is in general accordance with accepted industry practice and that sufficient capacity exists in the HTDF to contain the tailings that are projected to be produced through the remaining LOM. The QP did not participate in the site visit. However, the QP serves as the Engineer of Record for the HTDF and has visited the site annually (at a minimum) since 2019, most recently in October 2025. As such, the QP had considerable prior understanding of the design and operation of the HTDF.

12.4.2 Water Management

QP Devin Castendyk's data verification focused on confirming that prior technical reports demonstrate methodological soundness and internal consistency. The QP did not participate in the site visit. However, the QP has provided consulting support for water management at the Mine site and the Mill site since 2016 and has previously visited the Mine site and the Mill site numerous times. As such, the QP had considerable prior understanding of water management for the project.

12.4.3 Environmental, Permitting, and Community Impact

QP Devin Castendyk's data verification focused on confirming consistency with permitting and design requirements, reviewing environmental studies (including model inputs and results), reviewing monitoring data, and reviewing agency and stakeholder engagement that pertained to environmental and social issues. The QP did not participate in the site visit. However, the QP has provided environmental and permitting support for the Mine site and the Mill site since 2016 and has previously visited the Mine site and the Mill site numerous times. As such, the QP had considerable prior understanding of environmental, permitting, and social or community aspects of the project.

12.5 QP Comments on Section 12

12.5.1 Database, Geology, and Mineral Resources

On completion of the data verification process for Eagle Mine, it is the opinion of the QP that the geological data collection, analytical methods, QA/QC, and chain of custody procedures used by Eagle Mine are consistent with CIM best practice guidelines and that the data is of sufficient quality to support the MRE disclosed in Item 14 of this Report.

12.5.2 Mining

QP Mounhir considers that the data supporting the Mineral Reserves are reliable and adequate for the purposes used in the Report.

12.5.3 Metallurgy and Mineral Processing

QP Jin considers that the data supporting the metallurgy and mineral process designs are reliable and adequate for the purposes used in the Report.

12.5.4 Utilities, Onsite Buildings and Off-site Infrastructure

QP Karajeh considers that the data supporting the Project infrastructure are reliable and adequate for the purposes used in the Report.

12.5.5 Tailings

QP Obermeyer considers that the data supporting the tailings disposal facility design and operation are reliable and adequate for the purposes used in the Report.

12.5.6 Water Management

QP Castendyk considers that the data supporting the water management are reliable and adequate for the purposes used in the Report.

12.5.7 Environmental

QP Castendyk considers that the data supporting the environmental permitting are reliable and adequate for the purposes used in the Report.

13. Mineral Processing and Metallurgical Testing

13.1 Mineralogy

Two styles of mineralization have been identified for Eagle Mine, namely Massive Sulfide (MSU) that is predominantly made up of sulfide minerals and Semi Massive (SMSU) composed of disseminated sulfides in ultramafic gangue. Eagle Keel is a lower-grade version of Eagle East mineralization.

13.2 Sampling And Mineralogical Analysis

Figure 13.1 illustrates the location of the drill holes for the samples used in metallurgical testing and confirms the spatial representativeness of these drill holes in the Eagle East deposit.

Table 13.1 lists the Eagle East composite samples and assays. Four representative composite samples of Eagle East drill core were selected from four material types consisting of MSU, SMSU, High Copper Massive Sulfide (CMSU), and waste. Composites were selected to be representative of the average grade of all available core from each composite zone. The waste rock composite was selected from drill samples adjacent to potential ore to best represent potential dilution in the mining process.

Table 13.1: Eagle East Composite Samples and Assays

Composite Sample	F_{80} (µm)	%Ni	%Cu	%S	%Fe	%MgO
MSU	1 166	8.01	5.03	33.2	48.7	0.45
SMSU	1 230	2.65	2.17	13.1	25.7	17.7
CMSU	951	6.49	14.2	31.1	42.5	0.24
Waste	1 303	0.68	0.86	3.56	14.0	13.0

Note. F_{80} – passing size before grinding

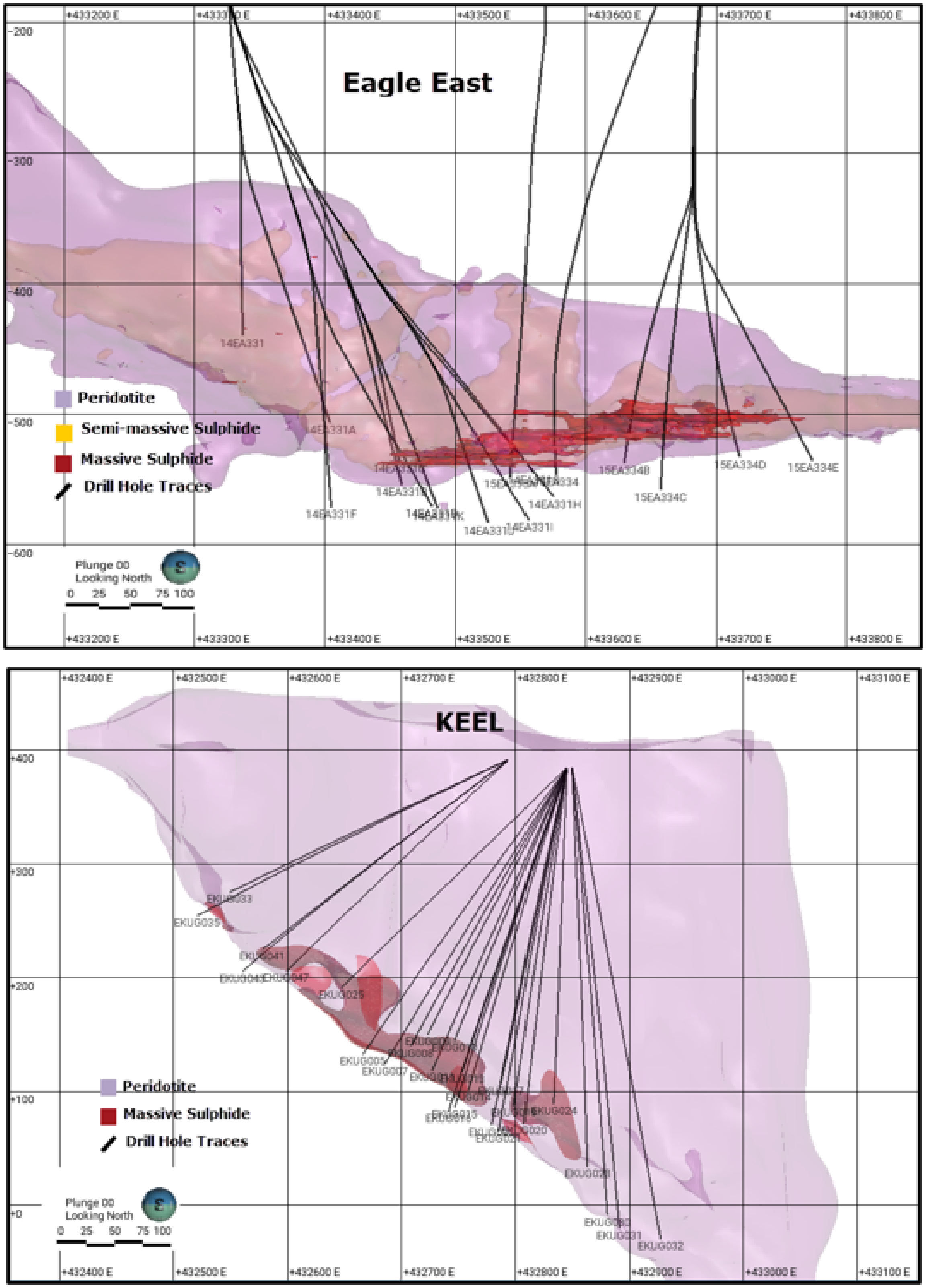


Figure 13.1: Location of Metallurgical Drill Holes and Samples at Eagle East and Keel

Nickel and copper mineralization in Eagle East samples are comprised of pentlandite (Pn) and chalcopyrite (Cp), respectively (XPS, 2017a). Pyrrhotite (Po), serpentine, pyroxene, plagioclase, olivine, amphibole, and iron oxides are considered gangue minerals. There were no minerals found in the Eagle East samples that are not known in the Eagle ore.

The Po/Pn ratio for Eagle East material is lower than that for Eagle MSU and SMSU samples due to the higher Pn grades and equivalent or lower Po grades (Table 13.2). Higher sulfide content was observed in the Eagle East samples. Higher grades and lower Po/Pn ratios are favorable and may present opportunities to achieve higher concentrate grades at equivalent recoveries.

Table 13.2: Pyrrhotite/Pentlandite Ratios in Eagle and Eagle East Samples

Sample	Eagle	Eagle East
MSU	3.9	2.2
SMSU	3.4	2.8
CMSU	n/a	2.0

X-Ray Diffraction (XRD) analysis of MSU, SMSU, and CMSU samples indicated a range of proportions of monoclinic and hexagonal pyrrhotite are present in the ores, which may impact the flotation performance of the mineral.

Eagle Keel samples are similar to those observed in Eagle East samples. Pentlandite primary association is with pyrrhotite, followed by the non-sulfide gangue (NSG), then chalcopyrite.

Waste rock adjacent to Eagle East mineralization is similar in mineralogy to NSG found currently in Humboldt Mill feed and may be classified as a pyroxenite, as opposed to the peridotite found around the Eagle deposit.

Platinum group metal (PGM) grades are higher in Eagle East material in comparison to Eagle ore. Preliminary mineralogical analysis shows inclusions of several PGM minerals within other sulfides present in the material. The size of the inclusions ranges from 10 µm to 100 µm. The following minerals were identified as being present in Eagle East material: maslovite (Pt-Bi- Te), michenerite (Pd-Bi-Te), sperrylite ($PtAs_2$), silver telluride (Ag-Te), volynskite (Ag-Bi-Te), and electrum (Au-Ag). The platinum and palladium minerals would be recoverable through conventional flotation and may benefit from the use of co-collectors along with xanthate to increase recoveries. The presence of silver requires further metallurgical analysis and testing to assess the potential for recovery.

13.3 Grinding Test Work

Grinding test work was completed on Eagle East ore samples to determine if the mineralization could be processed through the Humboldt Mill grinding circuit without circuit modification. For onsite testing, samples of Eagle and Eagle East ores were subjected to batch grinding tests under identical conditions, and the particle size distribution of the products was analyzed. At XPS Consulting & Testwork Services (XPS), Eagle East core samples were submitted for Bond Ball Mill Work Index testing to confirm the onsite test results.

Core samples were crushed to 100% passing 10 mesh (2 mm) in stages in a laboratory jaw crusher. The samples were then mixed and split into 1 kg charges using a rotary splitter.

Eagle core samples that had been previously crushed to 100% passing 2 mm were used as baseline samples for comparison to Eagle East samples. The size distribution of each crushed composite sample was determined, and the material assayed (refer to Table 13.1), and the 80% passing size (P_{80}) was determined.

The 80% passing size of samples was determined before grinding (F_{80}) and after grinding (P_{80}), and the reduction ratio, F_{80} / P_{80}, was calculated for different material types and blends of MSU to SMSU samples. The grinding test results can be summarized as follows:

- Reduction ratios for the Eagle East SMSU composite and 2:1 (MSU:SMSU) blend were both within 20% of the reduction ratios obtained for Eagle ores.
- The Eagle East MSU sample showed higher reduction ratios than Eagle MSU ore, indicating that the Eagle East MSU sample was less competent. Therefore, it will be possible to treat Eagle East mineralization in the Humboldt Mill grinding circuit and achieve equivalent product size with potential upside when processing MSU.
- Rosin-Rammler modeling of size distributions and comparison showed similar grinding performance for Eagle and Eagle East samples.
- Batch grinding tests showed that the grindability for the Eagle East mineralization is similar to or higher than that of Eagle samples.
- Bond Ball Mill Work Index results for Eagle East samples were comparable to historical Eagle results.
- Problems are not anticipated when processing Eagle East material in the current grinding circuit at processing rates similar to current operations.

Also, SGS had tested one Eagle Keel sample of 30 kg. The standard work index test results were in metric units:

- Rod Mill Work index RWi = 16.5 kWh/t and Ball Mill Work index BWi = 19.2 kWh/t.
- Further, XPS performed a liberation study on Eagle Keel samples and reported that locked particle associations for Keel are similar to those observed in Eagle East samples.

13.4 Flotation Test Work

A series of samples from Eagle, Eagle East, and Eagle Keel were subjected to batch flotation tests in the metallurgical laboratory at the Humboldt Mill to determine if the Eagle East and Keel samples have comparable overall recoveries and kinetics to Eagle ore. For onsite testing, batch flotation tests on both Eagle and Eagle East composite samples were completed. At XPS, a comprehensive program of flotation testing (batch tests, locked cycle tests, copper/nickel separation, and mineralogy) on Eagle East composite samples was completed.

Coarse rejects from drill core samples were used for Eagle East flotation test work. These samples were not used in the grinding test work because the size distribution of the samples was considered questionable due to the presence of a large proportion of fines. A larger proportion of fines could also bias the flotation tests and provide less than optimal results.

Batch rougher flotation tests were conducted on all material types in addition to the 2:1 (MSU:SMSU) blends from Eagle and Eagle East samples. Cleaner flotation tests were also carried out on 2:1 blends from Eagle and Eagle East samples.

Eagle samples were collected from core samples representing the first year of Eagle's mine life. The following material types and blends were tested: MSU, SMSU, CMSU (from Eagle East), and 2:1 (MSU:SMSU), and the head grades of the samples are shown in Table 13.3.

Table 13.3: Average Head Grades for Flotation Test Work

Composite Sample	%Ni	%Cu	%S	%Fe	%MgO
Eagle Keel	1.78	0.94	8.11	18.8	15.6
Eagle East					
MSU	8.01	5.03	33.2	48.7	0.45
SMSU	2.65	2.17	13.1	25.7	17.7
CMSU	6.49	14.2	31.1	42.5	0.24
2:1 (MSU:SMSU)	5.97	3.44	25.2	39.5	6.92
Eagle					
MSU	6.39	5.39	33.42	51.5	0.12
SMSU	2.19	1.90	12.31	25.8	15.87
2:1 (MSU:SMSU)	4.78	4.39	27.55	42.4	5.03

Flotation testing was carried out using reclaim water from the HTDF, rather than plant process water, to avoid any variation that would be introduced by changes in process water chemistry.

Table 13.4 shows the grades and recoveries for the batch rougher flotation tests conducted on the Eagle, Eagle East, and Keel samples. Mass pulls and metal recoveries were comparable for each sample pair, and metal recoveries were similar to those observed for Eagle ores. As expected, the nickel recovery varies with material type, and the copper recovery achieved was greater than 97%. Eagle East CMSU material would require significant blending with other ore types to lower copper grades in the mill feed to meet plant capabilities.

Table 13.4: Batch Rougher Flotation Test Results

Sample	Mass Recovery (%)	Concentrate Grade (%)		Recovery (%)	
		Ni	Cu	Ni	Cu
Eagle Keel	17.4	8.9	5.3	86.5	96.3
MSU					
Eagle	91.3	6.8	5.8	97.1	98.2
Eagle East	92.6	8.4	5.4	97.8	98.5
SMSU					
Eagle	31.7	6.0	5.8	86.2	97.5
Eagle East	28.4	8.4	6.6	87.8	97.4
2:1 (MSU:SMSU)					
Eagle	65.6	6.6	6.5	92.7	98.1
Eagle East	69.4	8.0	5.0	92.0	97.7
CMSU					
Eagle East	90.0	6.7	15.0	91.1	98.4

Flotation kinetics show that the recovery of nickel over time for each test sample indicated that Eagle Keel and Eagle East mineralization are similar to Eagle ore and can be processed in the Humboldt Mill.

13.5 Grade-Recovery Relations

The modeled nickel recovery to bulk cleaner concentrate has been revised in 2025 based on enhanced mill performance data collected over the past year. Recovery estimates for copper and nickel have been updated using data from March 2022 through February 2025. March 2022 was selected as the starting point, as it marks the period when the mill began targeting a 12% concentrate grade.

13.5.1 Bulk Nickel Recovery

The equation in Table 13.5 for the nickel recovery to bulk concentrate is based on the nickel grade of the ore and the concentrate grade targets. Adjustments were added for variation in nickel and copper grade in the nickel concentrate. The adjustments are 0.6% recovery lost per percent increase in nickel grade and 0.3% per percent decrease in recovery per percent increase in copper grade in the nickel concentrate. A 1% adjusting factor has been included to account for the additional recovery expected from the High-Pressure Slurry Ablation (HPSA) unit that is currently being commissioned.

13.5.2 Bulk Copper Recovery

The updated bulk recovery for copper is shown in the equation Table 13.5. The same data used for the nickel model was used to model the bulk copper recovery. A 0.5% adjusting factor has been added to account for the additional recovery expected from the HPSA unit that is currently being commissioned.

Table 13.5: Metallurgical Bulk Flotation Recovery Formulas (2025)

	Nickel Recovery (%)	Copper Recovery (%)
Bulk Flotation		
Eagle East	$= 1 + \frac{95.9585 * Ni\ Head\ Grade}{0.202399 + Ni\ Head\ Grade} + (12 - Ni\ Grade\ in\ Ni\ Con) * 0.6 + (2.2 - Cu\ Grade\ in\ Ni\ Con) * 0.3$	$= 0.5 + 99.2368 * \frac{Cu\ Feed\ Grade}{(0.0495488 + Cu\ Feed\ Grade)}$
Keel	$= 1 + \frac{95.9585 * Ni\ Feed\ Grade}{0.202399 + Ni\ Feed\ Grade} + (12 - Ni\ Grade\ in\ Ni\ Con) * 0.6 + (2.2 - Cu\ Grade\ in\ Ni\ Con) * 0.3$	$= 0.5 + 99.2368 * \frac{Cu\ Feed\ Grade}{(0.0495488 + Cu\ Feed\ Grade)}$
Eagle	If Ni Head Grade < 1.5242%: $= 1 + \frac{92.1271 * Ni\ Head\ Grade}{0.176766 + Ni\ Head\ Grade} + (14 - Ni\ Grade\ in\ Ni\ Con) * 0.6 + (3 - Cu\ Grade\ in\ Cu\ Ni\ Con) * 0.3$ If Ni Head Grade ≥ 1.5242%: $= 1 + 90 - 19.6567 * e^{-0.63681 * Ni\ Head\ Grade} + (14 - Ni\ Grade\ in\ Ni\ Con) * 0.6 + (3 - Cu\ Grade\ in\ Cu\ Ni\ Con) * 0.3$	If Cu Head Grade < 1.3673%: $= 0.5 + \frac{99.7364 * Cu\ Head\ Grade}{0.071729 + Cu\ Head\ Grade}$ If Cu Head Grade ≥ 1.3673%: $= 0.5 + 98.5 - 11.1274 * e^{-0.798395 * Cu\ Head\ Grade}$

13.6 Eagle Keel Ore Characterization and Discussion

Historical test programs have covered various ore zones, including Eagle, Eagle East, and the Keel. Through past production and performance monitoring, the mill operation has developed a solid understanding at the production level of the variation in ore characteristics of these different zones.

As illustrated in Figure 13.2, Eagle Keel ore is projected to comprise approximately 66% of total mined material over the remaining life of mine (LoM), based on the latest mine plan. Eagle Keel will serve as a primary source of ore production, particularly following the year 2026.

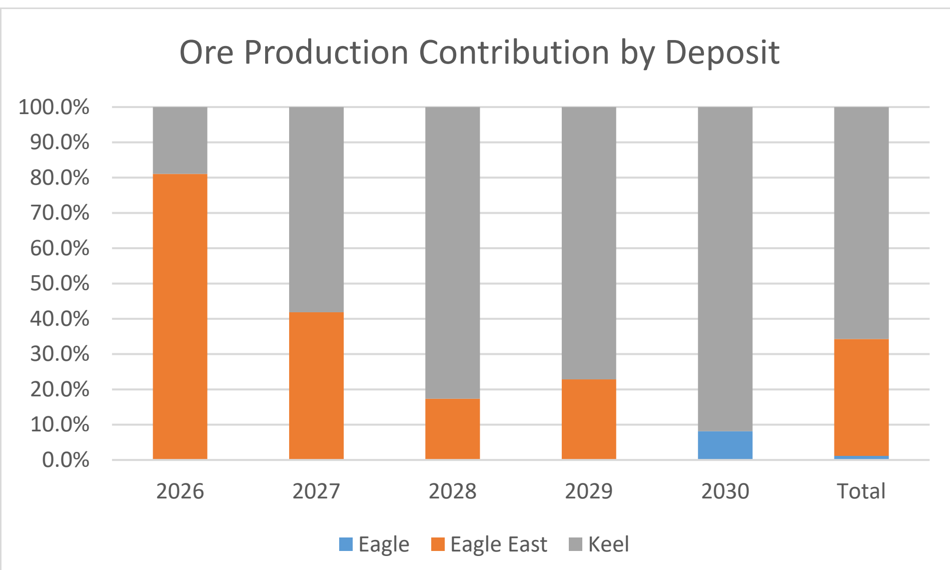


Figure 13.2: LOM Ore Production Contribution by Deposit

The comparison of Keel ore with other ore and the likelihood of its impact on metallurgical performance is discussed below:

- Keel ore is harder and more competent than Eagle East ore according to SGS grindability tests, which may lead to variation in power draw and ore throughput in the ball mill compared to historical ores.
- Locked particle associations for the Keel are similar to those observed in Eagle East samples.
- Ni and Cu head grades are lower than Eagle and Eagle East Feeds.
- It might be beneficial to increase the xanthate dosage to encourage pyrrhotite flotation in the roughers.

Eagle Keel ore behaves similarly to the SMSU ores but with lower grades, more talc and pyroxene, and slightly lower Ni liberation. Cu-Ni separation remains excellent.

14. Mineral Resource Estimates

This MRE represents an update to the December 31, 2022, MRE disclosed in the February 22, 2023, National Instrument 43-101 Technical Report titled "NI 43-101 Technical Report on the Eagle Mine, Michigan, U.S.A." It provides an update for the Eagle, Eagle East, and Keel deposits.

The Mineral Resources update for Eagle Mine has been prepared by Eagle Mine technical staff, using both historical and recent drilling results, in accordance with NI 43-101 and following the requirements of Form 43-101F1. The Mineral Resources estimate follows the CIM Estimation of Mineral Resources and Mineral Reserves Best Practice Guidelines (2019) and was classified following the CIM Definition Standards for Mineral Resources and Mineral Reserves (2014). The QP for this MRE is Mr. Brian Thomas, P. Geo, an independent QP, as defined under NI 43-101, and an employee of WSP based in Sudbury, Ontario, Canada. The Effective Date of this Mineral Resources estimate is February 28, 2026.

Eagle Mine currently consists of three deposits (Eagle, Eagle East, and the Keel), and the geological interpretations and MRE outlined in the following sections were derived from drill hole data, underground mapping, and geological models provided by Eagle Mine technical staff, using Seequent Leapfrog Edge™ and Maptek Vulcan Geomodeler™ software.

14.1 Key Assumptions and Data Used in the Estimate

14.1.1 Drill Hole Data

The Eagle Mine drill hole database that supports the updated MRE includes collar, downhole survey, assay, and lithology data. The elements and oxides of interest included in the assay data are Cu, Ni, Co, Ag, Au, Pt, Pd, S, Fe_2O_3, MgO, Cr, Zn, TiO_2, SiO_2, as well as bulk density measurements. Drill hole data is stored in an acQuire relational database and was exported as CSV files on December 12, 2024, for the purposes of this update. Summary statistics of available drill holes in the Eagle Mine drill hole database are provided in Table 14.1.

Table 14.1: Summary of Eagle Drill Hole Database December 12, 2024

Drilling Type	Number of Drill Holes	Total Meterage (m)	Number of Samples	Average Depth of Drill Holes (m)
DDH (Surface and Underground	1,516	447,696	38,641	295

Within the database and for the purposes of Mineral Resources estimation, unassayed values within the mineral wireframes were assumed to be waste and assigned a metal value of one-half the detection limit (of the determining methodology currently used) as shown in Table 14.2.

A total of 7 drill holes containing 103 assays were drilled after the data cut-off date, accounting for 154.8 m of sample length. These intervals were determined to be not material to the MRE, but it is recommended that these intervals be included in the next model update.

Table 14.2: Element Half Detection Values

Element	Detection Limit
Ag	1 ppm
Au	0.001 ppm
Co	0.002%
Cu	0.002%
Ni	0.002%
Pd	0.001 ppm
Pt	0.001 ppm
S	0.01%

It is the opinion of the QP that the geological data collection, analytical methods, QA/QC, and chain of custody procedures used by Eagle Mine are consistent with CIM best practice guidelines and that the data are of sufficient quality to support the MRE disclosed in Item 14 of this report.

14.2 Geological Interpretation

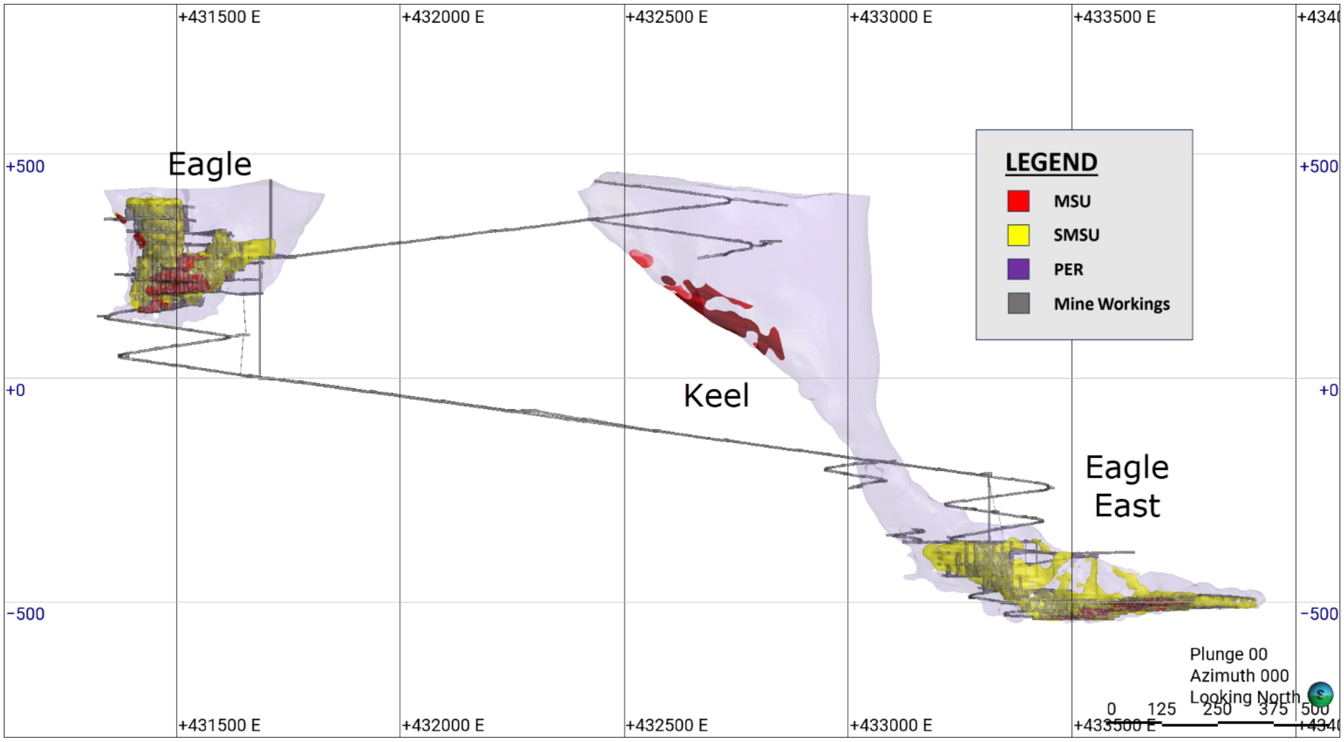
Wireframe solids representing the three deposits (Eagle, Eagle East, and Keel) were constructed primarily in Leapfrog Geo modeling software. The wireframes were generated by snapping to drill hole contacts utilizing the implicit modeling module and refining the final shapes by the use of interpretive polylines (structural trends) and underground mapping where applicable. Table 14.3 shows wireframe domains in each ore body.

Table 14.3: Wireframe Solids Utilized for Each Deposit

Geological Domains	Eagle	Eagle East	Keel
Siltstone	X	X	X
Gabbro		X	
Peridotite (<25% Sulfides)	X	X	
WPER (<0.4% Ni)			X
MPER (>0.4% Ni)			X
SMSU (25-85% Sulfides)	X	X	
MSU (>85% Sulfides)	X	X	X

The Eagle deposit (Figure 14.1) is predominantly a pod-like shape dominated by semi-massive sulfide (SMSU, 25-85% sulfide) with a central massive sulfide (MSU, 85-100% sulfide) core within a mineralized peridotite (PER) host.

The Eagle East deposit is an east-west trending lenticular shape dominated by a narrow, vertically oriented SMSU with a distinctly laterally flat, high tenor MSU. The Eagle East SMSU and MSU are hosted within mineralized peridotite proximal to the basal siltstone contact. The deposit is crosscut by a later gabbro dike trending southeast-northwest. Using Leapfrog Geo, the SMSU and PER domains were assigned a structural trend to accommodate the natural East/West bend in the intrusive unit. The MSU domain was given a global trend to accommodate its long and flat orientation.



*Source: Talon, 2026

Figure 14.1: Eagle, Eagle East, and Keel Deposits Looking North

The Keel deposit is located between Eagle East and Eagle deposits along the east-west-trending peridotite siltstone basal contact. The Keel exhibits as a thin trough-shaped accumulation of MSU (KMSU) along the mineralized peridotite/siltstone contact. While creating the geologic domains, the PER was assigned a structural trend to accommodate the natural East/West bend in the intrusive unit. The KMSU domain is modeled as a vein to accommodate its thin and curved orientation. See Figure 14.2 for the Keel and Eagle East deposit.

The metasediment (siltstone) country rock is non-mineralized and was not modeled for the purposes of this resource update.

14.3 Capping and Outlier Restrictions

14.3.1 Eagle

Previous versions of the Eagle (EA) model used grade capping top-cuts of 3.0 ppm Au, 3.5 ppm Pt, and 2.5 ppm Pd. The use of top-cuts was reviewed by analysis of histograms, cumulative distribution plots, and log-probability plots, and these values were considered reasonable and were not changed. In addition, a top-cut of 80 ppm for Ag was used for MSU and SMSU domains, while a top-cut of 20 ppm was used for the PER domain. Top-cuts were applied to samples after compositing. Table 14.4 shows the restrictions utilized in the Eagle deposit. In addition to these top-cuts, limits were placed on the radii of influence of high-grade samples as follows:

- In the MSU and SMSU domains, samples assaying greater than 10% Cu were constrained to 10% of the search ellipse distance.

- In the PER domain, a 10% distance limit was placed on samples greater than 1.0 g/t Au, 0.25 g/t Pd, 3 g/t Pt, or 3% Cu. A 5% distance limit was placed on samples greater than 3% Ni.

Table 14.4: Outlier Restrictions in Eagle Deposit

General		Outlier Restrictions		
Domain	Element	Method	Distance %	Threshold
Peridotite	Au ppm	Discard	10	1
Peridotite	Cu %	Discard	10	3
Peridotite	Ni %	Discard	5	3
Peridotite	Pd ppm	Clamp	10	0.25
Peridotite	Pt ppm	Clamp	10	3
MSU	Cu %	Discard	10	10
SMSU	Cu %	Discard	10	10

Notes: Discard indicates that Samples outside the Distance and above the Threshold are ignored.
Clamp indicates that Samples outside the Distance and above the Threshold are set to the Threshold value.
Distance indicates a % of the Search Distance Parameters.

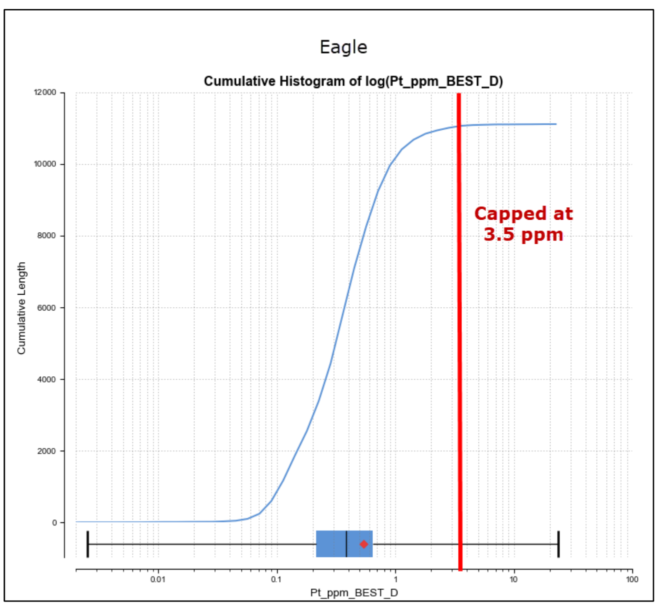


Figure 14.2: Cumulative Histogram of Pt Composites in SMSU Used in Determining Pt Top-Cut Value

Several methodologies were reviewed in the evaluation and determination of metal top-cut values. Figure 14.3 demonstrates the use of cumulative histograms in determining top-cuts for Eagle Pt values. Table 14.5 summarizes the top-cuts used in each of the different geological domains and shows the number of sample assays capped compared to the total number of samples.

Table 14.5: Number of Eagle Samples Affected by Top-Cuts

Domain	Samples	Elements			
		Ag	Au	Pd	Pt
Peridotite	Total	2581	6596	6609	6623
	Capped	3	8	2	6
MSU	Total	1434	2700	2702	2702
	Capped	35	78	209	174
SMSUE	Total	2187	5622	5622	5622
	Capped	6	27	9	39

14.3.2 Eagle East

The use of top-capping was reviewed by analysis of histograms, cumulative distribution plots, and log-probability plots. In addition, a comparison of estimated block grades with the input data was conducted. Outlier distance restriction was applied to all elements in the PER domain to limit the influence of high-grade samples along imperfect domain shape margins. See Table 14.6 for the restrictions utilized in Eagle East.

Table 14.6: Outlier Restrictions in Eagle East

General		Outlier Restrictions		
Domain	**Element**	**Method**	**Distance (m)**	**Threshold**
Peridotite	Ag ppm	Discard	10	7
Peridotite	Au ppm	Discard	10	0.2
Peridotite	Cu %	Discard	10	1.3
Peridotite	Ni %	Discard	10	1.6
Peridotite	Pd ppm	Discard	10	0.4
Peridotite	Pt ppm	Discard	10	0.5
Peridotite	S %	Discard	10	8
Peridotite	SG	Discard	10	3.4
MSU	Ag ppm	Discard	10	35
MSU	Au ppm	Discard	10	2
MSU	Cu %	Discard	10	10
MSU	Pd ppm	Discard	10	3

General		Outlier Restrictions		
Domain	**Element**	**Method**	**Distance (m)**	**Threshold**
MSU	Pt ppm	Discard	10	3.5
SMSU	Ag ppm	Discard	10	19
SMSU	Au ppm	Discard	10	5
SMSU	Co %	Discard	10	0.12
SMSU	Cu %	Discard	10	5
SMSU	Ni %	Discard	10	5
SMSU	Pd ppm	Discard	10	1.8
SMSU	Pt ppm	Discard	10	1.8
SMSU	S %	Discard	10	21
SMSU	SG	Discard	10	3.75

Notes: Discard indicates that Samples outside the Distance and above the Threshold are ignored.
Clamp indicates that Samples outside the Distance and above the Threshold are set to the Threshold value.
Distance indicates a % of the Search Distance Parameters.

14.3.3 Keel

The MPER domain in the Keel model uses grade capping top-cuts of 80 ppm Ag, 3.0 ppm Au, 3.5 ppm Pt, and 2.5 ppm Pd. The use of top-cuts was reviewed by analysis of histograms, cumulative distribution plots, and log-probability plots. In addition, a comparison of estimated block grades with the input data was conducted. Outlier distance restriction was also tested during the grade estimation. Outlier distance restriction was applied to all elements in the PER domain to limit the influence of elevated grades caused by sulfide veins. See Table 14.17 for the restrictions used.

Table 14.7: Outlier Restrictions in the Keel

General		Outlier Restrictions		
Domain	**Elements**	**Method**	**Distance (m)**	**Threshold**
Peridotite	Ag ppm	Discard	2	10
Peridotite	Au ppm	Discard	2	0.502
Peridotite	Co %	Discard	2	0.07
Peridotite	Cu %	Discard	5	1.6
Peridotite	Ni %	Discard	5	2.5
Peridotite	Pd ppm	Discard	2	1.342
Peridotite	Pt ppm	Discard	2	1.5
Peridotite	S %	Discard	2	20
Peridotite	SG	Discard	2	3.5

Notes: Discard indicates that Samples outside the Distance and above the Threshold are ignored.
Clamp indicates that Samples outside the Distance and above the Threshold are set to the Threshold value.
Distance indicates a % of the Search Distance Parameters.

14.4 Compositing

A 1.5 m composite length was used to standardize the sample length; this corresponds to the predominant sampling interval (see Figure 14.3).

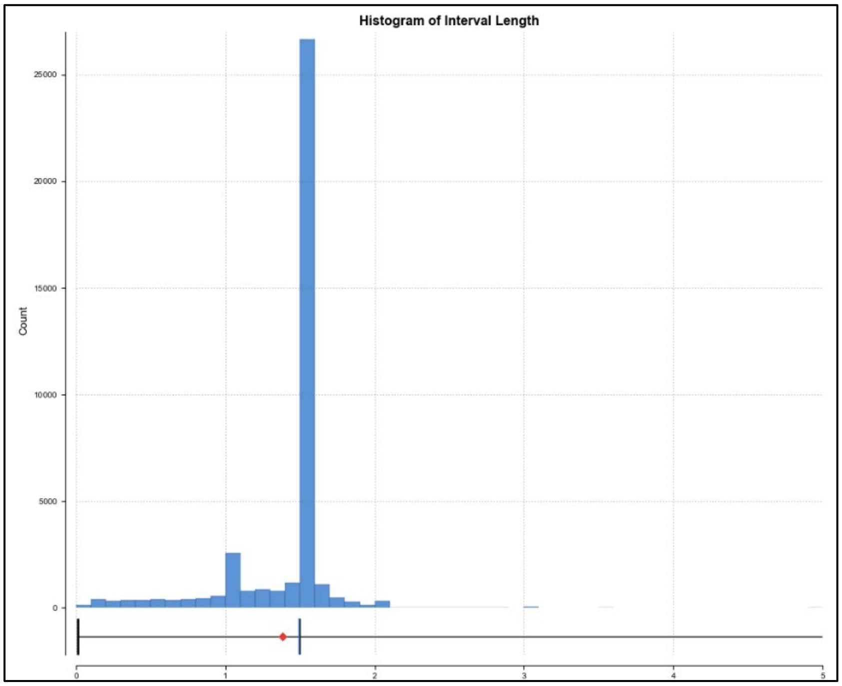


Figure 14.3: Histogram for Eagle Mine Sample Length

Compositing was carried out by domain. Residual composite segments were not distributed amongst other intervals or omitted; they were all included. Due to the lack of sampling in the sediment domain, any unsampled or unassayed intervals were assigned very low values (0.001) before compositing to prevent grade extrapolation into unsampled areas. Table 14.8, Table 14.9, and Table 14.10 present comparisons of raw assay data versus composites for the Eagle, Eagle East, and Keel deposits, respectively.

Table 14.8: Summary of Eagle Deposit Sample Statistics by Domain (weighted by length)

MSU										
Element	**Type**	**Ni %**	**Cu %**	**Co %**	**Au g/t**	**Pt g/t**	**Pd g/t**	**Ag g/t**	**S %**	**SG**
Count	Raw	2951	2951	2951	2679	2679	2679	1458	2951	2444
	Composite	2898	2896	2896	2700	2702	2702	1434	2898	2459
Minimum	Raw	0.06	0.11	0.00	0.01	0.01	0.00	1.00	0.83	2.53
	Composite	0.29	0.48	0.01	0.01	0.04	0.00	2.00	2.05	2.53
Maximum	Raw	8.07	22.80	0.24	18.80	27.00	14.70	169.00	44.70	4.99
	Composite	8.07	22.50	0.24	18.80	19.95	13.05	169.00	44.20	4.99
Mean	Raw	6.02	4.84	0.16	0.46	1.37	1.00	19.03	34.89	4.54
	Composite	6.02	4.83	0.16	0.46	1.37	0.99	19.05	34.89	4.54
Standard Deviation	Raw	0.71	3.05	0.03	0.98	1.43	1.20	18.26	2.54	0.19
	Composite	0.67	3.02	0.03	0.97	1.40	1.17	18.44	2.41	0.18
Coefficient of Variation	Raw	0.12	0.63	0.19	2.13	1.04	1.20	0.96	0.07	0.04
	Composite	0.11	0.63	0.19	2.10	1.02	1.18	0.97	0.07	0.04
SMSU										
Element	**Type**	**Ni %**	**Cu %**	**Co %**	**Au g/t**	**Pt g/t**	**Pd g/t**	**Ag g/t**	**S %**	**SG**
Count	Raw	6415	6415	6415	5515	5515	5515	2135	6384	2838
	Composite	6265	6265	6265	5622	5622	5622	2187	6245	2913
Minimum	Raw	0.08	0.06	0.01	0.00	0.00	0.00	0.50	0.09	1.64
	Composite	0.08	0.06	0.01	0.00	0.00	0.00	0.50	0.09	1.64
Maximum	Raw	11.75	21.80	0.18	15.50	23.60	9.76	106.00	36.10	4.87
	Composite	9.19	15.50	0.18	15.50	23.60	6.42	104.80	36.10	4.87
Mean	Raw	1.96	1.95	0.05	0.27	0.51	0.31	9.59	10.40	3.33
	Composite	1.96	1.94	0.05	0.26	0.51	0.31	9.47	10.37	3.33
Standard Deviation	Raw	0.69	1.22	0.02	0.56	0.71	0.35	10.08	3.65	0.21
	Composite	0.68	1.20	0.02	0.54	0.71	0.33	9.87	3.63	0.21
	Raw	0.35	0.63	0.35	2.10	1.38	1.11	1.05	0.35	0.06

Coefficient of Variation	Composite	0.35	0.62	0.35	2.05	1.39	1.07	1.04	0.35	0.06
PER										
Element	**Type**	**Ni %**	**Cu %**	**Co %**	**Au g/t**	**Pt g/t**	**Pd g/t**	**Ag g/t**	**S %**	**SG**
Count	Raw	7017	7020	7013	6478	6501	6488	2574	7022	2896
	Composite	7025	7025	7017	6596	6623	6609	2581	7027	2950
Minimum	Raw	0.00	0.00	0.00	0.00	0.00	0.00	0.50	0.01	1.07
	Composite	0.01	0.00	0.00	0.00	0.00	0.00	0.50	0.01	1.07
Maximum	Raw	7.27	13.10	0.22	43.10	43.40	5.39	6800	40.90	4.47
	Composite	7.27	12.90	0.22	43.10	35.47	5.39	6800	40.90	4.29
Mean	Raw	0.55	0.44	0.02	0.06	0.11	0.07	4.94	2.80	3.05
	Composite	0.55	0.45	0.02	0.06	0.11	0.07	4.92	2.81	3.05
Standard Deviation	Raw	0.36	0.40	0.01	0.35	0.54	0.12	138.68	2.17	0.18
	Composite	0.35	0.40	0.01	0.27	0.50	0.12	137.55	2.07	0.17
Coefficient of Variation	Raw	0.67	0.90	0.47	5.68	4.76	1.79	28.07	0.78	0.06
	Composite	0.64	0.89	0.44	4.36	4.32	1.75	27.97	0.74	0.05

Table 14.9: Summary of Eagle East Deposit Sample Statistics by Domain (weighted by length)

MSU										
Element	**Type**	**Ni %**	**Cu %**	**Co %**	**Au g/t**	**Pt g/t**	**Pd g/t**	**Ag g/t**	**S %**	**SG**
Count	Raw	453	453	453	450	453	453	453	453	99
	Composite	501	501	501	497	501	501	500	501	116
Minimum	Raw	0.18	0.07	0.00	0.00	0.00	0.00	0.50	0.96	3.61
	Composite	1.78	0.98	0.04	0.02	0.41	0.11	2.88	8.12	3.61
Maximum	Raw	10.65	18.20	0.24	9.71	12.15	15.55	91.00	38.90	6.06
	Composite	10.44	18.20	0.23	8.59	12.15	12.90	91.00	38.90	6.06
Mean	Raw	7.67	6.07	0.17	0.52	2.23	1.67	20.43	34.46	4.57
	Composite	7.65	6.09	0.17	0.55	2.23	1.67	20.51	34.42	4.57
Standard Deviation	Raw	1.06	3.12	0.03	0.98	2.02	2.22	14.35	2.77	0.22
	Composite	1.03	3.15	0.03	0.99	2.02	2.17	14.45	2.61	0.21
Coefficient of Variation	Raw	0.14	0.51	0.19	1.88	0.91	1.33	0.70	0.08	0.05
	Composite	0.13	0.52	0.18	1.80	0.90	1.30	0.70	0.08	0.05
SMSU										
Element	**Type**	**Ni %**	**Cu %**	**Co %**	**Au g/t**	**Pt g/t**	**Pd g/t**	**Ag g/t**	**S %**	**SG**
Count	Raw	1891	1891	1891	1885	1891	1891	1891	1891	290
	Composite	2076	2076	2076	2070	2076	2076	2076	2076	361
Minimum	Raw	0.06	0.05	0.00	0.00	0.01	0.01	0.50	0.91	2.63
	Composite	0.31	0.25	0.01	0.00	0.00	0.00	0.50	1.65	2.63
Maximum	Raw	9.16	8.65	0.19	7.40	10.00	8.48	53.00	35.40	5.11
	Composite	7.53	8.52	0.19	7.40	10.00	8.48	52.63	36.00	5.11
Mean	Raw	2.26	1.84	0.05	0.23	0.61	0.42	7.65	9.54	3.33
	Composite	2.24	1.81	0.05	0.22	0.61	0.42	7.54	9.48	3.34
Standard Deviation	Raw	1.05	1.08	0.02	0.38	0.59	0.50	5.20	4.32	0.22
	Composite	1.03	1.04	0.02	0.35	0.56	0.47	5.03	4.27	0.22
Coefficient of Variation	Raw	0.47	0.59	0.38	1.66	0.96	1.19	0.68	0.45	0.07
	Composite	0.46	0.57	0.38	1.56	0.92	1.12	0.67	0.45	0.07
PER										
Element	**Type**	**Ni %**	**Cu %**	**Co %**	**Au g/t**	**Pt g/t**	**Pd g/t**	**Ag g/t**	**S %**	**SG**
Count	Raw	7535	7534	7530	7523	7535	7535	6503	7535	2151
	Composite	9412	9411	9398	9386	9412	9412	7556	9412	3227
Minimum	Raw	0.01	0.01	0.00	0.00	0.00	0.00	0.50	0.02	1.81
	Composite	0.01	0.01	0.00	0.00	0.00	0.00	0.50	0.04	2.03
Maximum	Raw	8.06	13.00	0.21	24.30	13.15	7.64	116.00	37.80	4.55
	Composite	7.26	5.09	0.18	24.30	5.35	5.80	38.00	32.79	4.26
Mean	Raw	0.61	0.48	0.02	0.07	0.16	0.11	2.28	2.49	3.08
	Composite	0.57	0.44	0.02	0.06	0.14	0.10	2.16	2.27	3.06

Standard Deviation	Raw	0.40	0.35	0.01	0.30	0.17	0.13	1.87	1.84	0.15
	Composite	0.37	0.33	0.01	0.26	0.15	0.12	1.56	1.72	0.15
Coefficient of Variation	Raw	0.66	0.73	0.43	4.56	1.10	1.22	0.82	0.74	0.05
	Composite	0.66	0.74	0.41	4.49	1.04	1.20	0.72	0.76	0.05

Table 14.10: Summary of Keel Deposit Sample Statistics by Domain (weighted by length)

MSU										
Element	**Type**	**Ni %**	**Cu %**	**Co %**	**Au g/t**	**Pt g/t**	**Pd g/t**	**Ag g/t**	**S %**	**SG**
Count	Raw	53	53	53	53	53	53	36	53	24
	Composite	49	49	49	32	49	49	34	49	22
Minimum	Raw	0.16	0.09	0.01	0.02	0.02	0.02	0.50	0.60	2.51
	Composite	0.16	0.09	0.01	0.02	0.02	0.02	0.50	0.60	2.51
Maximum	Raw	9.79	5.31	0.22	0.33	3.03	1.33	26.00	37.70	4.61
	Composite	9.79	4.97	0.21	0.23	3.03	1.33	26.00	37.20	4.58
Mean	Raw	5.39	2.07	0.15	0.11	0.50	0.32	6.05	28.32	4.08
	Composite	5.32	2.04	0.15	0.09	0.53	0.34	5.95	27.87	4.05
Standard Deviation	Raw	1.77	0.86	0.05	0.07	0.47	0.26	3.80	8.19	0.53
	Composite	1.70	0.75	0.05	0.05	0.54	0.28	3.34	7.92	0.54
Coefficient of Variation	Raw	0.33	0.41	0.33	0.64	0.95	0.81	0.63	0.29	0.13
	Composite	0.32	0.37	0.33	0.59	1.03	0.84	0.56	0.28	0.13
MPER										
Element	**Type**	**Ni %**	**Cu %**	**Co %**	**Au g/t**	**Pt g/t**	**Pd g/t**	**Ag g/t**	**S %**	**SG**
Count	Raw	8277	8279	8275	8261	8280	8280	7126	8280	2717
	Composite	7603	7602	7597	7592	7603	7603	6572	7603	2124
Minimum	Raw	0.002	0.002	0.001	0.0005	0.0025	0.0005	0.5	0.005	1.81
	Composite	0.01	0.01	0.00	0.00	0.00	0.00	0.50	0.04	2.03
Maximum	Raw	10.10	17.65	0.21	24.30	13.15	10.50	116.00	37.80	4.80
	Composite	7.26	5.09	0.18	24.30	5.35	5.80	38.00	32.79	4.26
Mean	Raw	0.67	0.53	0.02	0.07	0.17	0.12	2.48	2.78	3.10
	Composite	0.61	0.48	0.02	0.07	0.16	0.11	2.27	2.49	3.08
Standard Deviation	Raw	0.67	0.62	0.01	0.30	0.29	0.23	2.83	3.05	0.23
	Composite	0.38	0.32	0.01	0.29	0.15	0.12	1.57	1.70	0.15
Coefficient of Variation	Raw	1.01	1.17	0.67	4.31	1.66	1.93	1.14	1.09	0.08
	Composite	0.61	0.67	0.40	4.47	0.96	1.12	0.69	0.68	0.05

14.5 Bulk Density

Eagle Mine bulk density measurements are determined by a certified laboratory (ALS) as part of the regular drill hole sampling program. The resultant values reside within the acQuire drill hole database. The bulk density is interpolated into domain model blocks via Ordinary Kriging (OK) with sample weighting based on modeled variography. Blocks that remain unestimated are filled with average domain values unique to each deposit. Table 14.11 displays the average domain values for each deposit at Eagle Mine.

Table 14.11: Average Bulk Density for Each Unique Domain

Domain	Eagle	Eagle East	Keel
	Density (g/cm^3)	Density (g/cm^3)	Density (g/cm^3)
Massive Sulfide (MSU)	4.51	4.51	4.51
Semi-massive Sulfide (SMSU)	3.35	3.35	
Peridotite (PER)	3.08	3.08	
MPER			3.14
WPER			2.97
Sediment (SED)	2.70	2.70	2.86

14.6 Variography

The spatial continuity of the capped composite grades, in each mineralized domain and for each orebody, was assessed using Leapfrog Edge software. A two-structure, spherical variogram was modeled for each domain as shown in the example in Figure 14.4. Contacts between the domains were defined as “hard” boundaries. Geometric anisotropy was determined for each domain and grade item from the contoured variograms, and subsequent ellipses were checked against the geological structure to confirm validity and alignment. Examples of the anisotropy and modeled variograms are shown in Figure 14.4 and Figure 14.5. All variogram models are on file at Eagle Mine. A table of resultant search ellipses and estimation parameters can be found below in Table 14.12, Table 14.13, and Table 14.14.

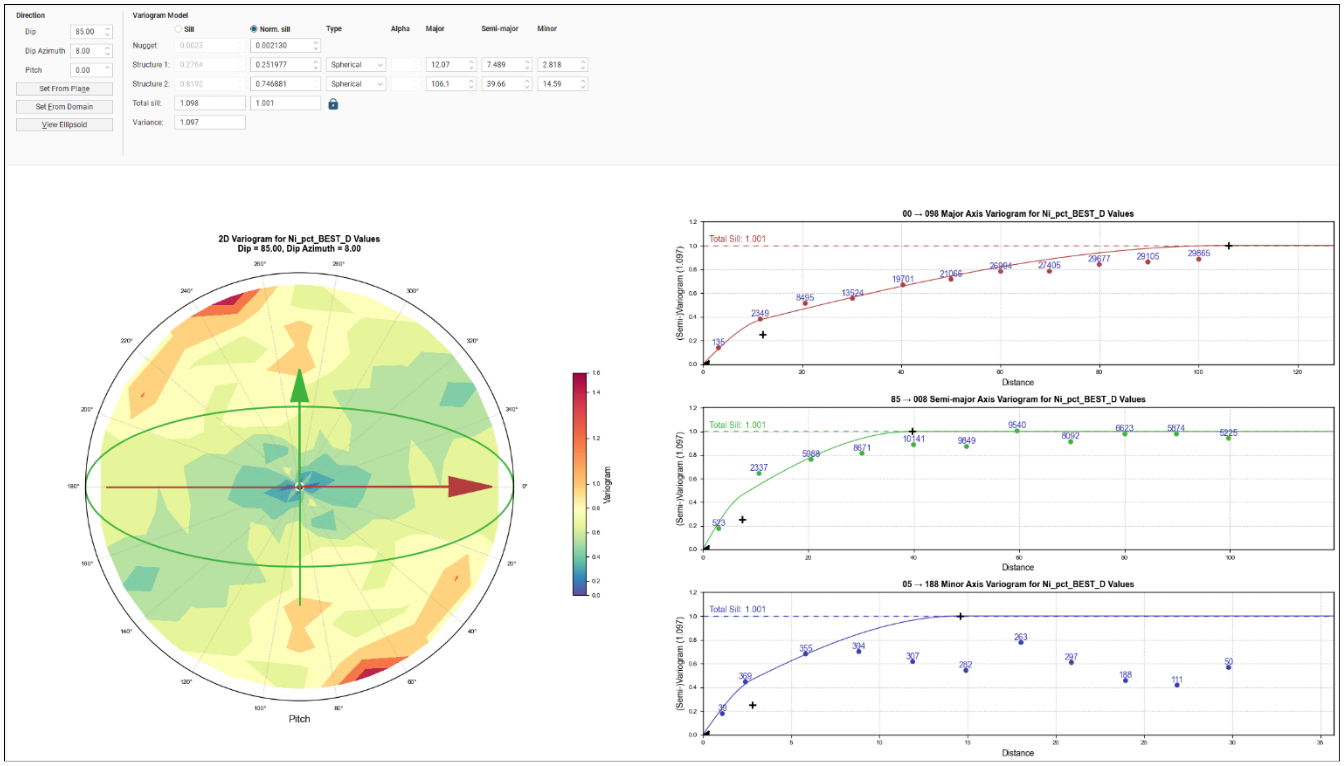
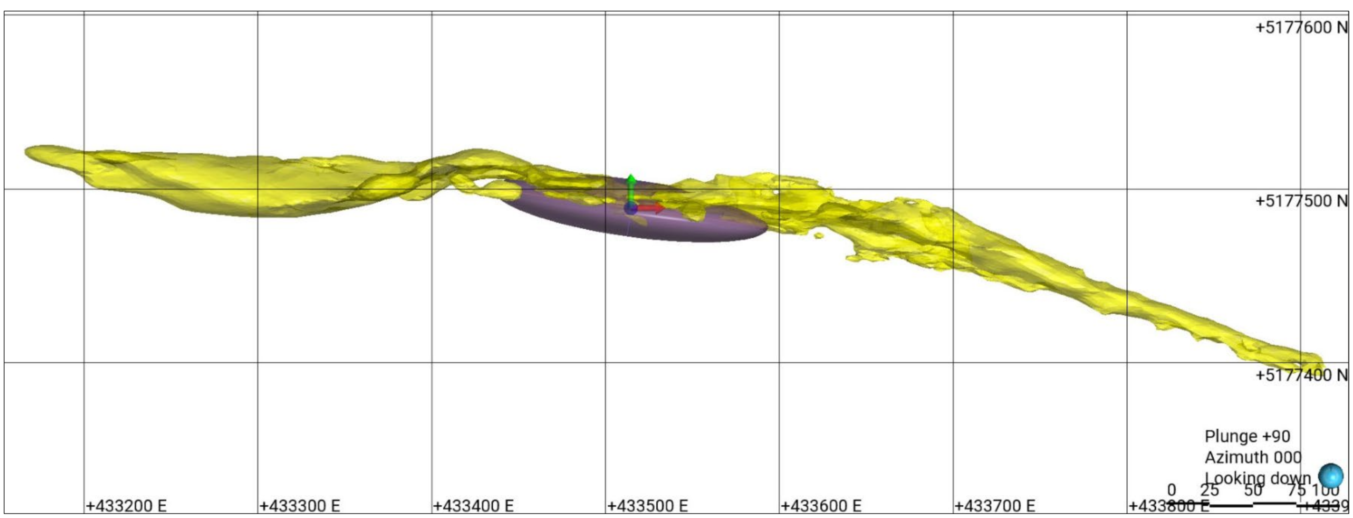


Figure 14.4: Eagle East SMSU Ni Variogram Model



*Source: Talon, 2026

Figure 14.5: Plan View of Eagle East MSU Domain Ni Grade Search Ellipse Derived from Variogram Model

14.7 Block Model Interpolations

All models at Eagle Mine use 5m x 5m x 5m parent cell blocks. The Eagle and Keel models sub cell to a 1m x 1m x 1m block size, whereas the Eagle East model is sub celled to a 2.5m(X) x 2.5m(Y) x 1.25m(Z) block size, reflecting the lateral nature of the mineralization. The sub-cells use parent cell grade values. No block rotations were utilized. Table 14.12 depicts block model extents and parameters for each deposit. The orientation, block sizes, and sub-celling applied to the Eagle deposits are reasonable for the geologic domains, the style of mineralization, and the mining methods employed.

Table 14.12: Block Model Extents and Parameters

Deposit	Co-ordinate	Origin (UTM)	Extents (m)	Parent Cell Size (m)	No. of blocks	No. of Subcell Splits	Minimum Cell Dimension (m)
Eagle	Easting (X)	431,325	550	5 m	110	5	1
	Northing (Y)	5,177,450	200	5 m	40	5	1
	Elevation (Z)	100	350	5 m	70	5	1
Eagle East	Easting (X)	433,130	850	5 m	170	2	2.5
	Northing (Y)	5,177,380	200	5 m	40	2	2.5
	Elevation (Z)	-600	450	5 m	90	4	1.25
Keel	Easting (X)	432,400	730	5 m	146	5	1
	Northing (Y)	5,177,250	300	5 m	60	5	1
	Elevation (Z)	-495	960	5 m	192	5	1

Each model contained similar variable fields. The variables common to all block models are summarized in Table 14.13.

Table 14.13: Parameter Fields Common to all Models

Summary of Common Block Model Fields	
Variables	**Description**
ni_k	Ordinary Kriged Nickel value in percent
cu_k	Ordinary Kriged Copper value in percent
den_k	Ordinary Kriged bulk density value in tonnes/m^3
pd_k	Ordinary Kriged Palladium value in gpt
pt_k	Ordinary Kriged Platinum value in gpt
au_k	Ordinary Kriged Gold value in gpt
co_k	Ordinary Kriged Cobalt value in percent
ag_k	Ordinary Kriged Silver value in gpt
zone	MSU, MPER, PER, SLST, SMSU, GAB, OB, OUT lithologies
ag_nn	Nearest Neighbor Silver value in gpt
au_nn	Nearest Neighbor Gold value in gpt
co_nn	Nearest Neighbor Cobalt value in percent
cu_nn	Nearest Neighbor Copper value in percent
ni_nn	Nearest Neighbor Nickel value in percent
pd_nn	Nearest Neighbor Palladium value in gpt
pt_nn	Nearest Neighbor Platinum value in gpt
sg_nn	Nearest Neighbor bulk density value in tonnes/m^3
ni_var	Kriging Variance for Nickel
ni_min_d	Distance to Closest Sample for Nickel
ni_ns	Number of Samples Used in Kriging Estimation for Nickel
ni_avg_d	Average number of Samples Used in Kriging Estimation for Nickel
cu_var	Kriging Variance for Copper
cu_min_d	Distance to Closest Sample for Copper
cu_ns	Number of Samples Used in Kriging Estimation for Copper
cu_avg_d	Average number of Samples Used in Kriging Estimation for Copper
pt_var	Kriging Variance for Platinum
pt_min_d	Distance to Closest Sample for Platinum
pt_ns	Number of Samples Used in Kriging Estimation for Platinum
pt_avg_d	Average number of Samples Used in Kriging Estimation for Platinum
class*	**Eagle Resource Classification: 1 is Measured, 2 is Indicated, 3 is Inferred**
classk*	**Keel Resource Classification: 2 is indicated, 3 is inferred**
eansr815*	**Eagle Reserve NSR Value Calculated from Script in US$**
earrc937*	**Eagle Resource NSR Value Calculated from Script in US$**
eensr815*	**Eagle East Reserve NSR Value Calculated from Script in US$**
eerrc937*	**Eagle East Resource NSR Value Calculated from Script in US$**
eknsr815*	**Keel Reserve NSR Value Calculated from Script in US$**
ekrrc937*	**Keel Resource NSR Value Calculated from Script in US$**

Note: *class values unique to each model

The Ordinary Kriging method of interpolation was used to estimate Cu, Ni, Co, Ag, Au, Pt, Pd, and bulk density block grades within the Eagle 3D block models in single passes. Grade estimation was completed utilizing

Leapfrog Edge software. The search ellipses were based on the geometric anisotropy derived from the variogram models for each of the grade items and domains; an example for the Eagle East SMSU Ni is shown in Table 14.14. The initial search distances were based on the modeled variogram ranges and increased up to 1.5 times the variogram ranges on an ad-hoc basis when it was noted that grades were not being interpolated into blocks distal to the composites.

Table 14.14: Eagle Estimation Parameters

Domain	Element	Dip	Maximum Distance (m)	Dip Azimuth	Intermediate Distance (m)	Pitch	Minimum Distance (m)	Minimum # Samples	Maximum # Samples	Maximum samples per DDH	1st Pass (%)
MSU	Cu %	80	77	10	77	0	22	4	10	3	100
	Ni %	80	77	10	77	0	22	4	10	3	100
	Co %	80	77	10	77	0	22	4	10	3	100
	Au g/t	80	77	10	77	0	22	4	10	3	100
	Pd g/t	80	77	10	77	0	22	4	10	3	100
	Pt g/t	80	77	10	77	0	22	4	10	3	100
	S %	80	77	10	77	0	22	4	10	3	100
	SG	80	77	10	77	0	22	4	10	3	100
SMSU	Cu %	80	80	10	80	0	30	4	10	3	100
	Ni %	80	80	10	80	0	30	4	10	3	100
	Co %	80	80	10	80	0	30	4	10	3	100
	Au g/t	80	80	10	80	0	30	4	10	3	100
	Pd g/t	80	80	10	80	0	30	4	10	3	100
	Pt g/t	80	80	10	80	0	30	4	10	3	100
	S %	80	80	10	80	0	30	4	10	3	100
	SG	80	80	10	80	0	30	4	10	3	100
PER	Cu %	80	121	10	121	0	44	4	30	3	100

Domain	Element	Dip	Maximum Distance (m)	Dip Azimuth	Intermediate Distance (m)	Pitch	Minimum Distance (m)	Minimum # Samples	Maximum # Samples	Maximum samples per DDH	1st Pass (%)
	Ni %	80	121	10	121	0	44	4 6	30	3	100
	Co %	80	121	10	121	0	44	4 6	30	3	100
	Au g/t	80	121	10	121	0	44	4 6	30	3	100
	Pd g/t	80	121	10	121	0	44	4 6	30	3	100
	Pt g/t	80	121	10	121	0	44	4 6	30	3	100
	S %	80	121	10	121	0	44	4 6	30	3	100
	SG	80	121	10	121	0	44	4 6	30	3	100

Table 14.15: Eagle East Estimation Parameters

Domain	Element	Dip	Maximum Distance (m)	Dip Azimuth	Intermediate Distance (m)	Pitch	Minimum Distance (m)	Minimum # Samples	Maximum # Samples	Maximum samples per DDH	1st Pass (%)
MSU	Cu %	89.97	200	9.77	15	6.02	40	4	20	3	100
	Ni %	89.97	45	9.77	15	6.02	40	4	20	3	100
	Co %	89.97	45	9.77	15	6.02	40	4	20	3	100
	Au g/t	89.97	200	9.77	15	6.02	40	4	20	3	100
	Pd g/t	89.97	200	9.77	15	6.02	40	4	20	3	100
	Pt g/t	89.97	200	9.77	15	6.02	40	4	20	3	100
	S %	89.97	45	9.77	15	6.02	40	4	20	3	100
	SG	89.97	45	9.77	15	6.02	40	4	20	3	100
SMSU	Cu %	85	160	8	60	0	16	4	20	3	100
	Ni %	85	80	8	48	0	16	4	20	3	100
	Co %	85	80	8	48	0	16	4	20	3	100
	Au g/t	85	160	8	60	0	16	4	20	3	100
	Pd g/t	85	160	8	60	0	16	4	20	3	100
	Pt g/t	85	160	8	60	0	16	4	20	3	100
	S %	85	80	8	48	0	16	4	20	3	100
	SG	85	160	8	96	0	32	4	20	3	100
PER	Cu %	85	150	8	75	0	30	4	20	3	100

Domain	Element	Dip	Maximum Distance (m)	Dip Azimuth	Intermediate Distance (m)	Pitch	Minimum Distance (m)	Minimum # Samples	Maximum # Samples	Maximum samples per DDH	1st Pass (%)
	Ni %	85	150	8	75	0	30	4	20	3	100
	Co %	85	150	8	75	0	30	4	20	3	100
	Au g/t	85	150	8	75	0	30	4	20	3	100
	Pd g/t	85	150	8	75	0	30	4	20	3	100
	Pt g/t	85	150	8	75	0	30	4	20	3	100
	S %	85	150	8	75	0	30	4	20	3	100
	SG	85	150	8	75	0	30	4	20	3	100

.

Table 14.16: Keel Estimation Parameters

Domain	Element	Dip	Maximum Distance (m)	Dip Azimuth	Intermediate Distance (m)	Pitch	Minimum Distance (m)	Minimum # Samples	Maximum # Samples	Maximum samples per DDH	1st Pass (%)
KMSU	Cu %	33.28	91.14	77.12	21.83	90.59	5.89	4	20	3	100
	Ni %	32.58	115.10	79.09	37.32	90.00	7.66	4	20	3	100
	Co %	31.90	85.75	81.71	45.29	90.00	10.32	4	20	3	100
	Au g/t	32.10	110.20	79.38	55.21	90.00	27.00	4	20	3	100
	Pd g/t	33.84	95.20	80.75	18.04	90.00	3.79	4	20	3	100
	Pt g/t	32.16	46.27	80.14	33.78	90.00	6.77	4	20	3	100
	S %	33.20	59.14	83.56	41.31	90.00	8.10	4	20	3	100
	SG	35.41	170.00	78.29	100.00	90.00	34.00	4	20	3	100
MPER and WPER	Cu %	83.08	65	6.29	45	150.25	35	4	18	3	100
	Ni %	83.08	65	6.29	45	147.60	35	4	18	3	100
	Co %	84.69	60	3.48	45	147.24	32	4	18	3	100
	Au g/t	89.00	65	188.00	40	22.21	40	4	18	3	100
	Pd g/t	89.62	65	184.20	65	27.49	35	4	18	3	100
	Pt g/t	88.94	40	184.07	30	20.84	20	4	18	3	100
	S %	83.08	80	6.29	70	158.06	45	4	18	3	100
	SG	83.52	75	6.30	50	129.14	50	4	18	3	100

All estimation parameter values were restricted to a single pass of the full ellipsoid range, and if the cell was not filled, a factor of 1.5x ellipsoid range was used on an ad hoc basis. After Kriging, any negative block values were set to the half detection value for that particular element (except for SG, which was discussed previously). See Table 14.13, Table 14.14, and Table 14.15 for estimation parameters. The Keel MSU (KMSU) used a Radial Basis Function method for grade interpolation, which allowed a structural trend to be used in conjunction with the search ellipsoid (see Table 14.15).

14.8 Mineral Resources Classification

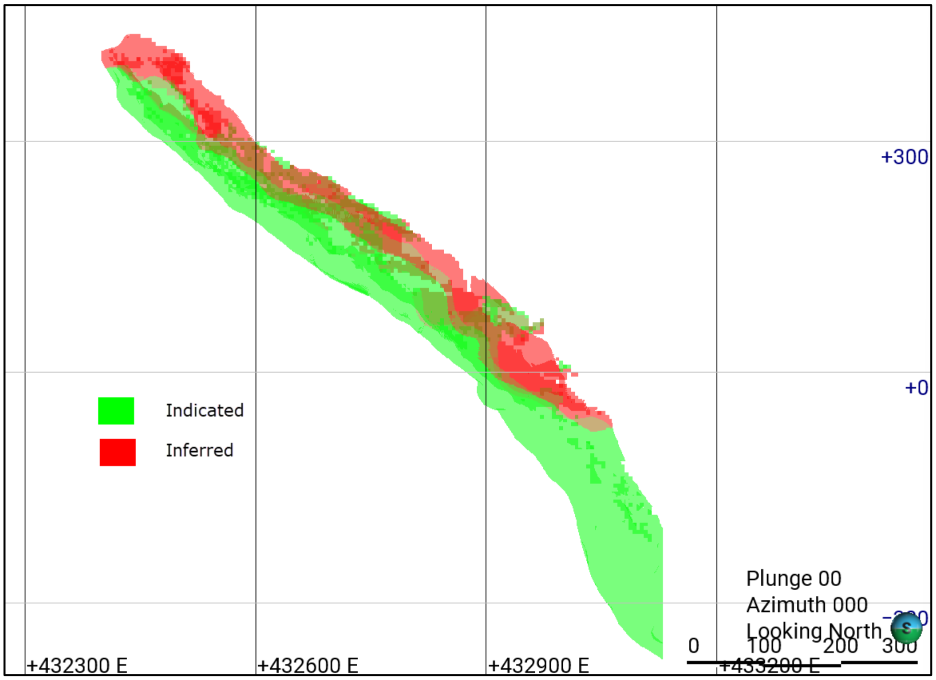
Definitions for resource categories used in this Technical Report are consistent with CIM Definition Standards for Mineral Resources and Mineral Reserves (2014). The classification of Mineral Resources at Eagle Mine incorporated the confidence in the drill hole data, the geological interpretation, data distribution, geostatistical analysis, detailed underground geological mapping of drifts and stopes, and the confidence in the grade estimation. While all the factors previously stated support confidence at Eagle Mine, the classification primarily relies on a combination of maximum distance to nearest sample and the average distance of samples interpolating grade into a block, as outlined in Table 14.17.

Table 14.17: Eagle Mine Mineral Resources Classification Protocol for Eagle and Eagle East

Class	Classification	Average Distance (m)	Maximum Distance (m)
1	Measured	<10	10
2	Indicated	10 to 20	20
3	Inferred	20 to 30	30

Table 14.18: Eagle Mine Mineral Resources Classification Protocol for the Keel Deposit

Class	Classification	Average Distance (m)
2	Indicated	0 to 30
3	Inferred	30 to 50



*Source: Talon, 2026

Figure 14.6: View looking North showing Coding of Mineral Resources Class in Keel

Mineral Resources have only been classified and reported for the SMSU, MSU, and the Keel domains. The SED and GAB domains have not been classified due to a lack of mineralization and confidence. The Eagle deposit contains a mix of resource classifications in which secondary smoothing was employed in upgrading the Inferred designation in small areas that occurred within a larger zone of Indicated Resource. In the case of Eagle East, despite sample distance, as well as previous cut and fill mining levels, supporting partial tonnage in a Measured classification (Figure 14.7). Eagle Mine technical staff felt more confident in conservatively designating the Eagle East deposit entirely as an Indicated classification. For Keel, a solid was created based on the classification distances in the above table to avoid the spotted dog effect.

In the opinion of the QP, the Eagle, Eagle East, and Keel deposits are reasonably classified and are consistent with CIM Definition Standards for Mineral Resources and Mineral Reserves (2014).

14.9 Block Model Validation

A statistical and visual assessment of the block model was undertaken to: 1) assess successful application of the estimation passes; 2) ensure that, as far as the data allowed, all blocks within mineralized domains were estimated and; 3) ensure that model estimates were representative of the data and performed as expected. The grade model was validated using the following techniques:

- The global de-clustered mean grades of the input data were compared with the global mean grades of the output block model. Table 14.19 provides an example of the numerical validation reviewed.
- Visual validation by comparison of the drill hole composite grades with the block model grades on vertical sections and plans. Figure 14.7 provides an example of the visual comparison performed.
- A Nearest Neighbor model was created and compared to the Kriged model using sectional swath plots. In Leapfrog Edge, Swath Plots of metal grades were used to compare the declustered Nearest Neighbor model

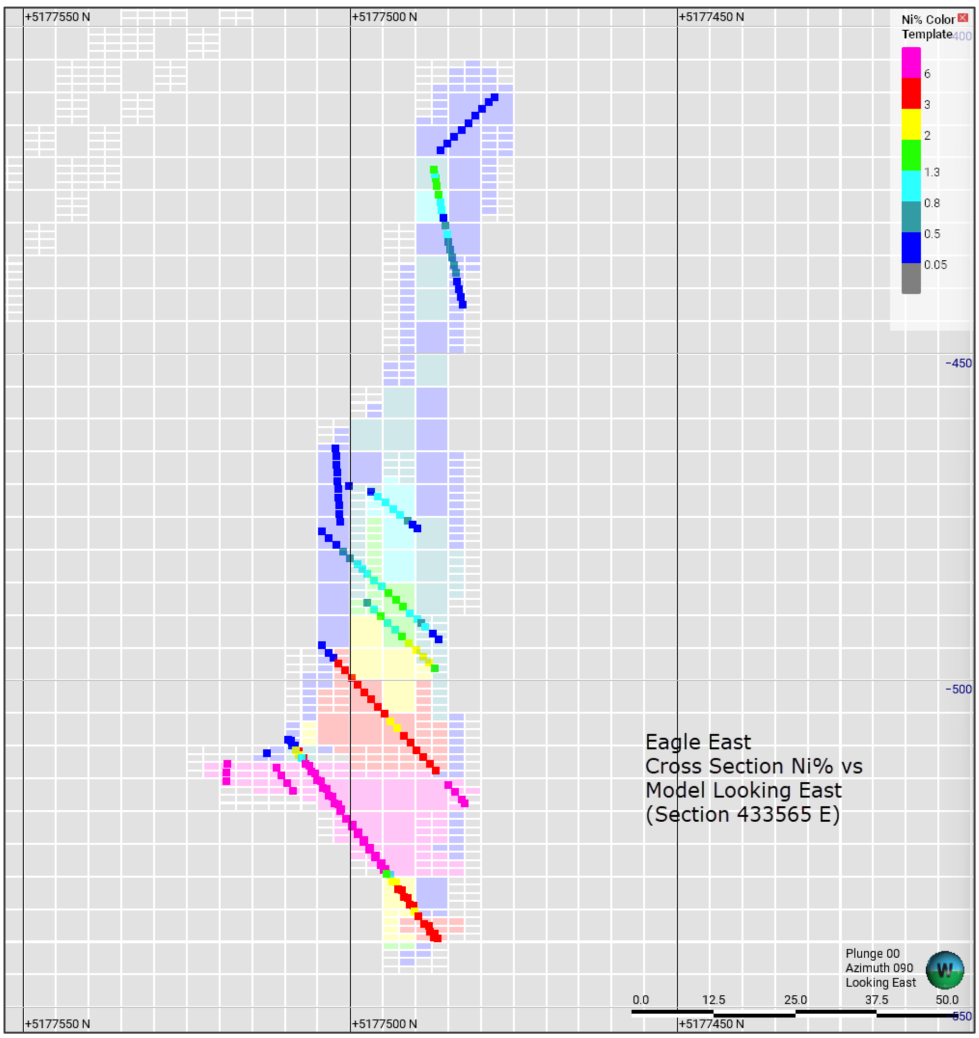
with the Kriged block model in east-west, north-south, and vertical slices through the deposit. Figure 14.8 offers an example of the format that swath plot visualization provides.

Table 14.19: Comparison of Input and Model Grade Means for Eagle East SMSU Domain

Element	Source	Nrec	Nsamp	Min	Max	Mean	Std.Dev	Var.	C.V.
Cu%	Raw	1891	1891	0.05	8.65	1.84	1.08		0.59
	Composite	2076	2076	0.25	8.52	1.81	1.04		0.57
	NN Model	32426	32426	0.25	8.52	1.87	1.09	1.19	0.58
	OK Model	32426	32426	0.67	6.05	1.81	0.64	0.41	0.35
Ni%	Raw	1891	1891	0.06	9.16	2.26	1.05		0.47
	Composite	2076	2076	0.31	7.53	2.24	1.03		0.46
	NN Model	32426	32426	0.31	7.53	2.27	1.04	1.09	0.46
	OK Model	32426	32426	0.78	5.51	2.24	0.75	0.57	0.34
Co%	Raw	1891	1891	0.00	0.19	0.05	0.02		0.38
	Composite	2076	2076	0.01	0.19	0.05	0.02		0.38
	NN Model	32426	32426	0.01	0.19	0.05	0.02	0.00	0.38
	OK Model	32426	32426	0.02	0.14	0.05	0.01	0.00	0.27
Au ppm	Raw	1885	1885	0.00	7.40	0.23	0.38		1.66
	Composite	2070	2070	0.00	7.40	0.22	0.35		1.56
	NN Model	32426	32426	0.00	7.40	0.23	0.33	0.11	1.47
	OK Model	32426	32426	0.05	2.53	0.23	0.16	0.03	0.70
Pd ppm	Raw	1891	1891	0.01	8.48	0.42	0.50		1.19
	Composite	2076	2076	0.00	8.48	0.42	0.47		1.12
	NN Model	32426	32426	0.00	8.48	0.41	0.44	0.19	1.08
	OK Model	32426	32426	0.09	4.35	0.39	0.23	0.05	0.59
Pt ppm	Raw	1891	1891	0.01	10.00	0.61	0.59		0.96
	Composite	2076	2076	0.00	10.00	0.61	0.56		0.92
	NN Model	32426	32426	0.00	6.48	0.59	0.54	0.29	0.91
	OK Model	32426	32426	0.13	3.63	0.56	0.31	0.09	0.54

Element	Source	Nrec	Nsamp	Min	Max	Mean	Std.Dev	Var.	C.V.
S%	Raw	1891	1891	0.91	35.40	9.54	4.32		0.45
	Composite	2076	2076	1.65	36.00	9.48	4.27		0.45
	NN Model	32426	32426	1.68	36.00	9.54	4.31	18.53	0.45
	OK Model	32426	32426	3.34	24.04	9.38	3.14	9.84	0.33

Block grades were checked visually onscreen in Leapfrog Geo and viewed on a series of sections and plans against the drill hole composite grades (see Figure 14.7). This comparison showed a good correlation between the input data and estimated values. The trends in mineralization were honored by the estimated grades and no obvious discrepancies were observed.



*Source: Talon, 2026

Figure 14.7: Visual Comparison of Input Composites and Resulting OK Estimates for Ni

The sectional swath plots indicate that the trend of the estimated block grades generally honors the trend of input grades and is smoother as expected from the effects of the Ordinary Kriging interpolation. Portions of the graphs where the block grades deviate from the input grades are generally associated with areas of low data, as expected.

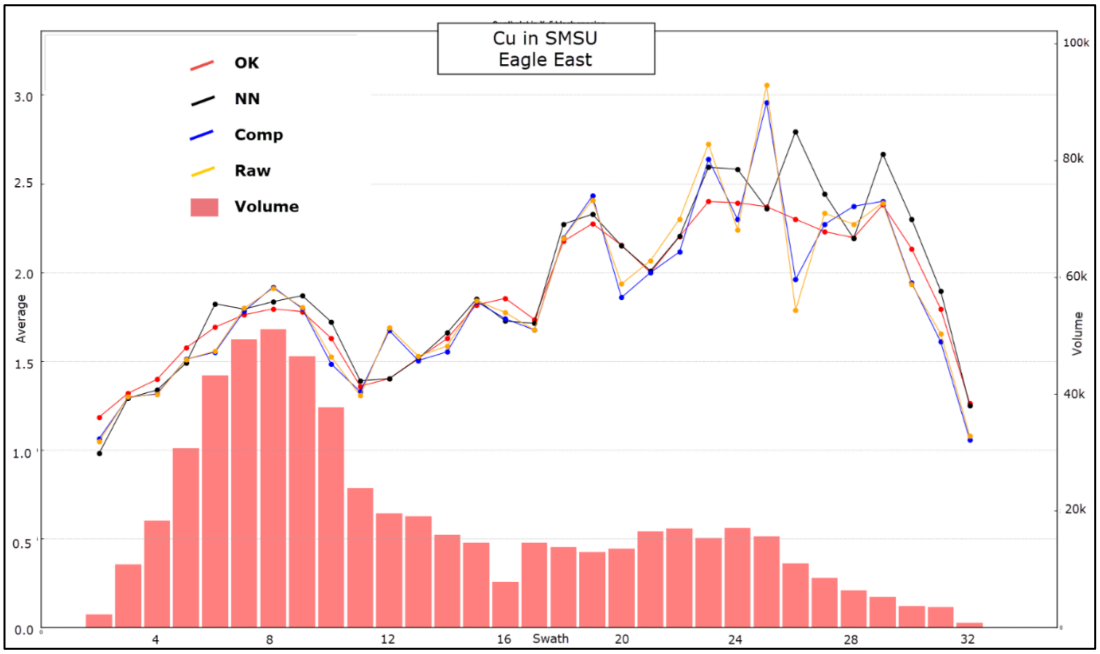


Figure 14.8: Swath plot using 5m slices of the Means of Input Value Versus Declustered NN and Model Means for Cu% in the Eagle Deposit

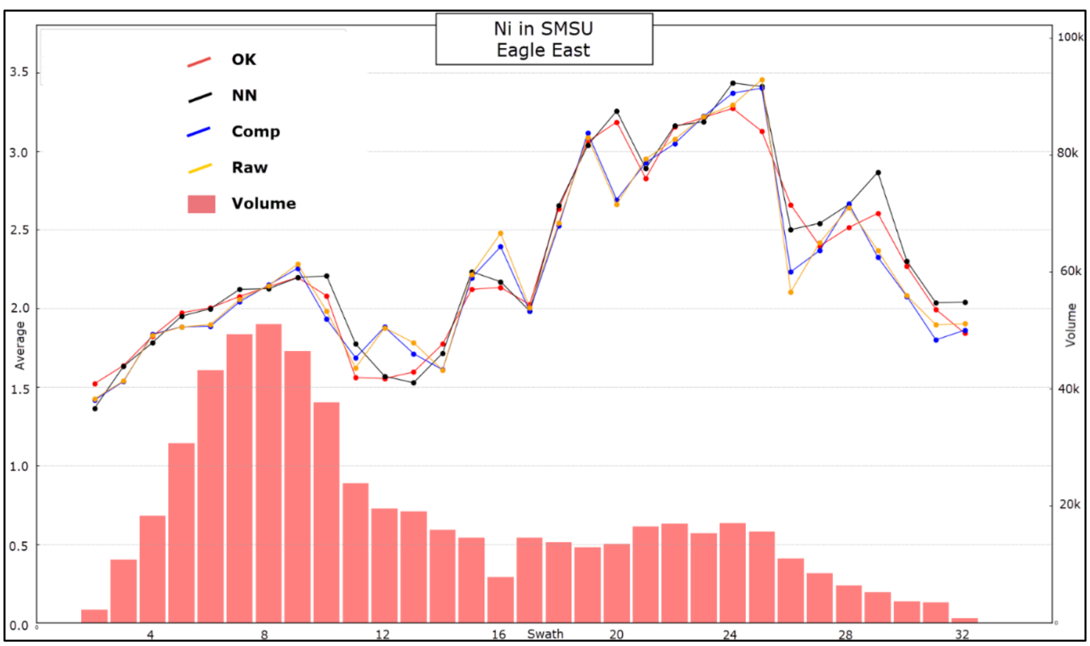


Figure 14.9: Swath plot using 5m slices of the Means of Input Value Versus Declustered NN and Model Means for Ni% in the Eagle Deposit

Globally, no indications of significant over- or underestimation were apparent in the model for any domain models. There were no obvious interpolation issues identified.

14.10 Reasonable Prospects of Eventual Economic Extraction (RPEEE)

Talon used an estimated block NSR value to apply a cut-off to the Mineral Resources estimate. The calculation was applied by means of a script that was run from within Vulcan mining software. The script included provisions for metal prices, metallurgical recoveries, smelter terms, transportation costs, and royalties. Mining methods considered were sub-level open stoping and drift-and-fill.

Metallurgical recoveries were derived from the performance characteristics of the mill and included formulae for the estimated deportments of all components to the various concentrates. Smelter terms included payables, treatment and recovery charges, and penalties for the estimated production of both nickel and copper concentrates. Transport costs reflected the present costs for the operation. Royalties were based upon the agreements in place at the time of reporting.

The QP reviewed the script and the inputs and considers them to be reasonable and well within the level of detail generally acceptable for the estimation of Mineral Resources. Metal prices used for Mineral Resources estimates are based on consensus, long-term forecasts from banks, financial institutions, and other sources (see Table 14.20). Nickel and copper metal prices used for the Mineral Resources estimation are fifteen percent higher than those used for Mineral Reserves estimates.

Table 14.20: Metal Prices Used for NSR Calculation in 2026 Mineral Resources Estimation

Element	Reserves	Resources
Nickel $/lb	$8.15	$9.37
Copper $/lb	$4.95	$5.69
Cobalt $/lb	$20.00	$20.00
Gold $/oz	$3,825	$3,825
Platinum $/oz	$1,500	$1,500
Palladium $/oz	$1,205	$1,205
Silver $/oz	$44.50	$44.50

Note: All values in US dollars.

The NSR cut-off value of $150.61/t was used for reporting the Mineral Resources estimates.

14.11 Mineral Resources Estimate

The Mineral Resources Estimate for the Eagle Mine is reported in accordance with NI 43-101 and has been estimated in conformity with generally accepted CIM Estimation of Mineral Resources and Mineral Reserves Best Practices guidelines.

The Mineral Resources estimate is reported at NSR cut-off values of $150.61/t for all deposits (Table 14.21). The Mineral Resources estimates are inclusive of Mineral Reserves but exclude mineralization within previously mined (depleted) areas.

Mineral Resources are not Mineral Reserves, and do not demonstrate economic viability. There is no certainty that all, or any part, of the Mineral Resources will be converted into Mineral Reserves. Inferred Mineral Resources are considered too speculative geologically to have economic considerations applied to them that would enable them to be categorized as Mineral Reserves.

Table 14.21: Eagle Mineral Resources Estimate (Effective February 28, 2026)

Category	Domain	Tonnes (kt)	Ni (%)	Cu (%)	Co (%	Au (g/t)	Ag (g/t)	Pt (g/t)	Pd (g/t)
Measured	MSU	-	-	-	-	-	-	-	-
	SMSU	34	1.26	1.47	0.03	0.21	7.71	0.40	0.24
	PER	5	0.82	0.98	0.03	0.14	4.83	0.24	0.17
Total Measured		**39**	**1.21**	**1.40**	**0.03**	**0.20**	**7.35**	**0.38**	**0.24**
Indicated	MSU	-	-	-	-	-	-	-	-
	SMSU	31	1.29	1.39	0.04	0.21	7.52	0.39	0.24
	PER	12	0.85	0.91	0.03	0.12	3.76	0.21	0.14
Total Indicated		**43**	**1.17**	**1.26**	**0.03**	**0.18**	**6.45**	**0.34**	**0.21**
Total M and I		82	1.19	1.33	0.03	0.19	6.88	0.36	0.22
	SMSU	3	1.44	1.47	0.04	0.18	7.22	0.37	0.24
	PER	16	0.91	0.69	0.03	0.07	2.79	0.18	0.12
Total Inferred		**19**	**0.99**	**0.82**	**0.03**	**0.09**	**3.50**	**0.21**	**0.14**

Notes:

1. Mineral Resources are reported inclusive of Mineral Reserves at an NSR cut-off value of $150.61/t.
2. Metal Prices used: $9.37/lb Ni, $5.69/lb Cu, $20.00/lb Co, $3,825/oz Au, $44.50/oz Ag, $1,500/oz Pt, $1,205/oz Pd.

Table 14.22: Eagle East Mineral Resources Estimate (Effective February 28, 2026)

Category	Domain	Tonnes (kt)	Ni (%)	Cu (%)	Co (%	Au (g/t)	Ag (g/t)	Pt (g/t)	Pd (g/t)
Measured	MSU	-	-	-	-	-	-	-	-
	SMSU	-	-	-	-	-	-	-	-
	PER	-	-	-	-	-	-	-	-
Total Measured		**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**
Indicated	MSU	6	7.95	3.78	0.18	0.16	10.43	0.99	0.59
	SMSU	650	1.98	1.67	0.05	0.21	6.99	0.49	0.33
	PER	508	0.90	0.76	0.03	0.10	3.31	0.26	0.19
Total Indicated		**1,164**	**1.54**	**1.29**	**0.04**	**0.16**	**5.40**	**0.39**	**0.27**
Total M & I		**1,164**	**1.54**	**1.29**	**0.04**	**0.16**	**5.40**	**0.39**	**0.27**

Notes:

1. Mineral Resources are reported inclusive of Mineral Reserves at an NSR cut-off value of $150.61/t.
2. Metal Prices used: $9.37/lb Ni, $5.69/lb Cu, $20.00/lb Co, $3,825/oz Au, $44.50/oz Ag, $1,500/oz Pt, $1,205/oz Pd.

Table 14.23: Keel Mineral Resources Estimate (Effective February 28, 2026)

Category	Domain	Tonnes (kt)	Ni (%)	Cu (%)	Co (%	Au (g/t)	Ag (g/t)	Pt (g/t)	Pd (g/t)
Measured	MSU	-	-	-	-	-	-	-	-
	MPER	-	-	-	-	-	-	-	-
	PER	-	-	-	-	-	-	-	-
Total Measured		**-**	**-**	**-**	**-**	**-**	**-**	**-**	**-**
Indicated	MSU	74	5.48	2.15	0.15	0.10	6.68	0.51	0.36
	MPER	1,977	0.97	0.73	0.03	0.08	2.98	0.19	0.13
	PER	1	0.82	0.68	0.03	0.09	2.46	0.11	0.11
Total Indicated		**2,053**	**1.14**	**0.78**	**0.03**	**0.08**	**3.12**	**0.20**	**0.14**
Total M and I		**2,053**	**1.14**	**0.78**	**0.03**	**0.08**	**3.12**	**0.20**	**0.14**
	MSU	1	5.51	2.10	0.15	0.10	6.37	0.53	0.36
	MPER	113	0.89	0.68	0.02	0.06	2.52	0.11	0.13
	PER	-	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Total Inferred		**113**	**0.92**	**0.69**	**0.02**	**0.06**	**2.54**	**0.11**	**0.13**

Notes:
1. Mineral Resources are reported inclusive of Mineral Reserves at an NSR cut-off value of $150.61/t.
2. Metal Prices used: $9.37/lb Ni, $5.69/lb Cu, $20.00/lb Co, $3,825/oz Au, $44.50/oz Ag, $1,500/oz Pt, $1,205/oz Pd.

Table 14.24 provides summary totals of the Mineral Resources estimates for all three combined zones at Eagle Mine.

Table 14.24: Eagle Mine Mineral Resources Estimate (Effective February 28, 2026)

Domain	Category	Tonnes (kt)	Ni (%)	Cu (%)	Co (%)	Au (g/t)	Ag (g/t)	Pt (g/t)	Pd (g/t)
Eagle	Measured (M)	39	1.21	1.40	0.03	0.20	7.35	0.38	0.24
Eagle East		-	-	-	-	-	-	-	-
Keel		-	-	-	-	-	-	-	-
Total Measured		**39**	**1.21**	**1.40**	**0.03**	**0.20**	**7.35**	**0.38**	**0.24**
Eagle	Indicated (I)	43	1.17	1.26	0.03	0.18	6.45	0.34	0.21
Eagle East		1,164	1.54	1.29	0.04	0.16	5.40	0.39	0.27
Keel		2,053	1.14	0.78	0.03	0.08	3.12	0.20	0.14
Total Indicated		**3,260**	**1.28**	**0.97**	**0.03**	**0.11**	**3.98**	**0.27**	**0.18**
Eagle	M&I	82	1.19	1.33	0.03	0.19	6.88	0.36	0.22
Eagle East		1,164	1.54	1.29	0.04	0.16	5.40	0.39	0.27
Keel		2,053	1.14	0.78	0.03	0.08	3.12	0.20	0.14
Total M&I	**M&I**	**3,299**	**1.28**	**0.97**	**0.03**	**0.11**	**4.02**	**0.27**	**0.19**
Eagle	Inferred	19	0.99	0.82	0.03	0.09	3.50	0.21	0.14
Eagle East		-	-	-	-	-	-	-	-
Keel		113	0.92	0.69	0.02	0.06	2.54	0.11	0.13
Total Inferred		**132**	**0.93**	**0.71**	**0.03**	**0.07**	**2.68**	**0.13**	**0.13**

Notes:

1. The updated MRE has been reported in-situ and has been prepared in accordance with the CIM Standards (2014) and follows Best Practices outlined by the CIM (2019).
2. Mineral Resources that are not Mineral Reserves do not have demonstrated economic viability.
3. The QP (for purposes of National Instrument 43-101 – Standards of Disclosure for Mineral Projects ("NI 43-101")) for the updated MRE is Brian Thomas, P.Geo., an employee of WSP and is "independent" of the Company within the meaning of Item 1.5 of NI 43-101.
4. The effective date of the updated MRE is February 28, 2026.
5. Mineral Resources are reported inclusive of Mineral Reserves at an NSR cut-off value of $150.61/t.
6. Metal Prices used: $9.37/lb Ni, $5.69/lb Cu, $20.00/lb Co, $3,825/oz Au, $44.50/oz Ag, $1,500/oz Pt, $1,205/oz Pd.
7. Rounding may result in apparent summation differences between tonnes, grade, and metal content.

14.12 Change from Previous Estimate

The previous Mineral Resources estimate was dated effective December 31, 2022, and changes since that estimate include 36 months of mining of the Eagle and Eagle East deposits and the inclusion of the Keel. Mining of the Eagle and Eagle East deposits depleted Mineral Resources primarily in the Measured and Indicated categories with little exploration additions. The reduction in Indicated Mineral Resources was offset by the introduction of the Keel, although at a much lower grade. Table 14.25 shows the change in tonnes and grade.

Table 14.25: Changes in Quantity of Mineral Resources from Previous Estimate

Classification	Nickel (kt)	Copper (kt)	Cobalt (kt)	Gold (koz)	Silver (koz)
Measured	-2	-2	0	-1	-34
Indicated	-9	-7	0	-2	-107
M&I	-12	-9	0	-3	-141
Inferred	0	0	0	0	-1

14.13 Risks and Opportunities

The QP has outlined the following risks and opportunities for the Eagle Mine MRE.

- Mineral domain models are interpreted from drill hole data and are subject to change with new information or re-interpretation at different cut-off values. Changes in modeling cut-offs could increase or decrease mineralized volumes.
- No mining has occurred in the Keel yet, and the nature of mineralization and grade continuity has yet to be confirmed.
- Some drill core intervals within the low-grade area of the Keel were not sampled and were assigned values of half detection limits during grade estimation.
- Different grade estimation methodologies can be used to support an MRE, and variations in the approach, including estimation parameters and outlier controls used, can have a material impact on the resources estimate.
- Changes in metal prices and mining costs can vary significantly over short periods of time, which has the potential to materially impact the MRE.
- Further infill drilling could provide an opportunity to increase resource confidence and may support the conversion of remaining Inferred resources to the Indicated category.

It is the opinion of the QP that the Mineral Resource has reasonable prospects for economic extraction based on reasonable grade continuity at the selected economic reporting cut-off. The QP is unaware of any known environmental, permitting, legal, title, taxation, socio-economic, marketing, political, or other relevant factors that could materially affect the Mineral Resources estimates.

15. Mineral Reserves Estimates

15.1 Introduction

This section presents the Mineral Reserves Estimate for Eagle Mine and details the key assumptions, parameters, and methods used for converting Measured and Indicated Mineral Resources to Proven and Probable Mineral Reserves.

The Mineral Reserves for the Eagle Mine were estimated using the CIM 2019 Best Practices Guidelines and are classified using the 2014 CIM Definition Standards.

The Mineral Reserves presented herein has been calculated based on the 2025 Mineral Resources Model update and has an effective date of February 28, 2026.

Mineral Reserves, which are inclusive of dilution and mining loss, are reported at the point of delivery to the process plant and are supported by a mining design, a detailed mine production schedule, and capital and operating cost estimates.

15.2 Estimation Procedure

The process involves converting Indicated and Measured Mineral Resources to Proven and Probable Mineral Reserves by identifying material that exceeds the cut-off grade and conforms to the geometrical constraints imposed by the selected mining method. This conversion also applies to modifying factors such as dilution and mining recovery.

The conversion of Mineral Resources to Mineral Reserves involves the application of the following procedures:

- Apply the mine design criteria to the Deswik Stope Optimizer (DSO) setting, including level spacing, stope dimensions, and minimum mining width.
- Apply modifying factors that include mining dilution, recovery, and cut-off grade.
- Generate preliminary stope shapes for various cut-off grades using DSO software.
- Design stope accesses, mine development, and infrastructure using Deswik CAD software.
- Determine the stopes mining sequence based on geotechnical guidelines.
- Apply the development and stoping production rates to create a detailed mining production schedule.
- Generate a life-of-mine (LOM) production plan and material take-offs (MTO) as a basis for cost estimation.
- Prepare the final Mineral Reserves statement.

15.3 Dilution and Mining Recovery

The Mineral Reserves estimate includes dilution and mining recovery, which are modifying factors that affect the quantity and quality of the material extracted during mining operations.

15.4 Mining Dilution

Mining dilution was accounted for from three (3) principal sources: planned (internal) dilution, unplanned (external) dilution, and backfill dilution.

Planned (Internal) Dilution refers to dilution from low-grade or waste material that is unavoidably included within the designed stope boundaries.

Unplanned (External) Dilution refers to dilution from material outside the stope resulting from blasted rock breakage beyond the defined profile of the stope in both the hanging wall and footwall. At Eagle Mine, this dilution is quantified using an ELOS (Equivalent Linear Overbreak/Slough) metric, with values assigned to stopes according to their respective zones. The applied ELOS values are detailed in Table 15.1.

Table 15.1: ELOS values for the different Eagle mine zones

Mine Zone	HW ELOS (m)	FW ELOS (m)	Total dil %
Upper Keel	0.75	0	7.9%
Middle and Lower Keel	0.5	0.5	7.6%
Eagle East	0.5	0.5	7.4%
Eagle	0.5	0.5	8.7%

Backfill Dilution: This refers to any dilution resulting from interaction between ore and backfill material during mining. The percentage of backfill dilution at Eagle Mine is based on exposure to CRF and defined by the mining method and stope type (primary vs. secondary), as outlined in Table 15.2.

Table 15.2: Backfill dilution values for the different Eagle mine zones

Excavation Type	Backfill dilution %
Transverse Primary Stope[1]	2%
Transverse Secondary Stope	10%
Longitudinal Stope[1]	2%
Drift and Fill	5 to 6%

Notes:

1. Backfill dilution is only applied to transverse primary and longitudinal stopes with end wall CRF exposure from an adjacent stope.

No dilution or overbreak was applied to the development.

The tonnage and grade associated with both external and internal dilution were determined directly from the resource block model, while the backfill dilution was incorporated at a zero grade.

15.5 Mining Recovery

Mining recovery accounts for material loss during the mining process and is defined as the percentage of actual mineable material extracted from the planned mining shape.

Mine recovery rates at the Eagle Mine vary depending on the zone and the mining method. Table 15.3 provides a summary of these rates.

Table 15.3: Mining Recovery Values for the Different Eagle Mine Zones

Mine Zone	Mining Recovery
Keel	93.7%
Eagle East Longhole	93.7%
Eagle East Drift and Fill	94.7%
Eagle	93.7%

For development drifts, mining losses are assumed to be negligible, and a 100% recovery is applied.

15.6 Stope Optimization

Deswik Stope Optimizer (DSO) software was used to determine the mineable portion of the Mineral Resources. DSO is a mine planning tool that generates and optimizes the design of stope shapes for a range of underground mining methods. The goal is to determine the Mineral Reserves from the Block Model by applying specified mining methods and design parameters. The software optimizes the stope design based on the mining method, the resource geometry, the dilution and mining recovery parameters, the NSR value of the blocks, and the NSR cut-off.

Multiple DSO scenarios were run to obtain the best results in terms of tonnage and grade. The Mineral Reserves were sequenced and scheduled into an integrated LOM schedule using Deswik Interactive Scheduling software and exported to spreadsheets for financial analysis.

The mine design is based on the following mining methods:

- Eagle Zone — Transverse sublevel stoping
- Eagle East Zone — Transverse and longitudinal sublevel stoping, and drift-and-fill mining
- Keel Zone — Transverse and longitudinal sublevel stoping

In the Upper Keel these preliminary DSO shapes served as the basis to create mineralized shells, which were subsequently cut to align with the level elevations and the projected strike length of the stopes.

An evaluation of marginal stopes has been conducted; stopes have been added where the design and sequence allow it, such as between 2 stopes and where there is no need for development to mine these stopes.

Development headings were subsequently designed and optimized, and stopes were then sequenced based on geotechnical guidance to align with the selected mining method. The final stope sequence was incorporated into the Deswik Scheduler, which was used to generate the production profile and define the overall Life-of-Mine (LOM) schedule.

15.7 NSR Values

Table 15.4 and Table 15.5 summarize the metal prices, parameters, and costs used to determine the NSR value of each block. NSR refers to the proceeds received from the sale of the mineral product net of deductions for costs incurred before the sale of the product and after it leaves the mining property. These costs include transportation, insurance, penalties, sampling and assaying, refining and smelting, and marketing. For estimating Mineral Reserves, the NSR value of the metal contained in a tonne of concentrate is applied to the metallic content of the corresponding ROM tonnes. Details of the refining contracts are confidential. The QP deems the terms reasonable

Table 15.4: NSR Input Metal Prices

Element	Unit	2026	2027	2028	2029	2030+
Nickel	$/lb	7.50	7.70	8.15	8.15	8.15
Copper	$/lb	5.50	5.00	4.95	4.95	4.95
Cobalt	$/lb	19.00	20.00	20.00	20.00	20.00
Platinum	$/oz	1,500	1,500	1,500	1,500	1,500
Palladium	$/oz	1,245	1,205	1,205	1,205	1,205
Gold	$/oz	4,200	3,825	3,825	3,825	3,825

Table 15.5: NSR Input Paramters

Recoveries in Bulk Flotation		
Ni	%	78-83
Cu	%	93-96
Co	%	80-85
Au	%	70-72
Pt	%	71-75
Pd	%	78-83
Nickel Concentrate		
Ni recovery from bulk to Ni conc	%	98.1-98.5
Ni recovery from ore to Ni conc	%	77.1-81.8
Cu recovery from ore to Ni conc	%	16.5-18.0
Copper Concentrate		
Cu recovery from bulk to Cu conc	%	80.8-82.5
Cu recovery from ore to Cu conc	%	75.4-78.8
Ni recovery from ore to Cu conc	%	1.2-1.6
Smelter Terms – Nickel Concentrate		Variable
Smelter Terms – Copper Concentrate		Variable

15.8 NSR Cut-Off Values

Table 15.6 presents the calculation of the NSR cut-off values for the Eagle, Eagle East, and Keel deposit. The NSR cut-off values consist of the unit costs for mining, processing, transportation, and general & administration. The NSR value of any given block must exceed the NSR cut-off to be included in the Mineral Reserves. Cut-off values were initially prepared by Eagle Mine staff before being reviewed by WSP. In addition to the full cost cut-off, a marginal and incremental cut-off was derived and are $107.29/t and $52.30/t, respectively. As the development requirements change over time, some fluctuations in cut-off values are expected. Certain mining areas of marginal ore were included in the mining plan as development was required to access higher-grade ore and maintain overall production rates. As long as all blocks meet incremental cutoff grade and the overall value is above the full cost cutoff grade, the reviewer is of the opinion that including a portion of lower-grade material does not impact the reserves declaration.

Table 15.6: Calculation of Eagle Mine NSR Cut-Off Values, $/t

Cost Center	Eagle
Mining	76.35
Processing	41.20
Transportation	14.06
General & Administrative	19.00
Total ($/t)	**150.61**

Source: Eagle Mine, 2026

Metal prices used for Mineral Reserves estimates are based on consensus, long-term forecasts from banks, financial institutions, and other sources.

The cutoff values were estimated from 2025 actuals with forecasted salary increases. Costs are shared proportionately among the deposits present in the actuals. An allowance for sustaining capital development is also included.

15.9 Mineral Reserves Estimate

Table 15.7 presents the Eagle Mine Mineral Reserves estimate effective as of February 28, 2026. It is based on stope wireframe shapes applied to the depleted Mineral Resources block model using Deswik mine design software. The estimate incorporates planned dilution, unplanned dilution, backfill dilution, and mining recovery. It considers mining with transverse sublevel stoping, longitudinal sublevel stoping, and drift-and-fill mining, and backfilling with cemented and uncemented rockfill.

The Mineral Reserve is based on a 2025 updated resource model, which Eagle Mine depleted to February 28, 2026, using as-built solids.

The author considers that the Mineral Reserves estimates are classified and reported in accordance with CIM definitions.

The author is not aware of any mining, metallurgical, infrastructure, permitting, or other relevant factors that could materially affect the Mineral Reserves estimate (Table 15.7).

Table 15.7: Summary of Mineral Reserves as of February 28, 2026

Domain	Category	Tonnes	Grade							Contained Metal						
			Ni	Cu	Au	Ag	Co	Pt	Pd	Ni	Cu	Au	Ag	Co	Pt	Pd
		(kt)	(%)	(%)	(g/t)	(g/t)	(%)	(g/t)	(g/t)	(kt)	(kt)	(koz)	(koz)	(kt)	(koz)	(koz)
Eagle	Proven	27	1.16	1.36	0.18	6.94	0.03	0.35	0.22	0.31	0.36	0.15	5.92	0.01	0.30	0.19
	Probable	14	1.04	1.08	0.15	5.74	0.03	0.28	0.18	0.14	0.15	0.07	2.58	0.00	0.13	0.08
	Sub Total	41	1.12	1.27	0.17	6.52	0.03	0.32	0.20	0.45	0.51	0.22	8.50	0.01	0.42	0.27
Eagle East	Proven	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	Probable	1 155	1.31	1.09	0.13	4.62	0.03	0.33	0.23	15.15	12.61	4.99	171.7	0.40	12.2	8.36
	Sub Total	1 155	1.31	1.09	0.13	4.62	0.03	0.33	0.23	15.15	12.61	4.99	171.7	0.40	12.2	8.36
Keel	Proven	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	Probable	2 290	0.94	0.68	0.07	2.71	0.03	0.17	0.12	21.50	15.48	5.52	199.4	0.59	12.8	8.81
	Sub Total	2 290	0.94	0.68	0.07	2.71	0.03	0.17	0.12	21.50	15.48	5.52	199.4	0.59	12.8	8.81
Total	Proven	27	1.16	1.36	0.18	6.94	0.03	0.35	0.22	0.31	0.36	0.15	5.9	0.01	0.30	0.19
	Probable	3 459	1.06	0.82	0.09	3.36	0.03	0.23	0.16	36.79	28.25	10.57	373.6	0.99	25.2	17.3
	Total P&P	**3 486**	**1.06**	**0.82**	**0.09**	**3.39**	**0.03**	**0.23**	**0.16**	**37.10**	**28.61**	**10.73**	**379.6**	**1.00**	**25.5**	**17.4**

Notes:

1. The Mineral Reserves disclosed are classified as Proven and Probable and are based on the 2014 CIM Definition Standards and 2019 CIM Estimation of Mineral Resources and Mineral Reserves Best Practice Guidelines.
2. Mineral Reserves are estimated at a stope full cost NSR cut-off of $150.61/t, a stope marginal cost NSR cut-off of $107.29/t, and a development NSR cut-off of $52.30/t
3. Mineral Reserves are estimated using average long-term prices of $8.15/lb Ni, $4.95/lb Cu, $20/lb Co, $3825/oz Au, $44.50/oz Ag, $1500/oz Pt, $1205/oz Pd.
4. Bulk density interpolated in block model ranges from 2.98 t/m3 to 4.44 t/m3 and averages 4.11 t/m^3.
5. The reference point at which the Mineral Reserves are defined is where the ore is delivered to the process plant and therefore not inclusive of milling recoveries or payable metal deductions.
6. Contained Metal for Au, Ag, Pt and Pd is reported in Troy Ounces and calculated as follows:
   Contained Metal, (koz) = Tonnage (kt) * Grade (g/t) *0.032151
7. Numbers may not add due to rounding.
8. The QP is not aware of any environmental, permitting, legal, title, taxation, socio-economic, marketing or political factors that might affect the estimate of Mineral Reserves, other than those specified in Section 15.10.

Compared to the previous Mineral Reserves estimate effective December 31, 2024, disclosed in LMC's 2024 AIF, the Mineral Reserves have been increased by approximately 801kt, primarily by the addition of the Keel, with estimates of contained metals rising 6 kt of nickel and 5 kt of copper. These changes have included the actual depletion due to production between December 2024 and February 2026, as shown in Table 15.8 and Figure 15.1. The increase in Mineral Reserves tonnage is mainly driven by the addition of the Keel deposit to the 2025 Mineral Reserves.

Table 15.8: Change in Mineral Reserves to February 28, 2026

Item	Tonnes (kt)	Ni (%)	Cu (%)	Ni (kt)	Cu (kt)
December 31, 2024, Mineral Reserves	3484	1.19	0.91	41.6	31.8
Material Mined December 2024 to February 2026	-816	1.43	1.14	-11.7	-9.3
Additional reserves	818	0.88	0.75	7.2	6.1
February 28, 2026 Mineral Reserves	3486	1.06	0.82	37.1	28.6

Figure 15.1: Change in Mineral Reserves Since December 31, 2024

The QP has not reviewed the December 31, 2024, Mineral Reserves statement, and the numbers for the purpose of this comparison are based on Mineral Reserves estimates made publicly available on SEDAR in LMC's 2024 AIF.

15.10 Factors Affecting Mineral Reserves Estimate

The Mineral Reserves are subject to the types of risks common to underground mining operations and include:

- Interpretations of mineralization geometry, and continuity of mineralization zones.
- Changes in market conditions, commodity prices, and COG estimation assumptions.
- Changes in rock quality and geotechnical assumptions.
- Changes in process plant recoveries.
- Changes in hydrogeological conditions and water inflow assumptions.
- Changes in input factors used to assess dilution and mining recovery factors.
- Assumptions regarding social, permitting, and environmental conditions.

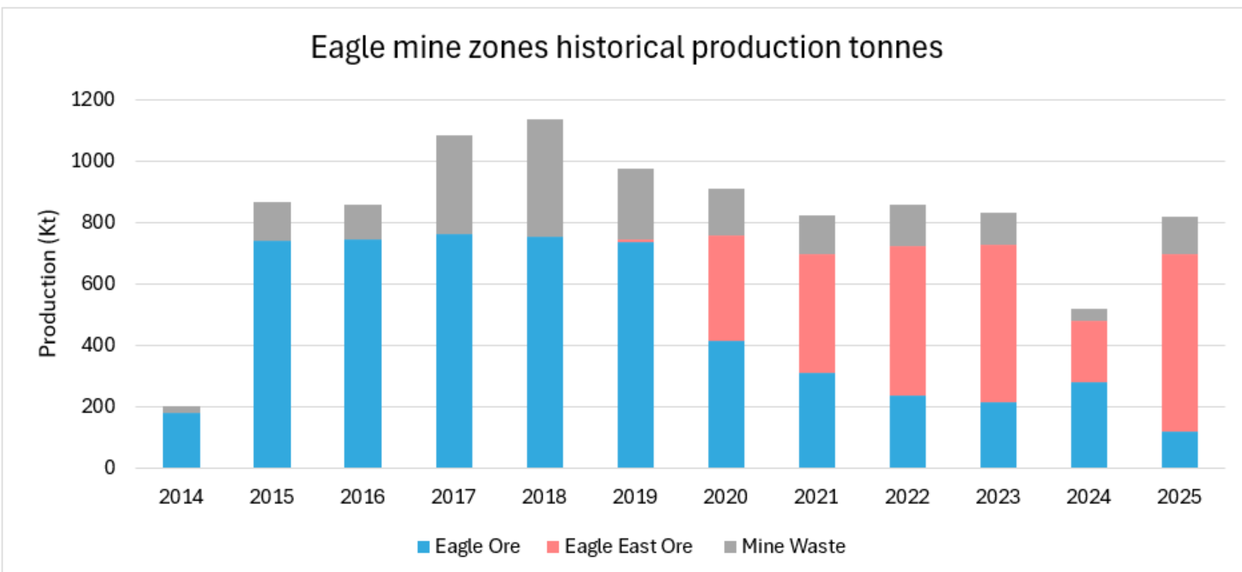
To the extent known to the responsible QP, there are no known environmental, permitting, legal, title, taxation, socio-economic, marketing, political, or other relevant factors that could affect the Mineral Reserves estimate that are not documented in this section.

16. Mining Methods

16.1 Introduction and Mining History

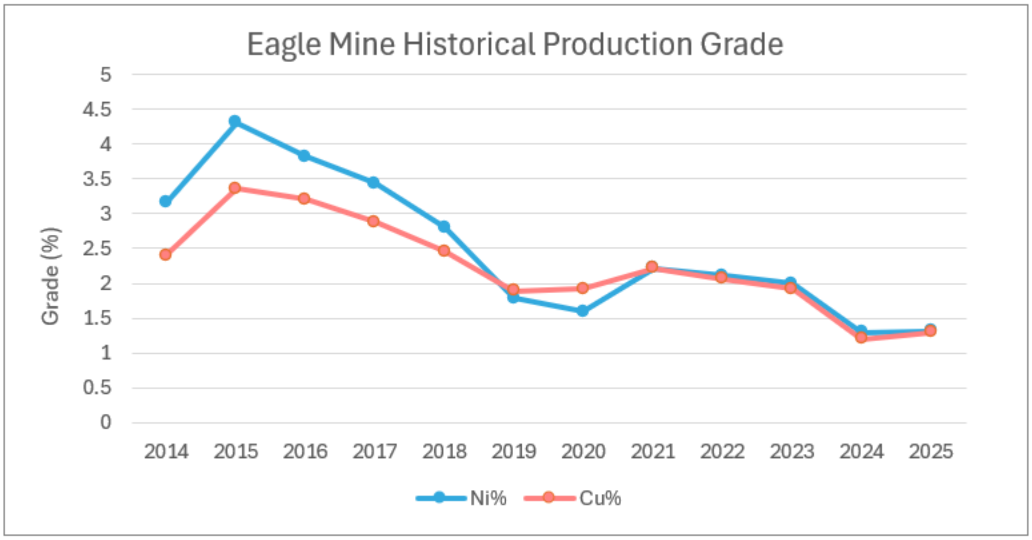
The Eagle Mine is an underground mine with a history of producing 2,000 tpd of Nickel-Copper ore. The ore is hauled to the surface in diesel-powered trucks via the ramp and then trucked to the Humboldt processing plant at a separate site. From 2014 to 2019, ore production was exclusively from the Eagle Deposit. Beginning in 2020, steady production in Eagle East resulted in a blend of ore from Eagle and Eagle East. Beginning in 2026, with the Eagle Deposit largely depleted, all ore haulage will originate from the lower portion of the mine – primarily Eagle East – with Lower Keel production coming online in H2 2026

Figure 16.1 and Figure 16.2 summarize the production history of the mine in terms of production tonnes and grade.



Source: Eagle Mine, 2026

Figure 16.1: Eagle Mine Production History – Production tonnes

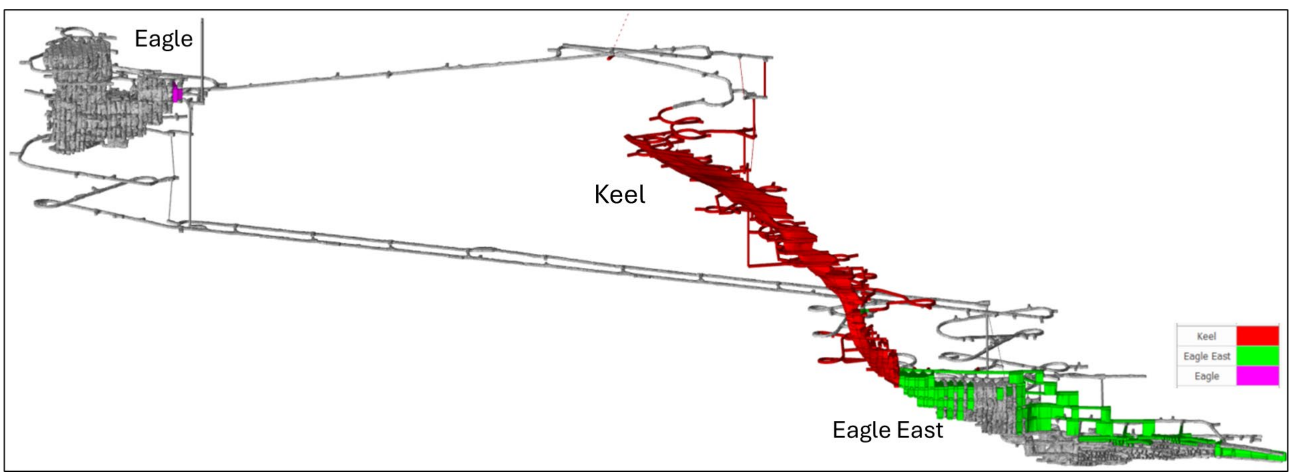


Source: Eagle Mine, 2026

Figure 16.2: Eagle Mine Production History – Grade

16.2 Deposit Descriptions and Relative Locations

Figure 16.3 provides an isometric view of the Eagle Mine. Underground workings are accessed via the main ramp, which has its portal entrance within the mine site industrial area. The mine has two active mineralized zones called Eagle and Eagle East. A third zone called Keel is currently under development and is planned to begin producing mill feed in H2 2026.



Source: Eagle Mine, 2026

Figure 16.3: Isometric View of Eagle Underground Mine

The Eagle is a near-surface deposit situated between 40 and 370 m below the surface. The deposit is about 250 m long and ranges from 15 to 85 m in width. Eagle was the first zone discovered and mined. Development of the main ramp began in September 2011, and commercial production was achieved in November 2014. Mining in this zone is done; the only remaining stopes are scheduled at the end of the mine life as they are near the permanent Alimak raise, which provides secondary egress to the entire mine.

The Eagle East is located approximately 2 km east of the Eagle deposit and 900 m below the surface. The deposit is a sub-horizontal conduit 30 to 70 m wide and 720 m in length, with a thickness of 50 to 120 m. It was discovered as a result of exploratory drilling conducted from the Eagle. Eagle East was developed from 2018 to 2020 and remains in production to the present. It is accessed from the lowest level of the Eagle via twin ramps, one providing access and return air ventilation, the other fresh air ventilation and secondary egress. Both SLOS and D&F (drift and fill) mining methods are employed at Eagle East.

The Keel is situated about 1.5 km east of the Eagle. The Keel is subdivided into three areas - Upper, Middle, and Lower Keel - based on orebody geometry and the -195 access level from the Eagle East ramp. Development of the Lower Keel has begun and is scheduled to be completed in 2026. The development of Middle and Upper Keel will continue into 2027 and 2028. Upper Keel will be mined using the Sublevel mining method (longitudinal retreat method), Middle and Lower Keel will be mined mostly via transverse long hole as the intrusion is wider in those areas.

For the upcoming years, most of the mine production will be derived from the Keel, as shown in Table 16.4.

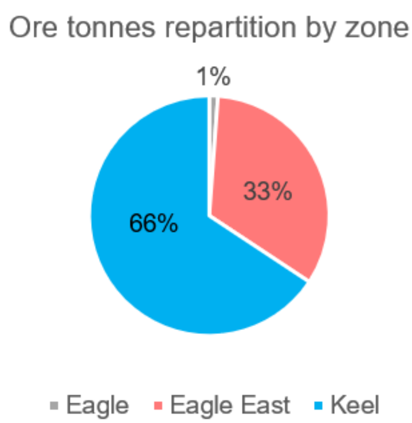
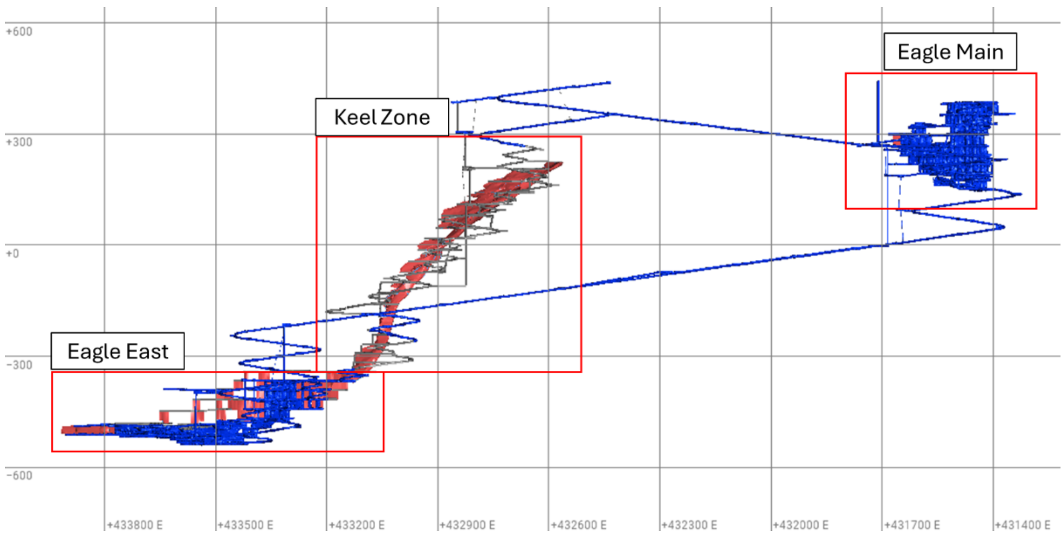


Figure 16.4: Ore Tonnes Repartition by Zone

The Eagle Mine has Mineral Reserves to support production until 2030 when the mine is scheduled to begin closure, unless additional ore is discovered.

16.3 Geomechanics

The geomechanics section discusses the geomechanical data and stability assessments provided by Eagle Mine that support the proposed LOM plan. This section discusses the LOM plan separated by the area of mining, namely, Eagle East, Keel, and Eagle Main (Figure 16.5).



Note: As-built in Blue and LOM plan in Red and Grey.

Figure 16.5: LOM Plan looking South

16.3.1 Geotechnical Domains

Eagle Mine domains rock masses with similar geotechnical characteristics primarily based on lithology. The geotechnical domains and their descriptions are outlined along with their associated lithologies in Table 16.1. The domains, lithologies, and descriptions in Table 16.1 were produced by Eagle Mine personnel and intended to apply to Eagle Main, Keel, and Eagle East. The main difference in lithology between Keel and the Eagle East and Eagle Main is that Keel contains a larger proportion of Feldspathic Peridotite within its intrusive domain. WSP understands that stope walls outside of the mineralized zone will be exposed in the Intrusive domain, and the Sedimentary domain is typically mainly encountered in development drifting, but not on stope faces.

Table 16.1: Geotechnical Domains (Eagle Mine, 2022b)

Domain	Lithologies	Description
Sedimentary (SED)	Siltstone (SLST)	Very strong (> 100 MPa) rock, typically brittle in nature, with distinct bedding and foliation, and one dominant joint set with near vertical dip to the east. Discontinuities are smooth and planar.
	Hornfels (HFLS)	
Intrusive (INT)	Peridotite (PER)	Very strong (> 100 MPa) rock, typically brittle in nature. One dominant joint set dipping near-vertically to the south, and several minor joint

Domain	Lithologies	Description
	Mineralized peridotite (MPER)	sets. Discontinuities are typically continuous, undulating, rough, and clean, though serpentinite infill is sometimes present and several millimeters in thickness.
	Semi-massive sulfide (SMSU)	
Massive (MSU)	Massive sulfide (MSU)	Strong, brittle rock typically having one dominant sub-vertical joint set plus minor random sets. Discontinuities are typically undulating and rough, and seldom contain infill.

16.3.2 Geomechanical Data Available for this Review

Eagle provided the following geomechanical data and studies for the review of their proposed LOM:

- The Ground Control Management Plan (GCMP) is understood by WSP to have been developed for Eagle Main and Eagle East (Eagle Mine, 2022b). This document includes, but is not limited to, the following information:
- Interpretations of the geomechanical characteristics and representative parameters for the rock masses in Eagle Main and Eagle East.
- Ground support standards in use at Eagle Mine.
- An in situ stress interpretation.
- As-built and LOM wireframes for the entire Eagle mine.
- Resource drill holes for the Keel deposit (from 2002 to 2021), which includes partial geotechnical logging data. The drill holes contained the following geotechnical information (but each drill hole does not have every dataset): RQD, Fracture Count, Micro-defecting observations, ISRM field strength estimates, Point Load Tests [PLTs], structure depths, joint condition, and structure types.
- Drill holes provided are EKUG002 to EKUG066 (collected in Keel from 2018 to 2021) and 69 drill holes collected in Keel from 2002 to 2014. 49 of the drill holes contained PLT data.
- Core box photographs were provided (core box photographs were captured in the core logging facility at surface after rock core transport).
- It is not known if the geotechnical core data provided was collected at the drill rig or on surface after core boxing and transport.
- Geotechnical core logging Standard Operating Procedure (SOP) used to collect data in Keel (Eagle Mine, 2022c). It is not known when this was first put in place, and if the entire dataset (from 2002 to 2021) used this SOP.

- LOM numerical modeling study, which was based on an earlier LOM iteration of Eagle East and Keel (OHMS, 2024).
- Some differences noted between the modelling LOM plan and the current LOM plan are that the OHMS appeared to have smaller stope sizes in Keel and a greater proportion of transverse stoping in Keel.
- A geotechnical study of mining in the Keel ore body (Eagle Mine, 2022a). This study was completed by Eagle's geotechnical staff and examined cut and fill mining in Keel.
- WSP studies of mine sequencing options and stope stability implications in Eagle East (WSP, 2022 & 2024).
- Keel stope sizing recommendations developed by Eagle's site geotechnical team (Eagle Mine, 2024). These recommendations were based on as-built knowledge from Eagle East.

16.3.3 Geomechanical Parameters

16.3.3.1 Rock Mass Classification

The rock mass classification systems used at Eagle Mine include RQD (Deere and Deere, 1989), RMR_{76} (Bieniawski, 1976), and the Q-system (Barton et. al., 1974). Table 16.2 presents the mean and lower bound values of RMR_{76} and Q' for each lithology in each geotechnical domain in Keel, provided by Eagle's geotechnical team (Eagle Mine, 2022a), while the classification values for Eagle East and Eagle Main (Table 16.3) were provided in the GCMP (2022b). The lower bound values represent the mean minus one standard deviation of the dataset (~16th percentile).

Table 16.2: RMR_{76} and Q' values for Keel (adapted from Eagle Mine, 2022a)

Domain	Rock Type	Mean RMR_{76}(1)	Mean Q'(2)	Lower Bound RMR_{76}(1)	Lower Bound Q'(2)
Intrusive	Feldspathic Peridotite	75	30	68	15
	Feldspathic Pyroxenite	73	25	63	8
	Gabbro	72	23	59	5.5
	Olivine Gabro	64	9	52	2.5
	Peridotite	82	65	76	36
	Pyroxenite	72	23	60	6
Sedimentary	Hornfels	72	23	64	9
	Sandstone	73	25	60	6
	Shale	77	39	65	10
	Siltstone	71	20	58	5
Massive	Massive Sulfide	77	39	65	10

(1) The RMR_{76} values estimated by Eagle for Keel (2022a) contained a typo in which the A5 factor was listed as 15 instead of 10; the RMR_{76} values in Table 2 reflect an A5 factor of 10.

(2) Q' is assumed considering $RMR_{76} = 9\ln(Q')+44$

Table 16.3: Rock Mass Classification by Domain in Eagle Main and Eagle East (Eagle Mine, 2022b)

Domain	RQD Lower Bound	RQD Mean	RMR_{76} Lower Bound	RMR_{76} Mean	Q' Lower Bound(1)	Q' Mean(1)
SED	47	73	54	58	5	7
INT	80	91	64	65	16	19
MSU	75	100	74	77	23	31

(1) Q' is assumed considering $RMR_{76} = 9\ln(Q')+44$

The rock mass classification for rock masses at Eagle Main and Eagle East is estimated from geotechnical drilling and as-built drift mapping (Eagle Mine, 2022b). The interpretation of rock mass classification for Keel is based on geotechnical data collection from resource drill holes (mostly RQD, fracture counts, PLT, and field strength estimates) and review of core box photographs. The Keel orebody does not contain geotechnical-specific drilling, nor has a third party produced a geotechnical interpretation of the rock mass characteristics at Keel; the only available interpretation of rock mass characteristics was produced by Eagle Mine(2022a).

The geotechnical data collected per resource drill hole at Keel was inconsistent, with most drill holes having RQD and fracture counts, but fewer having PLT, field strength estimates, joint conditions, etc. Due to the incomplete geotechnical data for Keel, the RMR_{76} values estimated by Eagle (2022a) were based upon the statistics of each parameter instead of by interval (as most core intervals in Keel do not have every RMR parameter logged).

WSP reviewed the RQD logged for some available drill holes within the Keel orebody. The RQD logging suggests that most intervals could be classified as "Good to Excellent"; however, the RQD database for Keel contains errors in the provided RQD data that include negative values and values >100%, ranging up to 150%, in approximately 20% of the data. To better understand the distribution of rock mass characteristics, WSP reviewed the core box photographs for the Hanging wall (HW) and Footwall (FW) for the Keel orebody from 200 masl to -240 masl for 36 drill holes (only within the EKUG dataset) and found that, for most drill holes reviewed, the RQD logging was an indicator of where blockier or competent rock was likely to be present. The core box photographs reviewed by WSP suggest that:

- The HW rock mass is mostly competent, although there are occasional areas of worse ground characteristics (blockier and altered structures), apparently related to the mineralized contact.
- The top three sub-levels in Keel contained more drill holes with poorer ground characteristics on the HW than the rest of the Keel orebody.
- Some of the drill holes throughout Keel showed poorer ground within the mineralized zone near the HW; these areas are assumed not to impact stope stability or dilution, as they are planned to be mined out within the stope shapes.
- It is possible that the rock mass exposed on some stope HWs has a lower Q' than contained in Table 16.2.
- The FW generally has worse rock mass characteristics, and most stopes will have blockier and occasionally altered rock in the FW.
- Some stopes have a gap (approximately 2 m – 10 m along drill hole) between the proposed stope shape and where the poorer rock mass is located on the FW.
- It is unclear what feature may be causing the poorer rock quality in the FW.

- It is possible that the mean Q' values in stope FWs are lower than assumed in Table 16.2.

It is recommended to collect more geomechanical data in Keel to better define the quality of the rock mass across the deposit and to better define areas of poorer rock mass characteristics. This process should begin with a reconciliation of geotechnical parameters collected in Keel against the core box photographs. Future logging should capture the component parameters to allow a Q' estimation (instead of assuming a Q' based on a typical relationship to RMR_{76}).

16.3.3.2 Intact Rock Strength

Laboratory intact strength testing has been used to determine the geomechanical strength parameters for Eagle Main and Eagle East as provided in the GCMP (Eagle Mine, 2022b). Table 16.4 presents the mean intact rock parameters provided in the GCMP.

Table 16.4: Typical Intact Rock Properties from Laboratory Testing

Domain	UCS (MPa)	Mi	Density (kg/m3)	Tensile Strength (MPa)	Young's Modulus (GPa)	Poisson's Ratio
Sedimentary	187.7	14.4	2.73	13.0	67.5	0.22
Intrusive	164.7	12.6	3.1	13.0	67.1	0.22
Massive	128.2	25.0	4.58	5.1	67.1	0.18

(TalonEagle Mine, 2022b); Representing Eagle Main and Eagle East

The quantity of laboratory tests and locations of the samples used in testing have not been provided to WSP, but it is understood to have been compiled and interpreted to be relevant for Eagle Main and Eagle East. Additionally, the GCMP (Eagle Mine, 2022b) indicates that triaxial testing was completed with a maximum confining stress of 20 MPa. This is less than the recommended confinement based on the mine's stress regime and intact rock strength. No geomechanical laboratory testing has been completed within Keel.

Since Eagle's mining experience in the waste rock in Keel (Peridotite and Feldspathic Peridotite) is limited, Point Load tests (PLTs) were conducted from drill holes within the Keel footprint (Eagle Mine, 2022a). These PLTs collected in the Feldspathic Peridotite and Peridotite units were reviewed by Eagle (2022a) to estimate mean Is values for both units. Table 16.5 presents the results of this review compared against the strength estimates estimated by Golder (2005) for Eagle Main. The PLT results suggest that intact strengths may be similar between the Eagle Main and Keel.

The PLTs used to produce Table 16.5 were collected from the core from 2004 to 2008. The PLTs in Feldspathic peridotite and peridotite represent most of the PLT database collected in Keel from 2004 to 2008 (2233 tests total). The PLTs used to produce Table 16.5 appear to be mostly diametral, with only one axial observed in the database. 146 PLTs collected from the EKUG drill holes were not included in the interpretation shown in Table 16.5.

The PLT data for 95 diametral and 51 axial tests from EKUG drill holes in Keel were reviewed by WSP. Of the diametral tests provided, two were completed in feldspathic peridotite, and 18 in peridotite, and the average Is values were within one standard deviation of the values presented in Table 16.5. Axial test results for these two rock types were available for the same borehole locations as the diametral tests. The axial results are lower than the diametral (40%-60% lower within individual lithologies), which could indicate some anisotropic strength in the rock mass.

Table 16.5: Comparison of Feldspathic Peridotite and Peridotite strengths (Eagle Mine, 2022a)

Rock Type	Source	Average Is	Std Dev	# of Tests
Feldspathic Peridotite	Golder, 2005	6.6	2.5	151
	Keel PLT	7.6	2.4	1324
Peridotite	Golder, 2005	8.6	2.8	272
	Keel PLT	6.8	2.5	280

16.3.3.3 Rock Mass Fabric

The interpretation of joint sets in the rock mass for Eagle Main and Eagle East (Table 16.6) was estimated from geotechnical oriented drill holes, downhole geophysical televiewer data, and mapping of underground development in these deposits and is recorded in the GCMP (Eagle Mine, 2022b). There is no oriented core logging, televiewer, or underground mapping data available for Keel. Studies of Keel (Eagle Mine, 2022a) assume that the sets from Eagle Main apply to Keel.

Table 16.6: Dominant Feature Orientations by Geotechnical Domain (Eagle Mine, 2022b)

Domain		Feature Set									
		BED	FOL	Joint Set Dip Direction							
				N	NE	E	SE	S	SW	W	NW
Eagle Main	SED	13/060	61/203	-	-	78/096	90/151	-	-	82/257	82/284
	INT	-	-	-	78/072	45/102	-	88/187	81/213	-	83/307
	MSU	-	-	-	-	-	82/146	84/195	-	-	82/307
Eagle East	SED	27/052	53/201	54/018	62/062	-	82/138	-	-	89/275	-
	INT	-	-	69/009	65/066	86/094	-	85/187	-	-	-
	MSU	-	-	-	-	-	75/124	-	-	69/282	-

16.3.3.4 Major Structures

Information regarding the presence and characteristics of major structures (lithological contacts, faulting, dikes, etc.) was provided to WSP as part of Eagle's GCMP (2022b). The GCMP states that in Eagle Main, post-mineralization faults have been noted near the footwall (south) Peridotite-Siltstone contact and appear to be parallel to the contact, within the intrusive rather than defining the contact. Faulting within the massive sulfides is rare, and faults and joints adjacent to the massive sulfides are infrequent. Faults within the Peridotite are present, but with no observable relative displacement. Veins consisting of quartz-dolomite, calcite- talc, and rare sphalerite-galena have been seen near the margins of the massive sulfide and may represent faults occupied by vein material.

The GCMP states that in the area of Eagle East, one post-mineralization fault, which has been intruded by a gabbro dike, was identified at the west end of the mineralized zone. The orientation of the dike is approximately 60°/335° (Dip/Dip Direction), cross-cutting the host rock and ore zone. Observations of increased rock noise were reported as mining approached the dike, but the gabbro was of good quality, consistent with the host rock sediments. When the dike was encountered in the ore zone, the gabbro was of very poor quality, soft, and highly altered.Excavations through the dike exhibited stress damage, primarily observed through bolt loading and popped bolt plates.

No structural interpretation was available for the Keel ore body for this review. The RQD logging of resource drill holes provided by Eagle and WSP's review of core box photographs suggests that within Keel, there is occasionally damage associated with the mineralized hanging wall contact (typically in the upper areas of Keel) and damage associated with the footwall rock masses. These lower RQD areas occasionally exhibit alteration, which may indicate the presence of a major structure. It is recommended that Eagle develop a structural model for the Keel ore body area to guide mine engineering decisions related to both the stoping areas and long-term development.

16.3.3.5 In Situ Stress

The in situ stress tensor estimated at Eagle is based on measurements completed in Eagle Main and is recorded in the GCMP (Eagle Mine, 2022b).

Table 16.7: In Situ Stress Tensor in Use at Eagle Mine (Eagle Mine, 2022b)

Stress	Dip (°)	Dip Azimuth (°)	Gradient (MPa/m)	K (stress constants)
σ1 (major horizontal)	05	276	0.0745	K_H = 2.76
σ2 (intermediate horizontal)	01	006	0.0373	K_h = 1.38
σ3 (minor vertical)	85	093	0.0270	K_v = 0.027

16.3.4 Stability Implications of the Proposed LOM Design

Eagle provided WSP with a Deswik mine plan to review against the available geomechanical data and stability assessments. The following sub-sections provide WSP's commentary and recommendations regarding the stability of different aspects of the proposed mine plan provided by Eagle Mine staff.

16.3.4.1 Stope Sizing and ELOS

The LOM plan contains 2 stopes in Eagle Main and approximately 40 to 50 stopes in Eagle East, with 3 partial levels of drift and fill to be completed in Eagle East. Commentary on the stope geometry in Eagle Main and Eagle East can be summarized as follows:

- The 2 stopes in Eagle Main are transverse and located on the 265L sub-level (~145 m deep) and include a single primary and a single secondary stope (the primary stope sill drives have already been developed); the sizing of these stopes is similar to the as-built stopes on this sub-level.

- The stope sizes in Eagle East are split by transverse and longitudinal stope orientations, are near vertical, and have common sub-level heights of 25 m (sill floor to sill floor), with the exception of some longitudinal stopes with a 30 m sub-level height.
- The transverse stope geometry (Table 16.8) is consistent with the as-built stope sizes in Eagle East. Stope performance in Eagle East is typically governed by wedge kinematics and induced stress changes. Stope geometry in Eagle East has been previously studied (Eagle Mine, 2022b, WSP, 2022; WSP, 2024; and OHMS, 2024).
- The longitudinal stopes in Eagle East have strike lengths up to 30 m with HW to FW widths of approximately 5 m to 10 m. These dimensions follow the limits set out in the GCMP (Eagle Mine, 2022b).

Table 16.8: Dimensions for Transverse Stopes in the Eagle East (compiled from WSP, 2022; WSP, 2024; Golder, 2005)

	Strike Length (m)	HW to FW Width (m)
Primary	7	20
Secondary	13	40[1]

Note: [1] Maximum secondary length based on CRF strength results.

For Keel, the transverse stopes generally follow the same geometry as Eagle East except there is no difference in strike length between Primary and Secondary stopes (both at 10 m), sub-level heights (sill floor to sill floor) range from 25 m to 30 m (except for 3 stopes which have a 50 m sub-level height), and the HW and FW has variable dip (from 90° to 50°). The longitudinal stopes in Keel have 30 m sub-level heights, generally dip at approximately 50°, have spans less than 10 m, and have variable strike lengths (Figure 16.6).

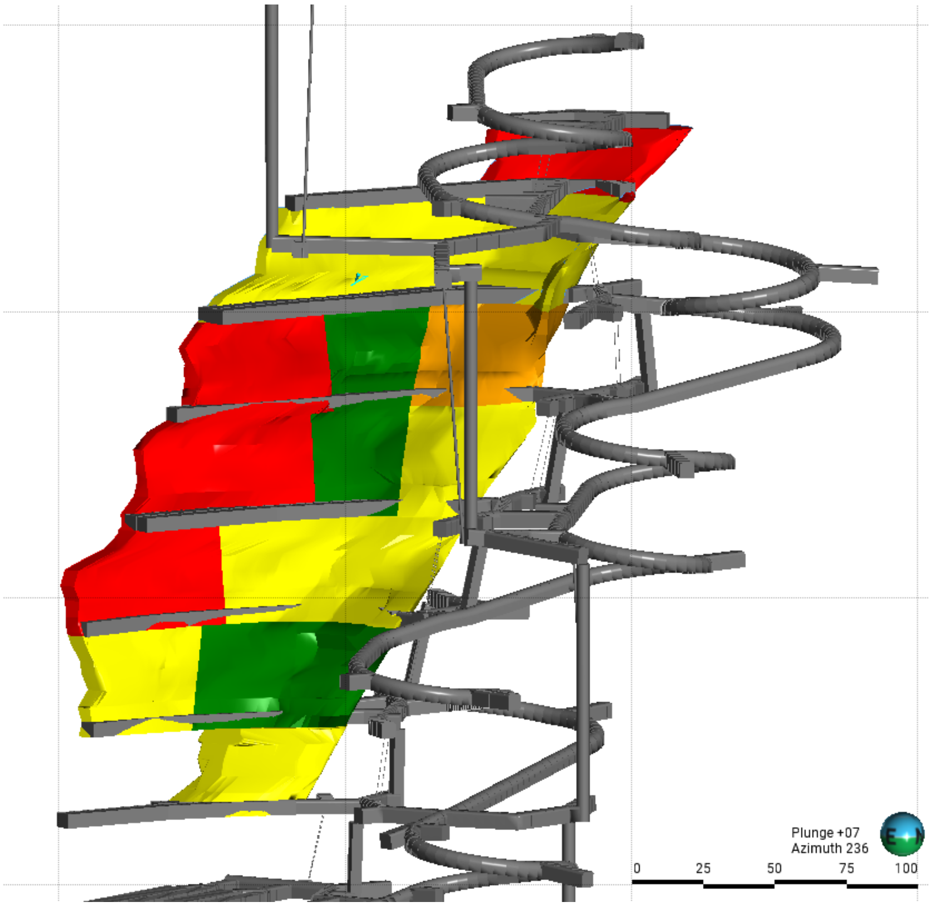


Figure 16.6: Current LOM Upper Keel Longitudinal Stopes Coloured by Strike Length (Green = <35m, Yellow = 35-45m, Orange = 45-55m, Red = >65m)

No assessments were provided to WSP, which examined the stability of the Keel stopes in the LOM. Previous numerical modeling studies (OHMS, 2024, and Eagle Mine, 2022a) considered different (and generally smaller) stope sizes than those provided in the current LOM. The stope geometry used for Keel stopes in the LOM is not aligned with internal recommendations prepared by Eagle's geotechnical engineers (Eagle Mine, 2024), which recommend keeping the transverse stope geometries identical to those used in Eagle East and limiting the longitudinal stope strike lengths to 35 m for those stopes dipping at less than 80°. WSP understands that the internal Talon stope geometry recommendations for Keel were based on as-built stope performance in Eagle East; the stope performance data used to produce these recommendations was not available for review by WSP.

Stope stability was reviewed empirically by WSP using the Matthews Stability chart method with input parameters (Q', A, B, and C) derived from data made available by Eagle Mine. The stope stability parameters (as described in Potvin, 1988) assumed by WSP were as follows:

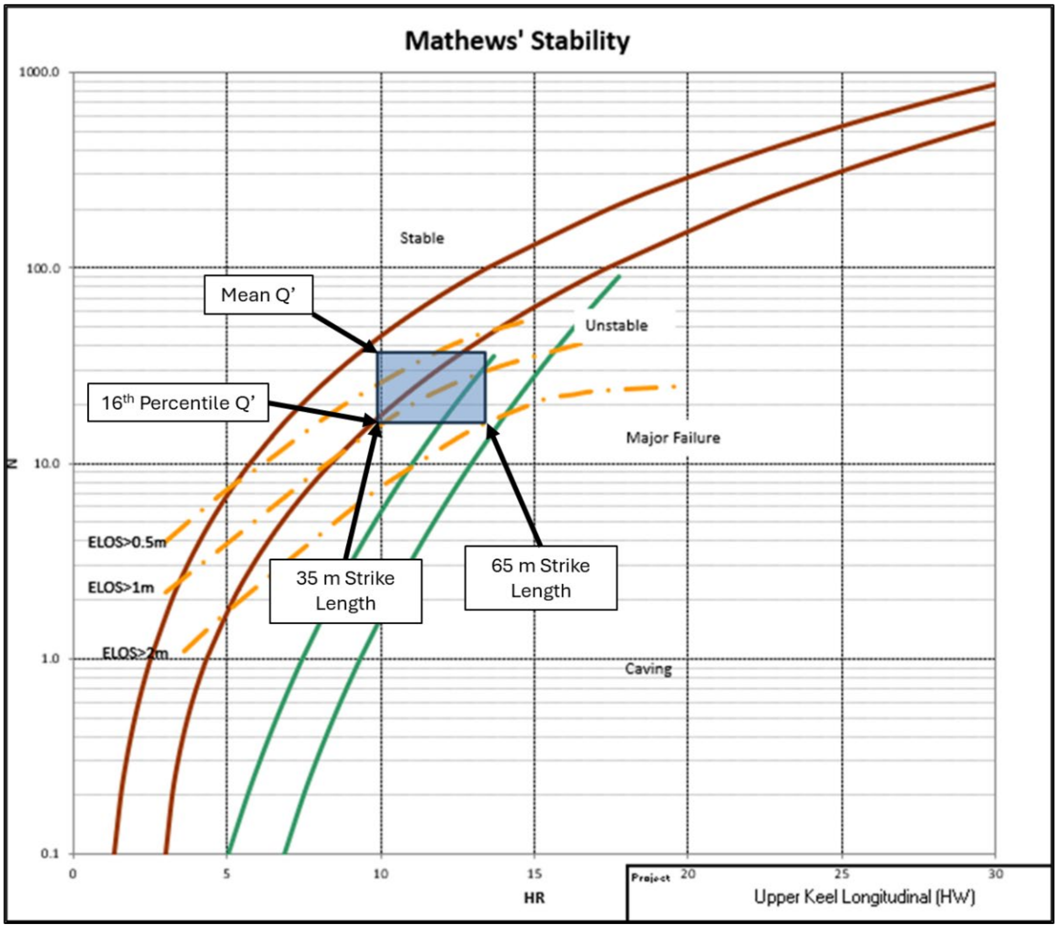
- Q' of 16.9 to 19 (for Eagle East) and 15 to 30 (for Keel). This is based on the possible average and lower bound (defined as the 16th percentile) Q' parameters for the Intrusive domain in Table 16.3 and for the Feldspathic Peridotite in Table 16.2.
- A factor range from 0.1 to 0.8 (in Eagle East and lower Keel) and 0.8 to 1 (top of Keel).

- The A factor in Eagle East ranges from 0.1 to 0.8 based on previous studies (WSP, 2022; WSP, 2024; Eagle Mine as-built data); however, it should be noted that WSP (2022) suggested that an A factor of 0.1 was likely conservative for Eagle East.
- The values for upper and lower Keel are assumed based on images from OHMS (2024) (specifically Figure 8-10); however:
- The provided figure shows only the stresses at the end of mine life, which are likely inaccurate for each individual stope face.
- The image itself is not of good quality, and
- The OHMS study was examining an older version of the LOM plan and sequence, making the results potentially different from what could be expected from the current LOM plan and sequence.
- B values range from 0.2 to 0.4, with 0.3 being typical for the stope faces. These parameters are selected directly from 11 as-built stope stability assessments provided by Eagle from stopes in Eagle East (WSP, 2022). This value is an assumption for Keel, as no structural orientation data is available within the Keel ore body that could be used to revise the B factor.
- C values range from 4 (for 50° dipping faces) to 8 (for 90° dipping faces). WSP (2022) suggested that C values be selected (where appropriate) based on gravity and slabbing mechanisms.

It was noted by WSP (2022) that the empirical stability calculations performed by Eagle for Eagle East did not correlate well with the as-built conditions of the stopes; typically, the stope would perform better than the stability chart would suggest. This provides further evidence that some of the values selected for this assessment (based on historic assessments) are potentially conservative.

The stope stability empirical review (considering the stability factors and assumptions mentioned above) suggests that generally the stope geometries proposed in the LOM mine are likely stable when considering moderate stress conditions (A ≥ 0.3), Q' values ≥ 16.9, B factors of 0.3, and gravity-driven C factors. There are some exceptions to the above statement:

- Longitudinal stopes in upper Keel that have strike lengths less than or equal to 35 m are likely to be stable under typical rock mass and stress conditions. Stopes with strike lengths larger than 35 m may require paneling and have increased dilution (Table 16.8).
- The transverse stopes on the -245L sub-level have a 50 m sub-level height and have an increased potential for instability and dilution. These are likely to need paneling from an additional sub-level drive at -220L.
- Areas of poorer rock mass characteristics may still be encountered in areas of Eagle East or Keel that may necessitate local stope adjustments.
- The stope stability statements made in this Technical Report do not consider kinematic wedge potential. This remains a gap that will need to be closed in future study stages.



Potvin (1989), Unsupported Transition curves, Nickson (1992) supported curves, and Clark and Pakalnis (1997) ELOS curves are shown.

Figure 16.7: Stope Stability Plot Results for the Upper Keel Longitudinal Hanging Wall Considering a Range of Input Parameters

Equivalent linear overbreak/slough (ELOS) assumptions for LOM stopes in the Eagle East and Keel deposits were based on Clark and Pakalnis (1997) ELOS curves plotted on the stope stability chart. The results of the ELOS check are shown in Table 16.9, based on the stope stability input parameter ranges described above. The ELOS assumption does not account for wedge kinematics; this remains a gap in the assumptions, which can be mitigated by reconciling overbreak of as-built stopes in Eagle East. As-built stope overbreak data in Eagle East were available individually, by stope, but have not been compiled and reconciled based on aggregate statistics (mean overbreak, range in overbreak, correlated to different stope sizes, etc.). As-built reconciled overbreak statistics would represent the highest confidence data to forecast future overbreak for stopes of similar size in similar rock mass conditions; it is recommended that Eagle compile the as-built overbreak data and review these ELOS values against aggregate as-built overbreak statistics.

Table 16.9: Assumed ELOS for Each Stope Face

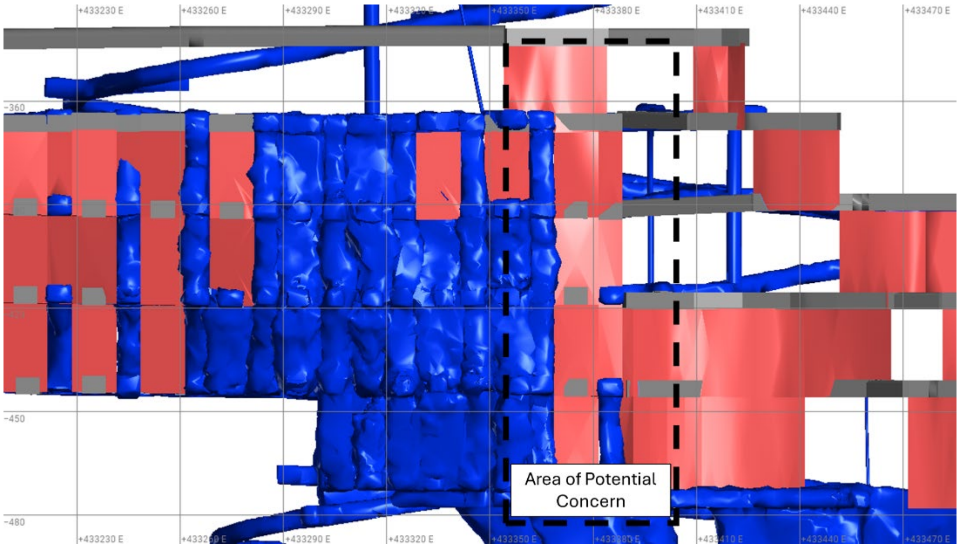
Stope Face of Interest	ELOS (m)
Upper Keel Longitudinal Stope (HW) - Considering 35 m Strike Length	<0.5 to 1
Upper Keel Longitudinal Stope (HW) - Considering 45 m Strike Length	0.5 to 1.25
Upper Keel Longitudinal Stope (HW) - Considering 55 m Strike Length	0.75 to 1.75
Upper Keel Longitudinal Stope (HW) - Considering 65 m Strike Length	0.75 to 2
Upper Keel Longitudinal Stope (EW)	<0.5
Upper Keel Longitudinal Stope (FW)	<0.5 to 0.5
Transverse Stopes (Keel and Eagle East) (EW)	<0.5 to 1.75
Transverse Stopes (Keel and Eagle East) (HW)	<0.5 to 1.5
Transverse Stopes (Keel and Eagle East) (FW)	<0.5 to 1
Eagle East Longitudinal (HW)	<0.5 - 0.75
Eagle East Longitudinal (FW)	<0.5 - 0.75
Eagle East Longitudinal (EW)	<0.5

16.3.4.2 Pillar Stability

Pillars at Eagle Mine are mostly temporary and diminishing based upon the selected mining sequence (e.g., diminishing sill pillars in the Keel longitudinal area and temporary pillars where secondary stopes in the transverse mining areas have yet to be taken). This section reviews the provided stability assessments for interpretations of pillar stability.

There is no available study that has assessed stability due to induced stress changes for the current LOM plan and sequence. Four previous studies (WSP, 2022; Eagle Mine, 2022a; WSP, 2024; and OHMS, 2024) have assessed stability in Eagle East, in Keel, or in both. These studies suggest the following:

- Temporary pillars representing secondary stopes in Eagle East may experience increased stress concentrations and have the potential to produce stress damage and seismicity on the East side of the Eagle East transverse mining area (Figure 16.8) (WSP, 2022, and WSP, 2024). The transverse stopes in this area are almost completely mined out, but some remain to be taken, and the as-built stopes are nearly vertical across four sub-levels, potentially increasing the stress on this East abutment. This area may present stress challenges for secondary stopes and their accesses, which could impact development speed, rehabilitation needs, and ground support requirements.



The area of stress concern previously identified (WSP, 2022, and WSP, 2024) is outlined.

Figure 16.8: Eagle East Looking North Showing As-Built Development (Blue) and LOM Stopes (Red) and Development (Grey)

- The temporary sill pillars in upper Keel are likely to have less induced stress potential and rock mass damage (OHMS, 2024, and Eagle Mine, 2022a); however, this should be confirmed with updated numerical modeling.
- The LOM plan and sequence assessed by OHMS (2024) assessed an outdated LOM, and the resulting model output images typically only exhibited the end-of-life stress state of the mine, which is not useful for assessing the stability of temporary pillars during mining. Ultimately, this study was not of much use for indications of pillar stability, although it does provide useful insight into other topics (drift stability and approximate end-of-life stress state).
- An updated numerical model must be completed for the LOM plan and sequence during the next study stages. This numerical model may result in local changes to pillars, sequencing, ground support, and infrastructure offset distances.

16.3.4.2.1 Keel Crown Pillar

The vertical distance from the top of the upper stoping level in Keel to the surface topographic survey is approximately 210 m. The vertical distance from the back of the upper stoping level in Keel to the decline above Keel is approximately 190 m; WSP understands that this 190 m is in rock. WSP does not know how thick the overburden is above Keel and cannot confirm if the thickness of the rock crown pillar is greater than 190 m.

A Keel crown pillar stability review was completed by Eagle Mine (2023) for the 2023 LOM design, which considers different stoping dimensions than what is proposed in the current LOM. The crown pillar stability review included empirical stability estimates (scaled span) and 2D elastic numerical assessments. The stability review concluded that the upper Keel footprint is relatively small with a relatively large crown pillar thickness (~190 m), that the probability of failure (from the scaled span assessment) is less than 1%, and that long-term crown pillar stability in upper Keel is achievable through tight filling of mine workings (Eagle Mine, 2023). WSP understands that there is no structural model of the crown pillar rock mass at Keel. It is recommended that, during the next study stage, Eagle update the crown pillar stability assessment for the current LOM and consider the implications of a structural model.

16.3.4.3 Ground Support

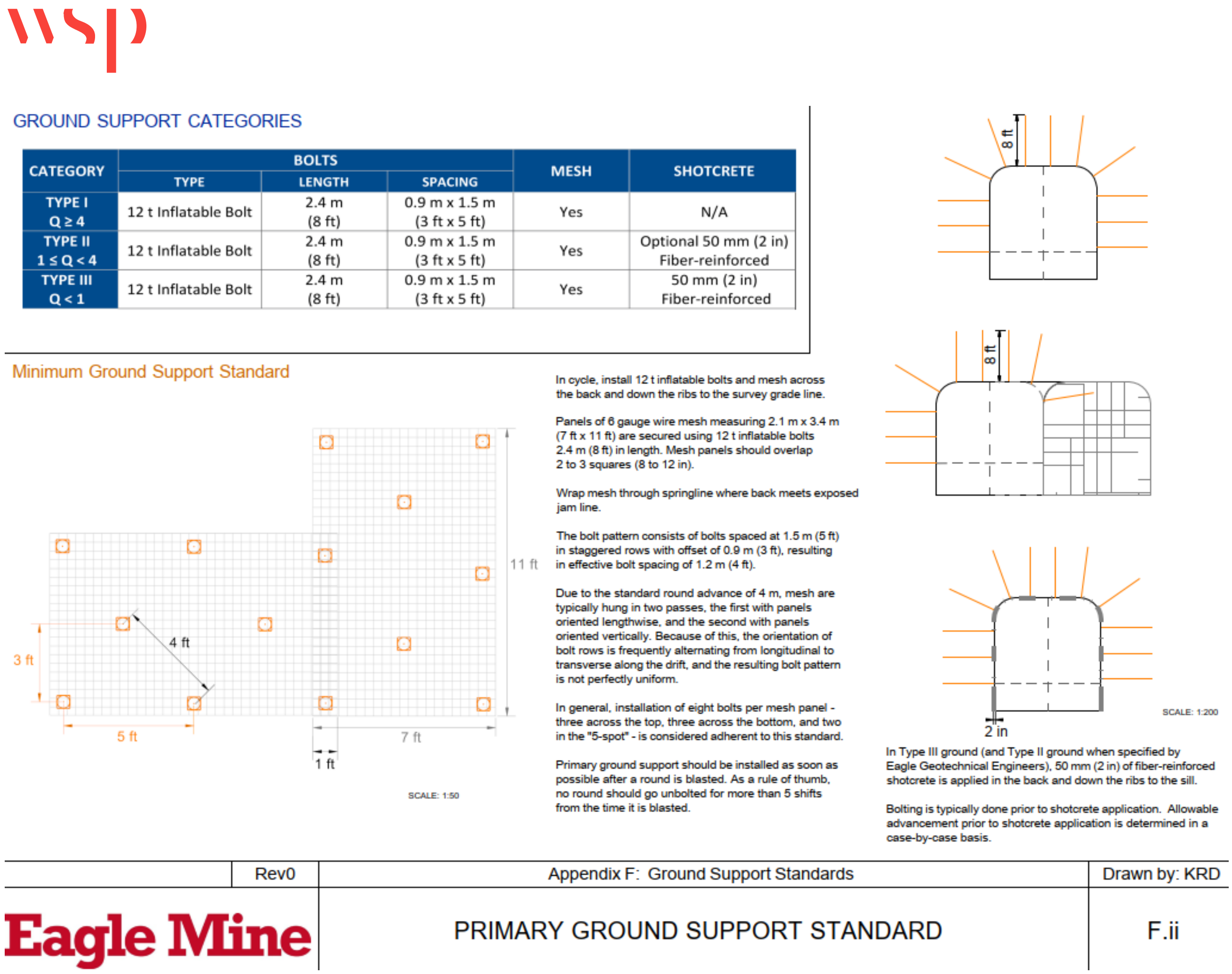
Ground support at Eagle is based on the rock mass quality "Q" index. Three categories of support exist: Type 1 support for Q > 4, Type 2 support for 1 < Q < 4 and Type 3 for Q < 1. Specifications for the installed rock support for each rating category are defined below.

Type 1 Ground (Q 4) - Pattern bolting consisting of 2.4 m (8 ft) fully encapsulated resin rebar bolts or inflatable bolts on a 1.5 m by 1.8 m (5 ft by 6 ft) spacing with galvanized welded wire mesh (6 gauge with 10 cm (4 in) wire spacing). In addition, there is an overlapping “5-spot” pattern of the same dimensions with an offset of 0.75 m by 0.9 m (2.5 ft by 3 ft).

Type 2 Ground (1 < Q < 4) - Pattern bolting consisting of 2.4 m (8 ft) fully encapsulated resin rebar bolts or inflatable bolts on a 1.5 m by 1.8 m (5 ft by 6 ft) spacing with galvanized welded wire mesh (6 gauge with 10 cm (4 in) wire spacing). In addition, there is an overlapping “5-spot” pattern of the same dimensions with an offset of 0.75 m by 0.9 m (2.5 ft by 3 ft) and an optional 5 cm (2 in) thick application of shotcrete. Shotcrete contains a fiber additive at a dosage of 1.5 lbs/yard batched.

Type 3 Ground (Q < 1) - Pattern bolting consisting of 2.4 m (8 ft) fully encapsulated resin rebar bolts or inflatable bolts on a 1.5 m by 1. 8 m (5 ft by 6 ft) spacing with galvanized welded wire mesh (6 gauge with 10 cm (4 in) wire spacing). In addition, there is an overlapping “5-spot” pattern of the same dimensions with an offset of 0.75 m by 0.9 m (2.5 ft by 3 ft) and a mandatory 5 cm (2 in) thick application of shotcrete. Shotcrete contains a fiber additive at a dosage of 5 lbs/yard batched.

Additional ground support measures, such as “spot” bolting to increase the tightness of the mesh to the back, may be installed in areas where deemed necessary by Eagle staff. Bolting and mesh are installed across the back and down the ribs, to the survey grade line. Fully encapsulated resin rebar is used as the primary bolt element in headings with moderate to high stress damage, in areas of high potential corrosion (see Table 16.11), and in non-temporary headings. Figure 16.9 summarizes the three types of primary support based on the Q index. The dimensions of Eagle underground openings are listed in Table 16.10.



GROUND SUPPORT CATEGORIES

CATEGORY	BOLTS			MESH	SHOTCRETE
	TYPE	LENGTH	SPACING		
TYPE I Q ≥ 4	12 t Inflatable Bolt	2.4 m (8 ft)	0.9 m x 1.5 m (3 ft x 5 ft)	Yes	N/A
TYPE II 1 ≤ Q < 4	12 t Inflatable Bolt	2.4 m (8 ft)	0.9 m x 1.5 m (3 ft x 5 ft)	Yes	Optional 50 mm (2 in) Fiber-reinforced
TYPE III Q < 1	12 t Inflatable Bolt	2.4 m (8 ft)	0.9 m x 1.5 m (3 ft x 5 ft)	Yes	50 mm (2 in) Fiber-reinforced

Notes: Note that fully encapsulated resin rebar bolts are used instead of inflatable bolts in areas with moderate to high stress damage, in areas of high potential corrosion (see Table 16.11), and in non-temporary headings.

Figure 16.9: Primary Ground Support Standard from the GCMP (Eagle Mine, 2022b).

Table 16.10: Excavation Dimensions Proposed in the LOM

Excavation Type	Span (m)	Height (m)
Decline	5.5 (18 ft)	5.5 (18 ft)
Muck bays	5.5 (18 ft)	6.0 (20 ft)
Level access	5.0 (16 ft)	5.5 (18 ft)
Footwall drive	5.0 (16 ft)	6.0 (20 ft)
Stope accesses	5.0 (16 ft)	5.3(17.5 ft)
Eagle Sill cuts (primary)	10.0 (33 ft)	5.3(17.5 ft)
Eagle East Sill cuts (primary)	5.0 (16 ft)	5.3(17.5 ft)
Sill cuts (secondary)	5.0 (16 ft)	5.3(17.5 ft)

Secondary support at Eagle consists of a pattern of 3.7 m (12 ft) Super Swellex bolts (for temporary headings only, not experiencing stress damage), 3.7 m (12 ft) fully encapsulated rebar bolts (for permanent or stress-damaged headings of limited width), or 6 m (20 ft) cable bolts (for permanent or stress-damaged headings). Both are installed on a 1.83 m by 1.83 m (6 ft by 6 ft) pattern through the primary support pattern. Cable bolts are plated and tensioned (5 tons). Secondary support is typically installed at Eagle in intersections, critical excavations, and excavations with spans greater than 6.0 m.

Face support is required to be installed in stressed ground, as identified by the site geotechnical engineers, including in all primary transverse stope headings in Eagle East. The face bolting standard consists of installing support (screen and bolts) before drilling the round. The screen is installed with a 0.6 m (2 ft) overlap on the back to within 3 m (10 ft) from the floor. The bolting pattern is 1.2 m by 1.5 m (4 ft by 5 ft). The screen is installed on the face as tightly as possible to the side walls with bolts installed at a maximum of 1.5 ft from the walls.

Recent rock mass damage and ground support performance observed by Eagle staff in Eagle East have resulted in changes to the ground support patterns and bolt elements in use at Eagle (e.g., replacing inflatable bolts with resin rebar in permanent headings and headings experiencing stress damage, increasing the length of cable bolts in stope brows which are under high stress, etc.). Based on observations of bolt corrosion and ground support performance concerns, Eagle has adjusted the bolt elements to be used in Eagle based on potential exposure time of the elements to corrosion (Table 16.11).

Table 16.11: Corrosion Protection Based on Expected Excavation Lifespan

Element	Open < 60 Days	Open > 60 Days	
		Production	Development
BOLTS	Inflatable Non-coated	Inflatable K2 plastic coated	#7 rebar
BOLT PLATES	Non-coated	K2 plastic-coated	Non- coated
MESH	Non-galvanized	Galvanized	Polymer

The studies provided to WSP do not review the potential stability implications on ground support design for Keel, aside from the OHMS (2024) numerical modeling study. The OHMS study used an outdated LOM but suggested that sub-level access drifts are likely to experience increased stress damage; however, the worst damage estimates were in Eagle East.

Assuming ground conditions do not practically change between the Eagle East and Keel deposits, corrosion monitoring and potential rehabilitation are accounted for during LOM, and that the induced stress continues to decrease as mining moves upwards (OHMS, 2024), the ground support included in the LOM is likely reasonable for most openings; although, it must be verified with stability assessments using the latest LOM layout and sequence. Residual uncertainty remains as follows:

- The amount of rock mass with poor characteristics that the Keel ramp and sub-level access drifts will encounter is unknown, as minimal geotechnical data has been collected in the infrastructure areas at Keel.
- Discrete structures (e.g., faults, poor quality lithological contacts, etc.) are likely to be encountered and will require heavier ground support (similar to what has been done elsewhere in the mine when drifting through faults).
- Induced stress impacts on drifting need to be examined for the proposed LOM drifting in the Eagle East and Keel, as previous studies utilized outdated LOM plans and sequences.

- The kinematic wedge potential must be examined for drifting in the Keel based on structural orientation data to be collected within the Keel mining area.
- Bolt plates in long-term development drifts do not consider corrosion protection; this may result in loss of bolt plates due to corrosion over the LOM, potentially impacting mesh and bolt performance. A ground support and corrosion monitoring program is in place to help manage and mitigate this risk.

16.3.4.4 Backfill Strength

The minimum cemented rock fill (CRF) backfill strength estimated for Eagle Mine is based on empirical calculations completed during a geotechnical study by Golder (2005); the estimated strength of 1.5 MPa is provided in the GCMP (Eagle Mine, 2022b). The backfill strength assumes transverse stoping mined overhand with a primary – secondary sequence, in which the primary stopes are backfilled with CRF and the secondary stopes are backfilled with uncemented rock fill.

The LOM provided for this study continues the same mine sequence for the transverse stopes (primary – secondary overhand), and the stope sizes are similar to what was considered in the previous backfill study (Golder, 2005) and what has been used to date in Eagle Main and Eagle East.

The longitudinal stopes in the LOM in Upper Keel include some stopes that are undercut and will result in CRF in the backs of stopes. An assessment of CRF stability when undercut has not been completed to WSP's knowledge. Mitchell's method (1991) suggests that, for the underhand longitudinal stopes in Keel, the CRF strength may need to increase to maintain a similar factor of safety to what was recommended by Golder (2005); however, the dip of the longitudinal stopes (~50°) is likely to improve CRF performance. Stope dip is not something explicitly assessed by Mitchell's method (1991). It is recommended that Eagle complete an assessment of CRF stability for underhand stopes in Upper Keel and revise the target CRF strength estimate as necessary.

16.3.4.5 Vertical Infrastructure Stability

The LOM plan includes new ventilation (~4.5 m diameter), orepasses (~4 m diameter), and escapeways (~1.2 m diameter) to be developed along the Keel ore body. To date, WSP is not aware of instability in the as-built ventilation raises (~4.5 m diameter) in Eagle East or in Eagle Main. No geotechnical data is available at the location of the proposed LOM vertical development near the Keel ore body. The proposed offsets between the LOM stopes and the ventilation raises in Keel are a minimum of 70 m. The proposed offset for the orepasses ranges but could be as close as 15 m (which is closer to the stopes than the as-built orepasses in the other ore bodies). The closer proximity of the LOM orepasses to the Keel stopes may indicate that the past performance of vertical development in Eagle East and Eagle Main may not be applicable in Keel.

The most recent numerical model (completed on an outdated LOM layout and sequence; OHMS, 2024) suggests that the vertical development will experience adverse ground conditions due to induced stress changes below -345 m asl. The LOM plan provided to WSP has no new vertical development proposed below -345 m asl.

To WSP's knowledge, no kinematic stability or rock mass stability assessments (e.g., wedge stability, McCraken and Stacey, etc.) have been completed for the proposed vertical developments. Based on assessments following McCraken and Stacey (1989), a minimum Q value of 6 is likely necessary throughout the raise to meet a 5% probability of failure for raises with a 4.5 m diameter. Given most rock at Eagle typically has better quality than a Q of 6, it is likely that suitable rock mass can be found in which to stage the vertical development.

It is recommended that the proposed LOM raises:

- Be drilled and logged geotechnically and surveyed with a downhole geophysical televiewer.
- Examined for kinematic stability.
- Examined for rock mass stability (McCracken and Stacey and numerically as part of a wider LOM numerical stress model.
- The offset of the orepasses from the stopes should be reviewed against induced stress changes as part of an updated mine-wide numerical induced stress model.

16.3.4.6 Mine Plan Commentary

This section provides a list of areas of the mine plan that may introduce risk to production and stability. These areas should be assessed for stability and refined as necessary in the next stages of study:

- The LOM stope sequence varies from what was assessed by OHMS (2024). The current sequence should be assessed in a numerical model to confirm it does not produce unreasonable stress on excavations during mining.
- The sub-level sill access drifts for sub-levels 200L and 170L in Keel intersect the sill drift from the HW and have a minimal pillar (< 3 m) between the access drift floor and the HW of the stopes. During stope blasting, it is likely the drift floor will be damaged, which will likely increase the time and difficulty in backfilling the stope to regain access. Such drift orientations may require the use of alternative backfill materials (other than rock fill or CRF) to ensure safe and stable re-entry to the sill drift. It is also possible that damage may be such that re-entry is not possible.
- Some orepasses and development are located on the FW of the Keel orebody near to resource drilling, which was logged with lower than typical RQD values (e.g., sub-level 40L). Core box photograph review suggests the FW in this area may have poorer ground characteristics. Excavations planned in this area may require heavier ground support and result in slower development times.
- The offset distances of access drifting and orepasses from the Keel ore body can be as low as 15 m. Updated numerical stress modeling of the LOM plan and sequence should be completed to understand if this is a stability risk. The consequence of this may be adjustments to the offset, ground support requirements, or development times.
- The easternmost longitudinal stopes in Eagle East are sequenced from east to west which produces a diminishing pillar. It is possible this diminishing pillar may be overstressed and should be assessed in an updated numerical model.
- A 50 m high stope in Keel is planned on the -245L sub-level. This stope is likely to be unstable. It is likely that a mid-height sill drift at -220L would need to be developed, or this stope risks instability / increased dilution.

16.3.5 Recommendations

The following items are recommended for future study stages to mitigate known uncertainty:

- Reconcile existing PLT, laboratory intact strength data, and geotechnical logging data to identify potential data gaps that should be closed through additional data collection.
- The above reconciliation and review should also consider the possibility of anisotropic intact rock strengths based on PLT and intact laboratory testing results.
- The reconciliation and review should identify where poorer ground is expected in the LOM and may result in updated stability assessment input parameters.
- Q is estimated based on empirical relationships, which are generalized and may not be fully applicable to the rock mass at Eagle Mine. Future geotechnical data collection and reconciliation efforts should focus on capturing Q parameters to directly estimate Q values from the core information.
- Rock mass fabric orientation in Keel is assumed. Eagle should collect additional structural orientation data (possibly from downhole geophysical televiewer surveys) to verify that structural orientation has not varied in Keel.
- A structural model for the Keel ore body should be developed.
- Complete the following for the proposed LOM mine plan and sequence:
- Mine-wide numerical model examining changes in induced stress and their implications on stability.
- Review stope, infrastructure, sequence, ground support, and pillar stability based on the mine-wide numerical model and data reconciliation efforts.
- Review ELOS estimates based on the achieved as-built overbreak in Eagle East.
- Review stability recommendations for stopes and infrastructure based on wedge kinematics (this should be done after orientation data is captured in Keel).
- Review backfill strength for stopes that are undercut.
- Review proposed longitudinal stope strike lengths in Keel based on the above assessments and reviews.
- Review and address (as necessary) potentially challenging mine layout items listed in Section 16.7.6.

16.4 Mine Design

The Mineral Reserves estimate is based on a mine design and schedule that was prepared in Deswik software. The design undertaking requires estimation of numerous parameters related to production rates and the determination of dimensions of underground excavations, from input provided by geotechnical engineers.

Figure 16.10 summarizes the dimensions used for ramps, level development, in-ore drifts, and other excavations.

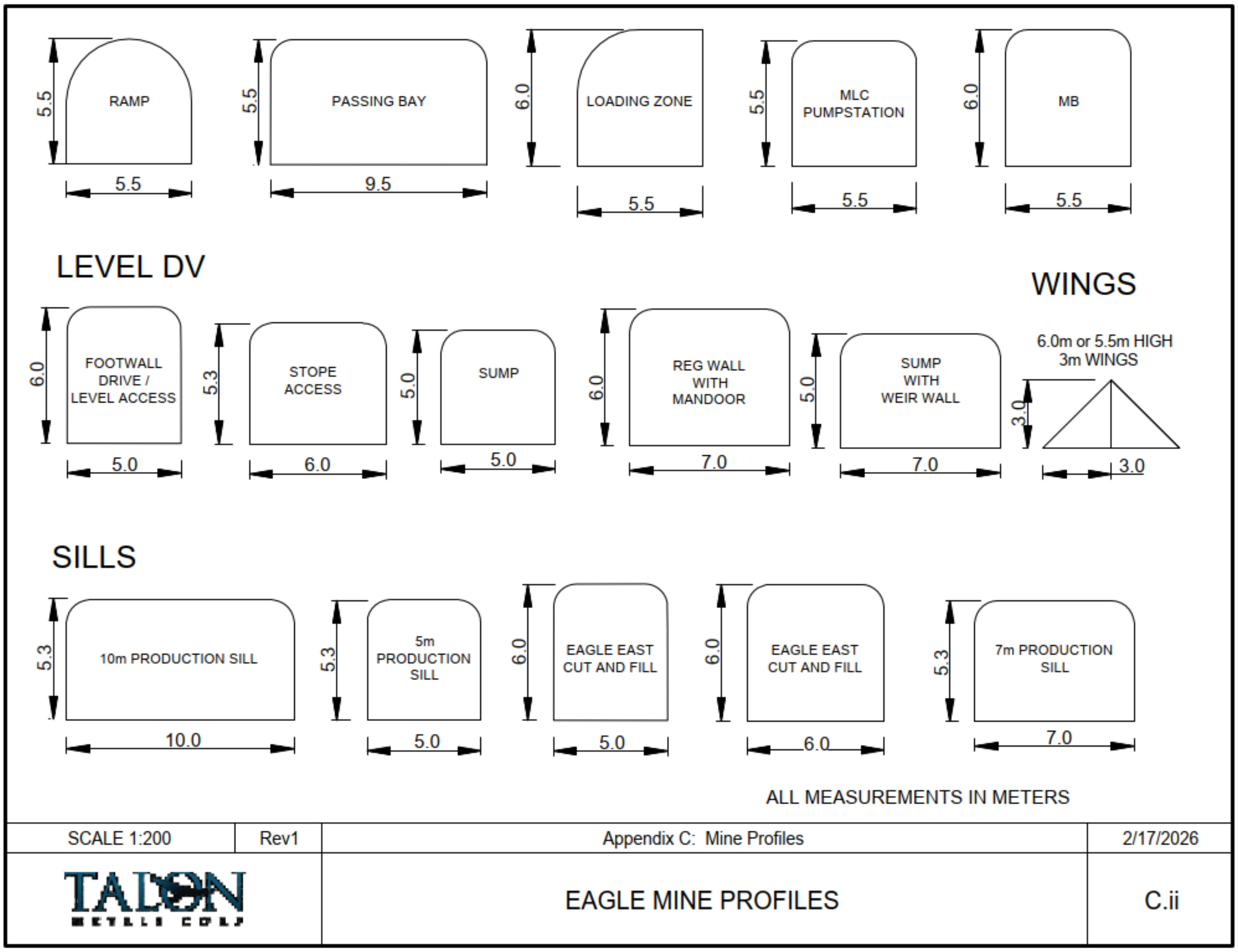


Figure 16.10: Drift Dimensions

Preliminary stope shapes are created using Deswik Stope Optimizer (DSO) software with respect to the geotechnical and economic criteria. The stope dimensions and design parameters were established by the Eagle Mine team. General development to access the stopes and major infrastructures is subsequently designed and optimized.

Figure 16.11 shows plan views of the dimensions adopted for transverse sublevel open stopes. Table 16.3 summarizes the different dimensions for the transverse and longitudinal sublevel open stopes

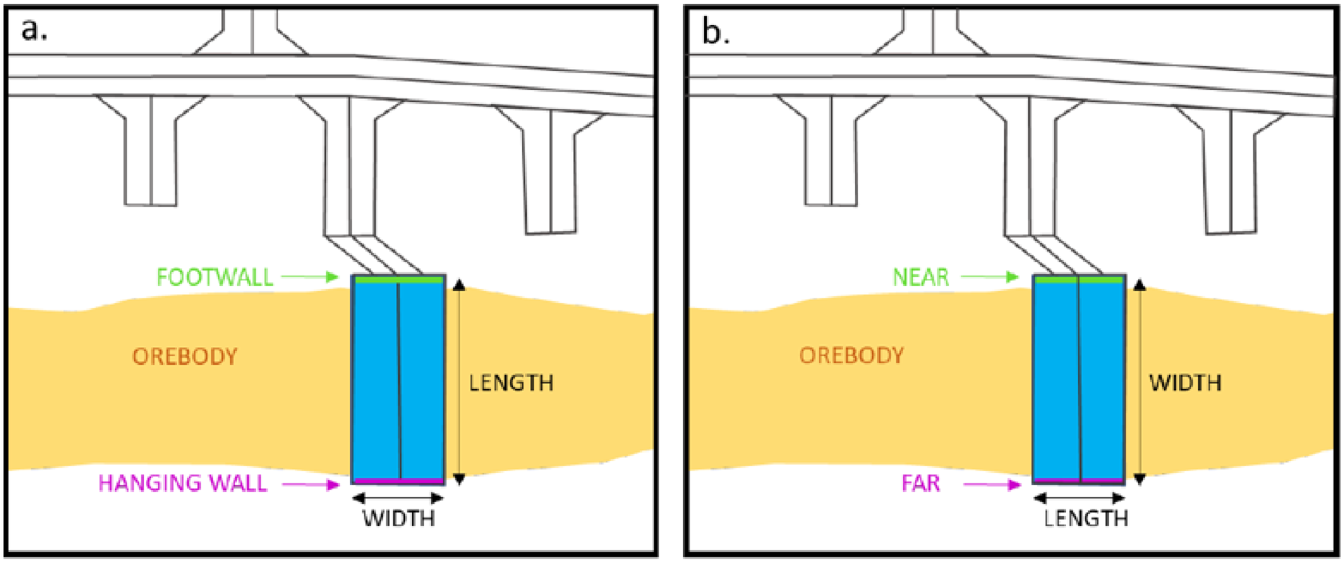


Figure 16.11: Dimensions for Transverse Sublevel Open Stopes (plan view)

Table 16.12: Dimensions for Sublevel Open Stopes

Stope Height	**Transverse**	Determined by level spacing, which ranges between approximately 25 and 30 meters
	Longitudinal	Determined by level spacing, which ranges between approximately 28 and 33 meters
Stope Width	**Transverse**	Stope widths range from 7 to 11 meters in primaries, and up to 15 meters in secondaries.
	Longitudinal	Longitudinal stopes range from 5 to 15 meters wide.
Stope Length	**Transverse**	Limited to 20 m for primary stopes and 35 m for secondary stopes. Primary stopes longer than 20 m are broken into multiple panels.
	Longitudinal	Length of stopes varies from 20 meters to less than 50 meters.
Strike and dip	**Transverse**	Strike and dip of the stope walls are defined using the apparent dip convention.
	Longitudinal	Strike and dip of the stope walls are defined using the apparent dip convention.

Source: Eagle Mine, 2026

Stopes are then sequenced following the geotechnical recommendations and production activities are scheduled using Deswik software modules.

The mine is constrained by ore haulage, backfill capacity, and lateral advance rates. These are built into Deswik as summarized in Table 16.13, Table 16.14, and Table 16.15.

Table 16.13: Production and Development Rates – Ore Tonnage

		Maximum Qty	Unit	Application
Global Constraint		787,000	t/yr	Over-the-road Haulage
Eagle		2,000	t/d	Stope Mucking Rate
Eagle East		2,000	t/d	
Keel	Lower	2,000	t/d	
	Middle	2,500	t/d	
	Upper	4,000	t/d	

Source: Eagle Mine, 2026

Table 16.14: Production and Development Rates – Backfill Capacity

		Maximum Rate		
		m^3/d	Trucks/d	t/d
Global Constraint		1,015	76	2,309
Eagle	Jam	870	65	1,974
	Drop Fill	1,200	89	2,703
	Gob	785	59	1,434
Eagle East	Jam	725	54	1,640
	Drop Fill	785	59	1,792
	Gob	850	63	1,531
Keel	Jam	1,000	75	2,278
	Drop Fill	870	65	1,974
	Gob	850	63	1,531

Source: Eagle Mine, 2026

Table 16.15: Production and Development Rates – Lateral Advance

	Development Type	Units	2026	2027	2028	2029	2030
Global Constraint	All	m/wk	105	105	105	105	105
Eagle	All	m/d	5.2	5.2	5.2	5.2	5.2
Eagle East	Capex	m/d	7.5	5	5	5	5
	Opex (excl. D&F)	m/d	7.5	5	5	5	5
	Drift & Fill	m/d	5	5	5	5	5
Keel	Capex	m/d	8	16	12	12	12
	Opex	m/d	4	8	6	6	6

Source: Eagle Mine, 2026

The parameters and assumptions for dilution and mining recovery are discussed in Item 15 of this Technical Report.

16.4.1 Backfill

16.4.1.1 Cemented Rockfill

Eagle Mine uses cemented rockfill (CRF) and uncemented rockfill (URF) to backfill mined stope voids. CRF is used to backfill the drifts in D&F mining and the primary stopes in transverse sublevel open stoping (TSLOS). URF is used to backfill secondary stopes in TSLOS. The backfill is hauled to stopes, and D&F drifts by the same mine trucks that transport ore to the surface. Trucks are equipped with ejector boxes that allow them to dump backfill directly into the required location, even in areas with low back clearance, without raising the truck box.

CRF is prepared on the surface at a backfill plant located at the mine site. The plant is a continuous mixer-type plant, capable of producing 2,000 tonnes per day. The CRF is prepared using recipes dependent on the mining zone and mining method. For example, the CRF used in D&F requires a less-fluid, stickier consistency than that used in TSLOS so that it can be tightly placed at a steep angle up to the back of the excavation.

The CRF composition utilizes mine development rock as a principal component, with sand added to improve gradation. The physiochemical composition of the CRF is:

1. 81.7% mine development rock or an approved substitute 3”-minus aggregate
2. 9.3% screened natural sand
3. 5% Type 2 Normal Portland cement (NPC)
4. Water: cement ratio (w:c) = 0.5 to 1.0
5. 2.5 oz/hundred weight NPC Euco-Fill 25 (Euclid Chemical Company) admixture

For quality control, the CRF used in SLOS and the D&F headings are tested utilizing the ASTM test method C39 for compressive strength. These tests consist of filling 6-inch cylinder casts (L:D = 2) with material sampled from underground trucks. Samples are typically collected every other day when CRF batching occurs, and are cured for 24 hrs, 72 hrs, 7 days, and 28 days prior to testing. A database exists at the mine for the recording of test results.

About half of the aggregate for backfill comes from development waste hauled to the surface and stockpiled at the mine site. It is crushed to less than 75 mm (3 in) before being fed to the backfill plant. The mine does not presently generate sufficient development waste to meet its backfilling requirements, so the remainder is purchased from two local quarries. This material, crushed to the required size, is delivered to the mine site by trucks.

The URF used for backfilling secondary stopes can be run-of-mine development waste without crushing. As much as possible, waste from development headings is hauled directly to and dumped into the stopes. In other cases, waste stockpiled on the surface is loaded into mine trucks and hauled back underground.

The site has established guidance concerning required CRF cure times in the proximity of blasting. The guidance is based on historical CRF cure data and provides recommended cure times based on anticipated blasting PPVs calculated for typical blasting charge weights over a range of distances.

16.4.1.2 Paste Backfill

Eagle Mine is currently investigating utilizing paste backfill as the backfill method for the upper and middle sections of the Keel in their underground mine to reduce operating costs and improve project economics. To generate the paste backfill product, Eagle Mine will convert its operating cemented aggregate rockfill (CAF) plant to produce paste backfill. The process will involve feeding purchased sand into a continuous mixer where it is blended with cement and water to produce paste backfill. The paste overflows from the mixer to a hopper, where it flows to a hydraulic piston paste pump. The design utilizes as much existing equipment as possible to minimize capital costs. Main process equipment upgrades that are expected are:

- Upgraded binder transfer screws.
- Increased water storage.
- High-pressure flush pump.
- A paste pump and hopper.
- Modifications to the mixer.

The paste is pumped from the paste plant into the mine's underground workings. The paste pipeline will be routed down the mine access ramp to muck bay 2, where a borehole will be drilled to the upper levels of the Keel orebody. The paste will then flow through a series of interlevel boreholes and to the correct stope for placement. Eagle Mine plans to only be mining one or two stopes at a time, so pipe changeovers are expected to be mostly manually performed in between pours."

16.5 Mine Infrastructure

During the site visit, the QP observed the underground infrastructure, mine services, and fixed equipment described in Item 18 of this Technical Report. The QP is of the opinion that they are appropriate for the scale of the Eagle Mine. Furthermore, these installations were observed to be of high quality and in working order, functioning normally during the underground tour.

16.5.1 Mine Access

The underground workings are accessed via the main ramp, which has its portal entrance within the industrial area of the mine site. 5.5m wide by 5.35 m high in profile and has a typical grade of -13% to -14.3%. The ore produced in the mine, and some of the development waste, is hauled to the surface in diesel-powered trucks via the ramp. In addition, the CRF and a portion of the URF used to backfill the stopes are hauled underground via the ramp.

16.5.2 Compressed Air

A compressor plant situated on the surface at the mine site supplies the mine's compressed air. The compressor plant has three Ingersoll Rand compressors, which provide a total capacity of 150 L/s (318 cfm) at 120 psi. Usually, two compressors operate at any given time with the third unit on standby.

16.5.3 Data and Communications

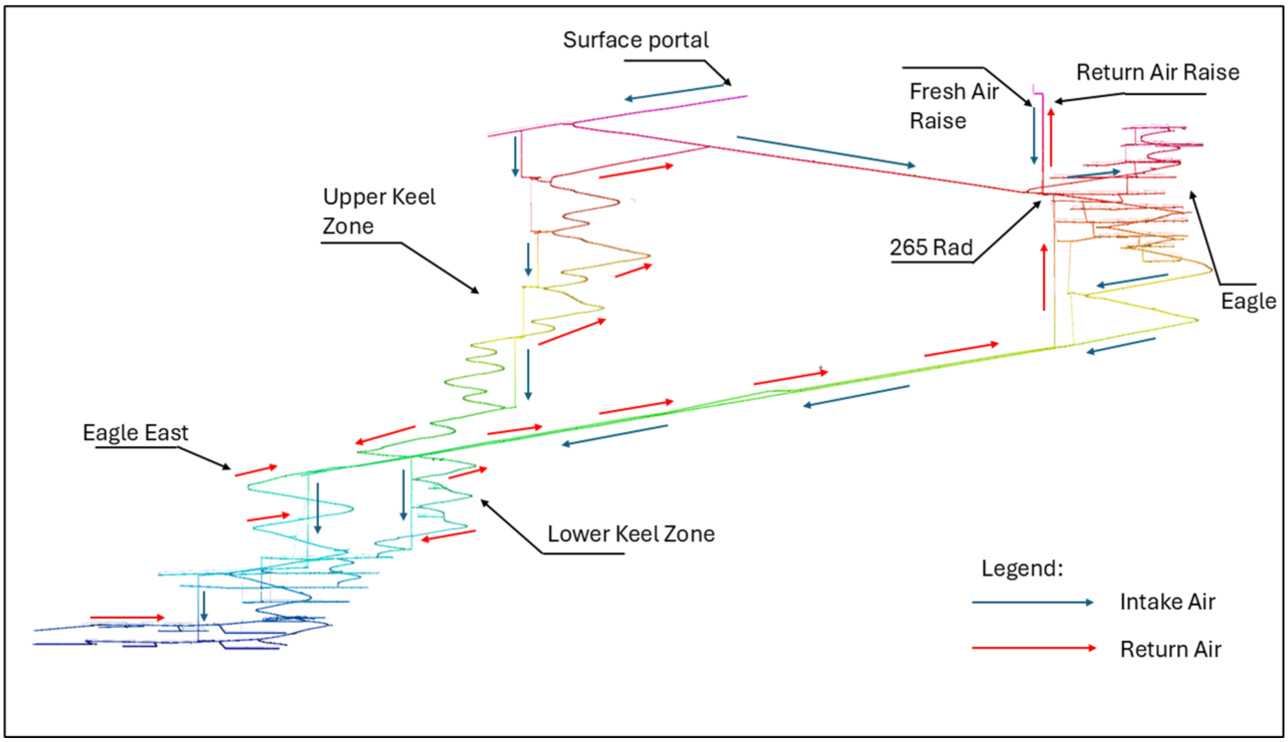
The underground mine data and communications systems consist of a leaky feeder system for two-way radio communication and a fiber-optic network. All underground equipment is equipped with radios, and hand-held units are also available. The fiber-optic network supports the control and monitoring system, such as mine geotechnical monitoring, primary ventilation, and dewatering monitoring. In 2023, Eagle Mine installed a private LTE network which utilizes the system for asset tracking, communications, and tele-remote operations.

16.5.4 Maintenance Shop

Mining equipment is mainly serviced and repaired at the maintenance shop on the surface. There is, however, an underground maintenance shop in the East Eagle. It is mainly used for servicing and repairing equipment that cannot easily be moved to the surface, such as jumbos, bolters, and longhole drills.

16.5.5 Ventilation

Figure 16.12 illustrates the ventilation system. Fresh air enters the mine via the portal of the main ramp and a fresh-air raise (FAR), consisting of a vertical, 4.5 m diameter borehole. The FAR is equipped with an Alimak elevator, which provides a secondary means of emergency egress from the mine. The return air is exhausted via a return-air raise (RAR), consisting of a second vertical, 4.5 m diameter borehole.



Source: Eagle Mine, 2026

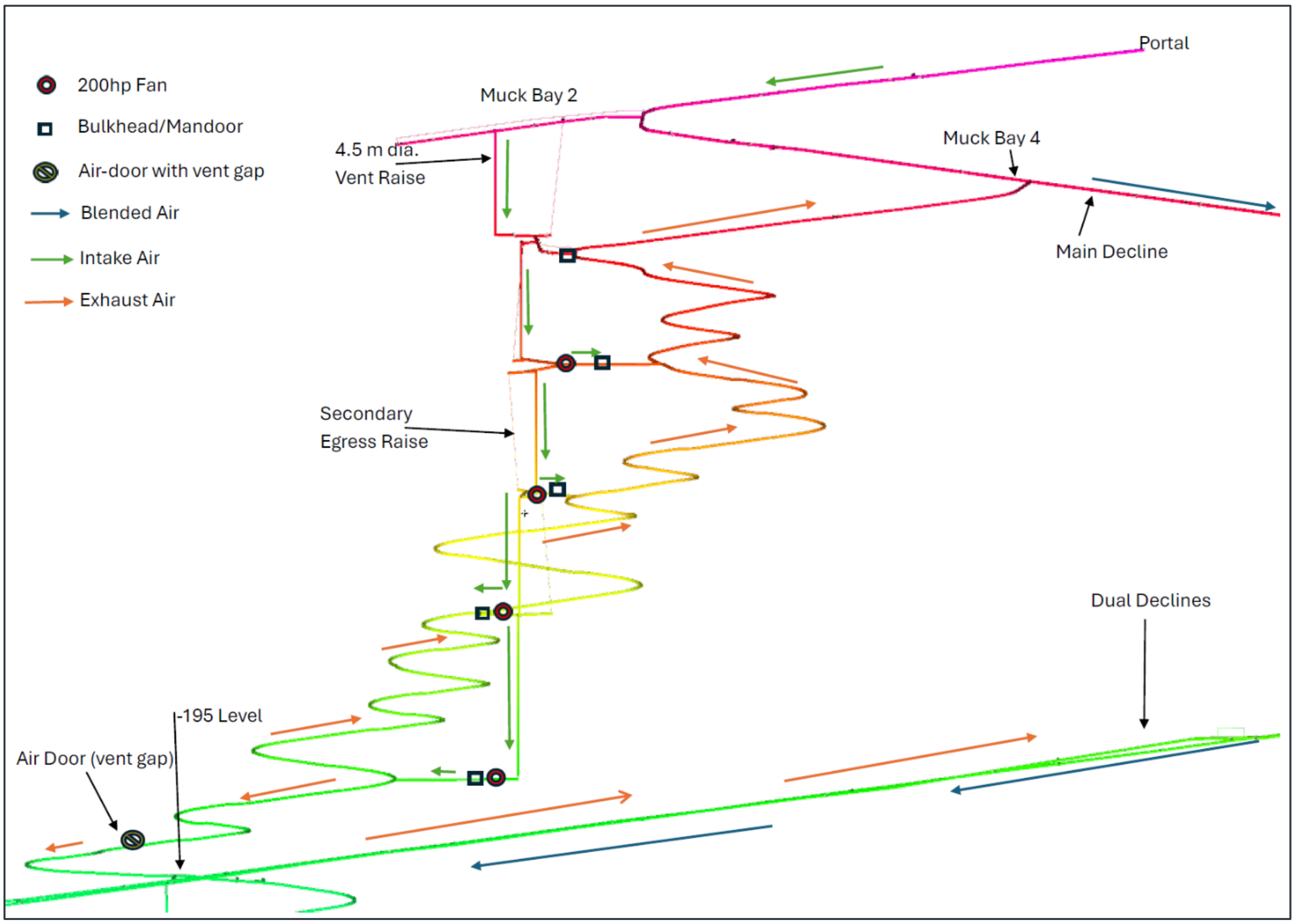
Figure 16.12: Eagle Mine Ventilation System, Isometric View

The return air is exhausted via the RAR by twin 522 kW fans installed at the collar of the raise. The portal is equipped with a 186-kW fan. The portal and the FAR are equipped with propane heaters, which maintain the air entering the mine above freezing temperature during the winter.

Fans in the main ramp direct fresh air to the lower levels of the mine. Return air is exhausted via 4 m by 4 m raises that connect the sublevels. The airflow is controlled with bulkheads installed at the exhaust-raise crosscuts. Auxiliary fans supply air to the crosscuts and development headings. Fresh air is provided to headings requiring auxiliary ventilation through 1.2 m diameter ducting, which is either flexible textile ducting or semi-rigid polymer ducting.

The ventilation system has been extended via twin ramps from the Eagle to the Eagle East. One of the ramps serves as the principal access to the zone and exhausts return air. The adjacent ramp provides intake ventilation and provides a secondary means of egress from the zone.

Figure 16.13 illustrates the ventilation system planned for the Keel and shows how it would fit in with the mine-wide ventilation system. Fresh air will be drawn to the upper level of the Keel via a series of 4.5 m ventilation raises starting at Muck Bay 2 (395 masl) and connecting the Keel sublevels. The air will be drawn by multiple 200 Hp ventilation fans built in bulkheads on each raise sublevel. The return air will flow from the lowermost raise back up through the Keel ramp, and into the main ramp at Muck Bay #4 (350 masl). The design avoids developing a ventilation raise connection to the surface and the permitting the raise would require.

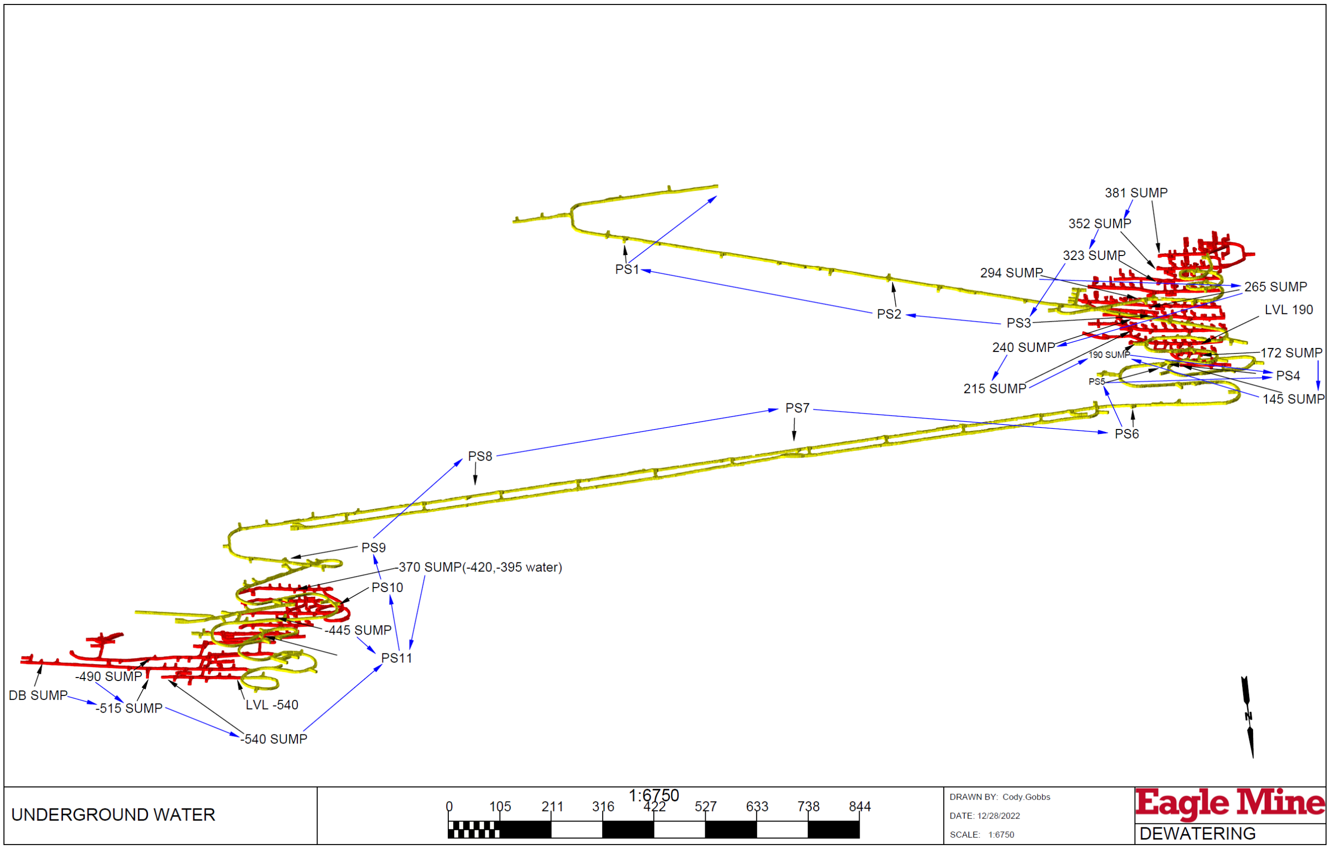


Source: Eagle Mine, 2026

Figure 16.13: Keel LOM Ventilation

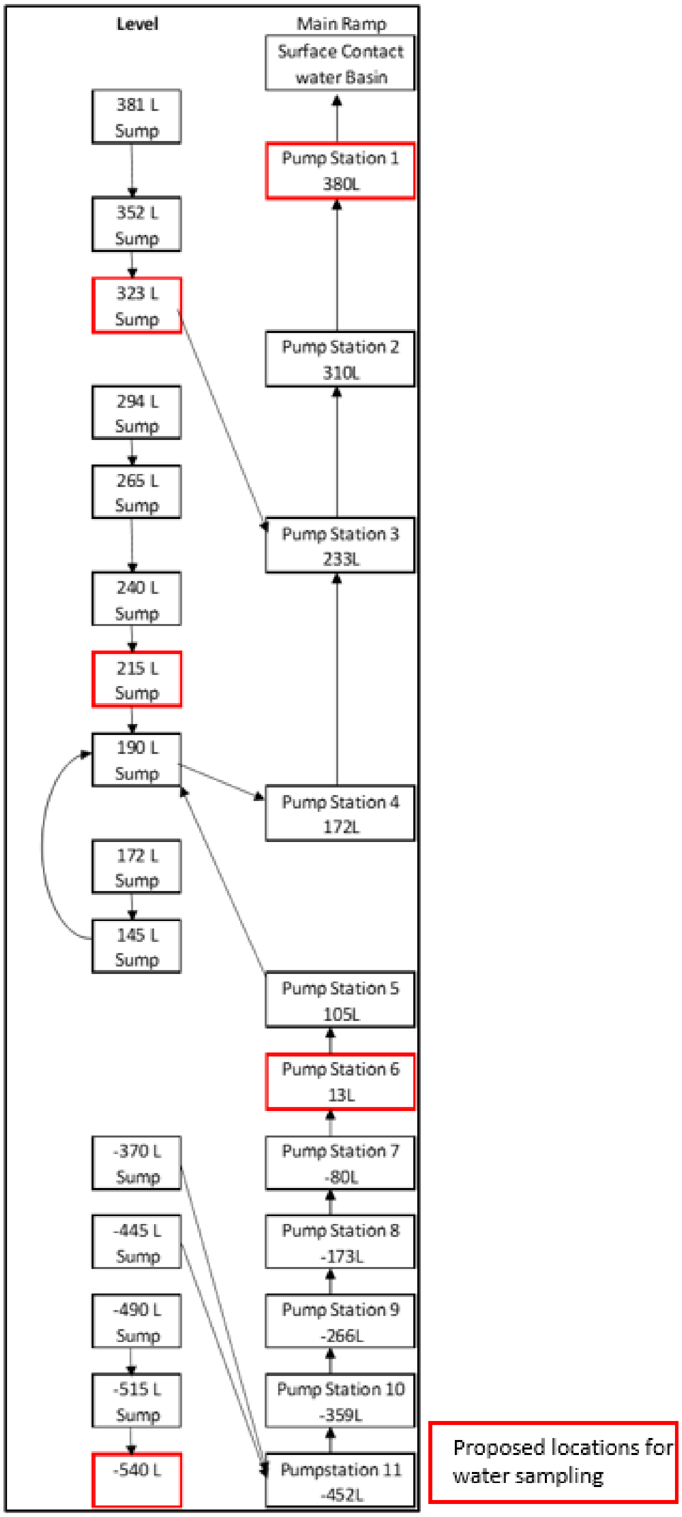
16.5.6 Dewatering System

Figures 16.14 and Figure 16.15 illustrate the dewatering system in an isometric view and schematic, respectively. The Eagle Mine is relatively dry, with low groundwater inflows compared to most mines. Consequently, a significant portion of the water that the dewatering system handles originates from mining operations such as drilling and dust control from washing down muck piles.



Source: Lundin Mining Corporation, 2022

Figure 16.14: Eagle Mine Dewatering System – 3D View



Source: Lundin Mining Corporation, 2022

Figure 16.15: Eagle Mine Dewatering System - Schematic

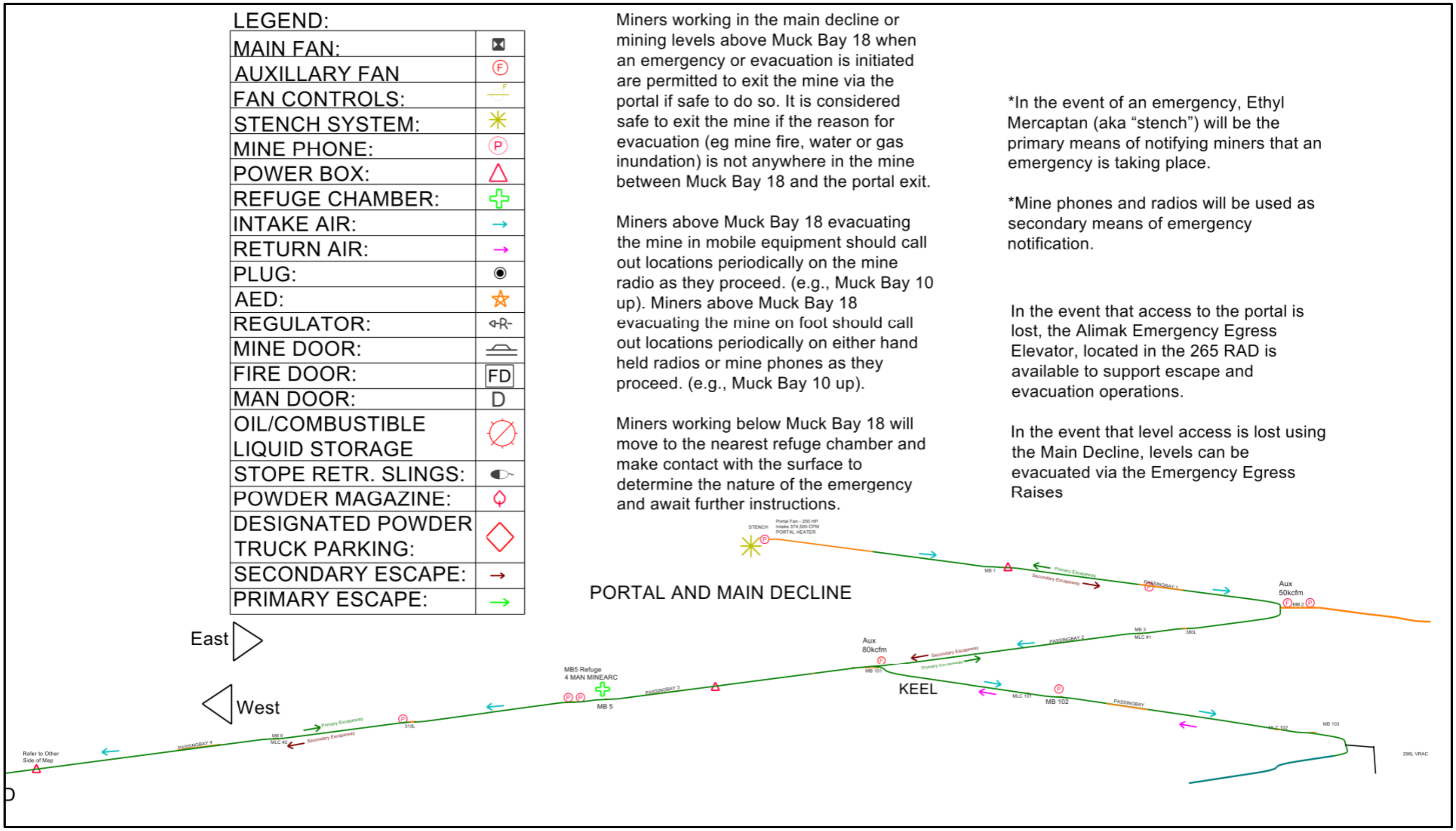
The dewatering system consists of pumping stations connected in series along the main decline. The water is pumped upwards from station to station and finally to the Surface Control Water Basin. The stations are spaced along the ramp at vertical intervals ranging from 70 m to 93 m. A main settling sump on the 190 level receives water pumped from the Eagle East.

16.5.7 Escapeways

Figure 16.16 through Figure 16.19 illustrate the mine's escapeways starting at the portal and progressing downward. The routes available for exiting in an emergency include portions of the main ramp, 1.2 m diameter borehole raises equipped with Laddertube manways, and a 4.5 m diameter borehole raise extending from surface equipped with an Alimak elevator. The Alimak elevator has a 2,000-kg capacity and can transport up to 20 individuals.

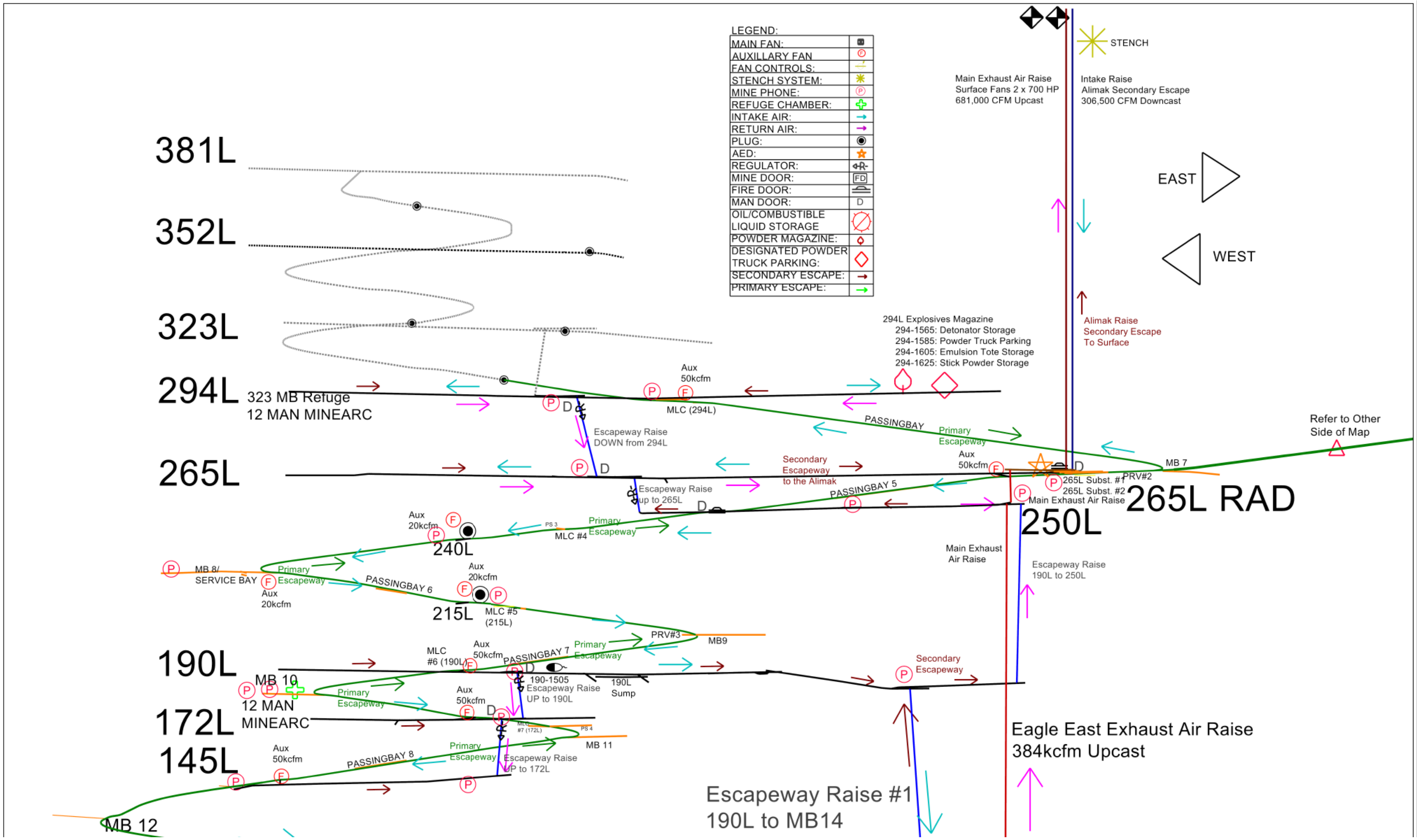
Portable mine refuge chambers supplied by MineARC are set up at strategic locations in the mine. They are equipped to provide breathable air supply to occupants in the event of an underground emergency. The mine has eight portable mine refuge chambers with a 12-person capacity and four units with a four-person capacity.

Reclamation activities are underway for the uppermost levels of the Eagle deposit, including 323L, 352L, and 381L, which are fully depleted. Figure 16.17 shows Eagle post-reclamation.



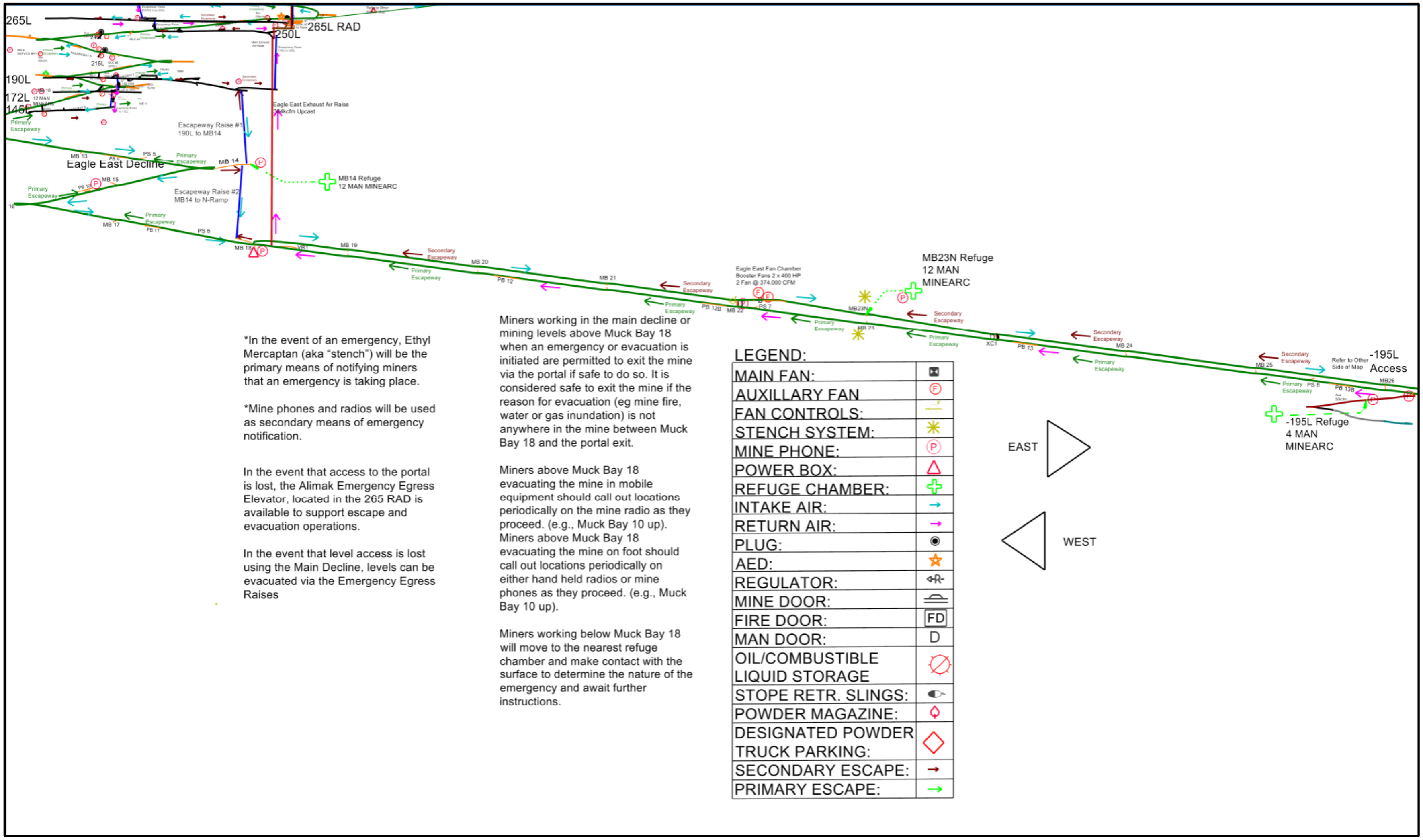
Source: Eagle Mine, 2026

Figure 16.16: Eagle Mine Escapeways – Portal and Upper Keel Access



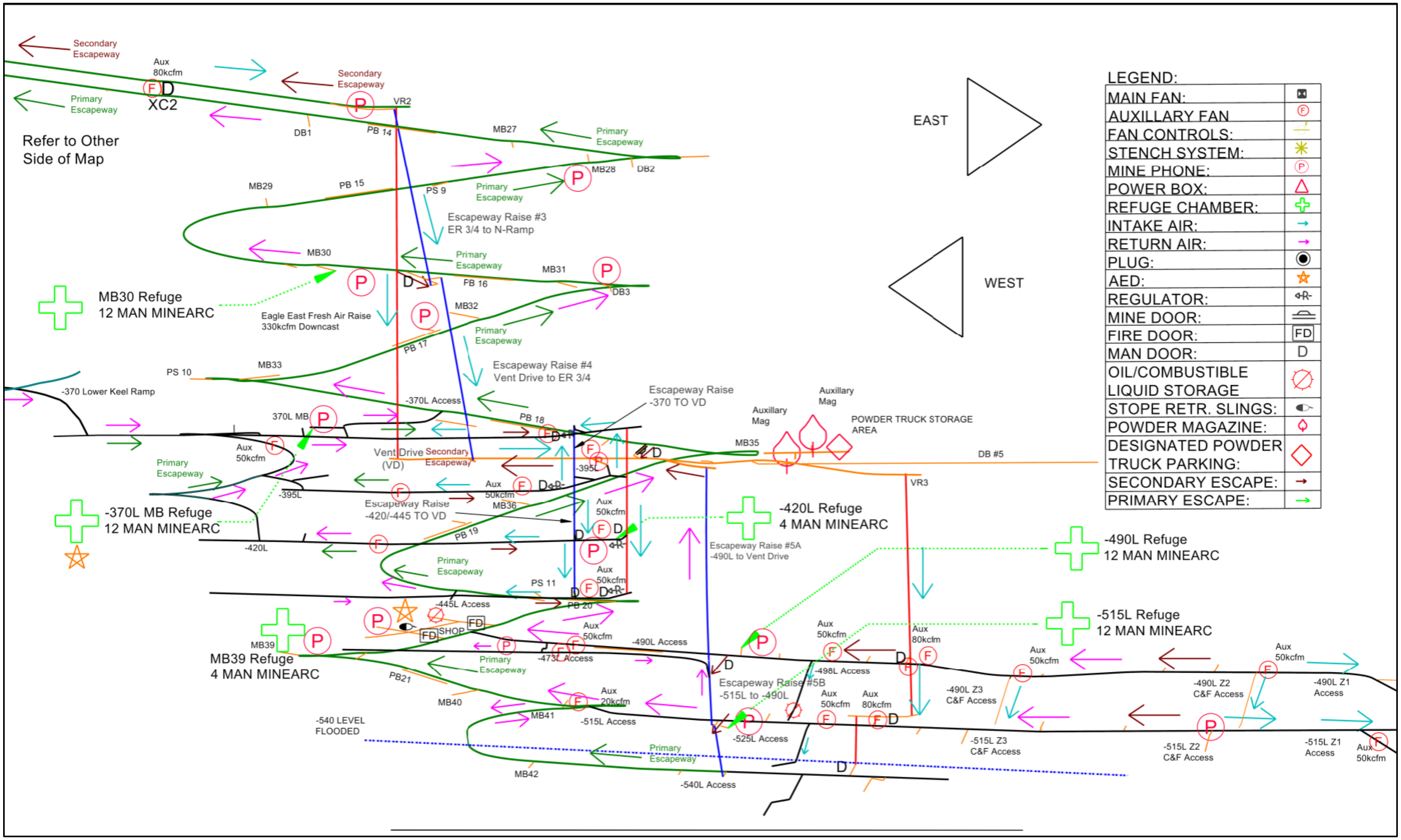
Source: Eagle Mine, 2026

Figure 16.17: Eagle Mine Escapeways – Eagle Zone



Source: Eagle Mine, 2026

Figure 16.18: Eagle Mine Escapeways – Eagle East Decline to -195L Keel Access



Source: Eagle Mine, 2026

Figure 16.19: Eagle Mine Escapeways – Eagle East Zone

The Keel will have two escape routes where it connects with the mine's main ramp at Muck Bay 4 (approx. 352 masl) and -195 masl. In addition, 1.2 m diameter borehole raises equipped with Laddertube manways will connect the sublevels along with additional 8-person refuge chambers.

The Eagle Mine has a warning system using ethyl mercaptan gas in case of an emergency requiring personnel to evacuate the mine or report to a refuge station. Release points for Ethyl Mercaptan gas are located at the ramp portal, the bottom of the Alimak raise, and in the Eagle East fan chamber.

Personnel entering the underground mine wear belt-mounted, self-contained self-rescuers (CSE Model SRLD), which provide the user with one hour of chemically generated oxygen. The Eagle Mine has a mine rescue station on the surface equipped with 20 Draeger BG-type closed-circuit breathing apparatus.

16.5.8 Underground Electrical System

Underground electrical power is fed by two separate 13.8 kV distribution systems, one from the portal and the second down the fresh-air raise (FAR). Both systems are fed from the site powerhouse.

The portal switchgear feed supplies power down the decline to Switchgear B. Transformers along the main decline provide 480 V power for the pump stations and a transformer located at the portal for the portal fan and heater. From the main Switchgear B at the 265 level, the power is fed down the main decline to provide electricity for pumps, ventilation fans, and mining equipment.

A 13.8 kV substation is installed at the ventilation raise collar to provide power to the main ventilation fans, heating units, Alimak elevator, and general surface facilities. The ventilation raise power supply is fed from the Vent Raise substation down the FAR to Switchgear A located at the 265 level. From the main Switchgear A, the power is fed up the main decline to the upper portion of the mine (294 to 381 levels) to provide power for pumps, ventilation fans, and mining equipment.

Each production level has a 750 kVA Mine Load Center (MLC) to feed ventilation and electro-hydraulic loads. Levels are equipped with breakers that allow for isolation from the main system. The underground feeds from the surface to the main underground substations on both systems are sized for full mine loads for redundancy in case of failure of the other system. A tie-in breaker is installed between the two substations on the 265 level.

16.5.9 Explosives Magazines

The explosives magazines are located in the underground mine. They are licensed to and managed by Eagle Mine. The magazine has a capacity to store 11.8t emulsion and 5.4t stick powder, sufficient to support 17 rounds and one stope, which is equivalent to five days of sill advance production and 10-days of stope production. Eagle Mine uses an emulsion blasting agent for both production stopes and development headings. In 2025, Eagle consumed 697t of emulsion and 301t of powder products as well as 65,335 Nonel Detonators, 6,368 electronic detonators, 72,510 boosters, and 40.9km of detonating cord.

16.6 Mining Methods

The configuration of the deposit is suitable for sublevel-type mining methods. Eagle Mines uses two mining methods: Drift-and-fill (D&F) and Sublevel Open Stoping.

For the Sublevel Open Stoping, both methods, longitudinal (LSLOS) and transversal (TSLOS), can be applied, depending on the characteristics of the deposit.

With longitudinal (LSLOS), the intrusion is excavated parallel to the strike of the deposit in contrast, with transverse (TSLOS), it is mined perpendicular to the strike, between the footwall and hanging wall.

Table 16.16: Summarizes the Mining Methods Used in the Eagle Three Mining Zones

Zone	Drift and Fill	Longitudinal (LSLOS)	Transverse (TSLOS)
Eagle			✓
Eagle East	✓	✓	✓
Keel		✓	✓

16.6.1 Drift and Fill (D&F) Mining

Drift and Fill (D&F) is one of the mining methods used only at Eagle East. Only two zones remain in Eagle East where drift mining methods will be utilized, as presented in Figure 16.20.

D&F is similar to the overhand cut-and-fill method. Both methods mine the deposit in successive lifts from bottom to top and access the lifts via attack ramps of variable inclination. The methods differ in the approach used to mine the ore in each lift. Overhand cut-and-fill excavates the complete width of the lift from footwall to hangingwall, whereas D&F mines it by advancing through the ore one drift width (~5 m) at a time. Consequently, with D&F, the size of the opening is limited to the width of a drift rather than the span from footwall to hangingwall.

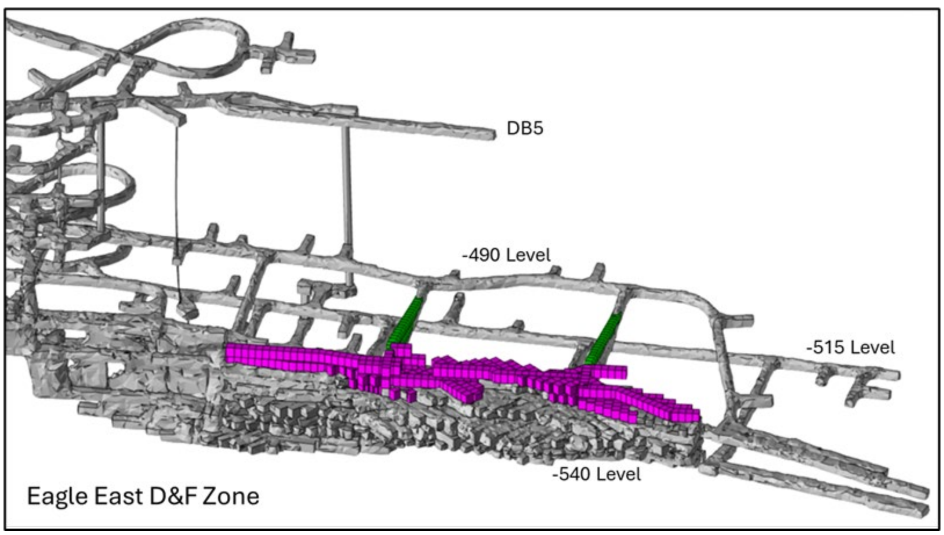


Figure 16.20: Drift and Fill Method at the Eagle Mine

Within the orebody, the lift is mined by driving drifts with a 5.0 m wide by 6.0 m high profile. First, a level access drift is advanced from the end of the attack ramp to the hangingwall to establish approximate ore boundaries. Next, main level drifts are driven left and right along from the level access along the strike of the deposit until they encounter waste or an adjacent D&F zone. Then, shorter drifts referred to as herringbones are driven from the main level drifts at about a 45˚ angle to them and advanced until they encounter waste at the footwall or hangingwall contact.

Once a drift has advanced to the contact, it is backfilled with cemented rockfill, and a new drift can be driven adjacent to it. The new drift will have a wall of CRF from the previous drift on one side and a wall of ore on the other. The herringbone drifts are mined one after the other, starting from the ends of the stope and retreating back towards the level access. Figure 16.21 illustrates a typical D&F stope in plan view.

Mine trucks haul the backfill underground from the CRF plant and dump it as close as possible to the point in the drift where the material is to be placed. An LHD equipped with a jammer attachment pushes the CRF into place by ramping it upwards and packing it as tightly as possible to the back of the drift, leaving a void of no more than 15 cm.

The level access and main level drifts are jam-filled incrementally as adjacent herringbone drifts are filled. Jam toes are cut with an LHD before fully curing to prevent having to blast out any backfill material to access the next herringbone drift. Jam-fill is allowed to cure for a minimum of 18 hours before resuming mining activity in the next adjacent herringbone drift. Once the lift has been mined and backfilled, the attack ramp is backslashed to access the next higher-up lift.

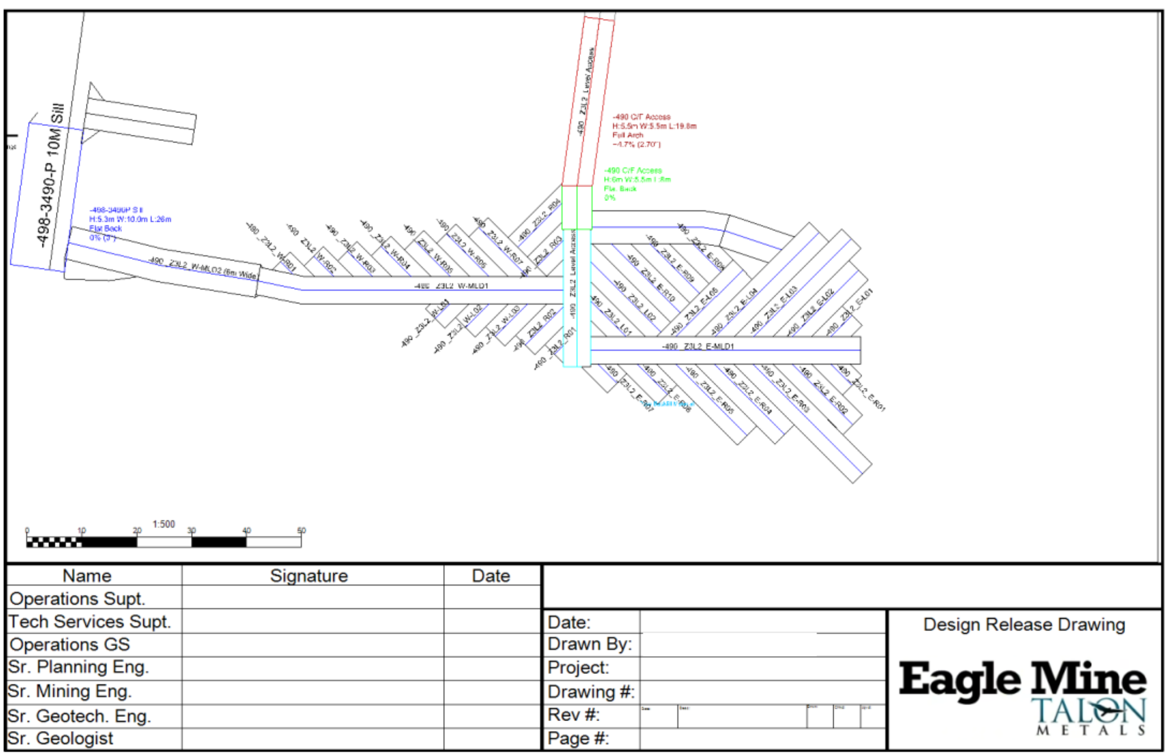


Figure 16.21: Typical Drift and Fill Stope – Plan View

16.6.2 Longitudinal Sublevel Open Stoping (LSLOS)

Longitudinal stopes are currently only utilized in Eagle East and are planned to be used in Upper keel as presented in Figure 16.22 and Figure 16.23

Longitudinal stopes are typically 6 m wide and 25 to 30 m in height. The stopes are mined along strike in panels up to 50 m in length. Longitudinal sills are designed and mined at widths of 6 m but can be widened to 10 m in some areas, depending on the width of the orebody.. Primaries have also been narrowed down to a minimum width of 4.5 m to minimize dilution when in waste.

After drilling, blasting, and mucking, longitudinal stopes are backfilled with uncemented rock fill. For stopes with adjacent panels, CRF is dumped into the stope until the material at the angle of repose reaches the upper sublevel. Uncemented rockfill is then dumped in the remaining void, with the CRF acting as a dam to contain the uncemented fill when the subsequent panel is mined.

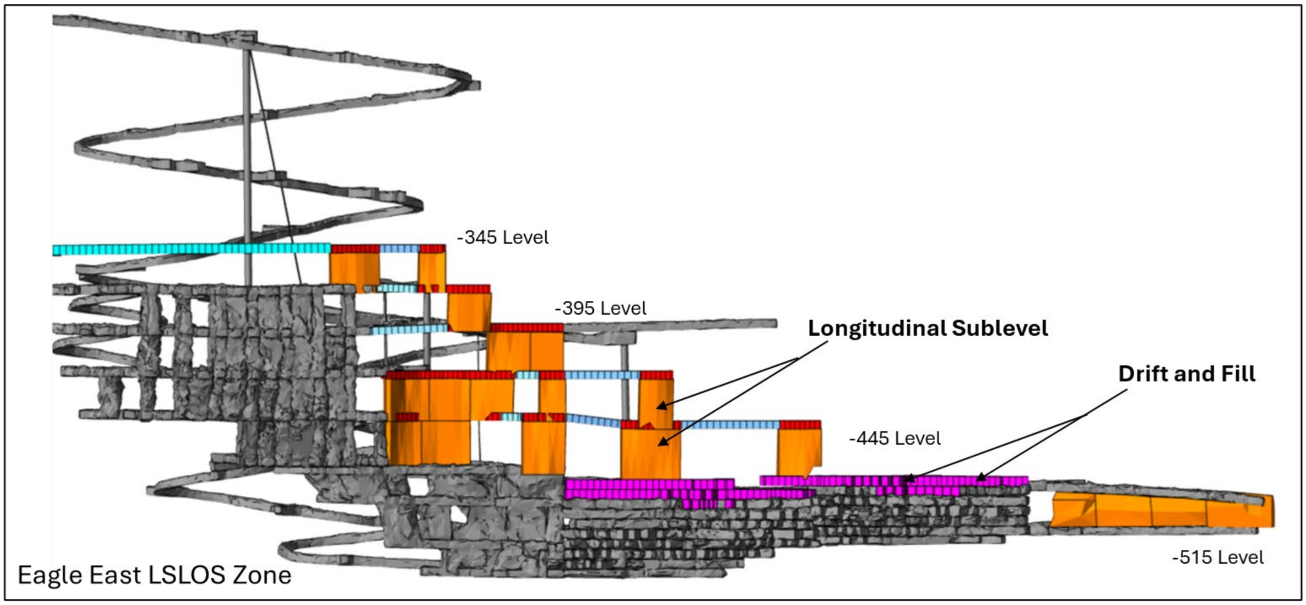


Figure 16.22: Eagle East LSLOS Stopes

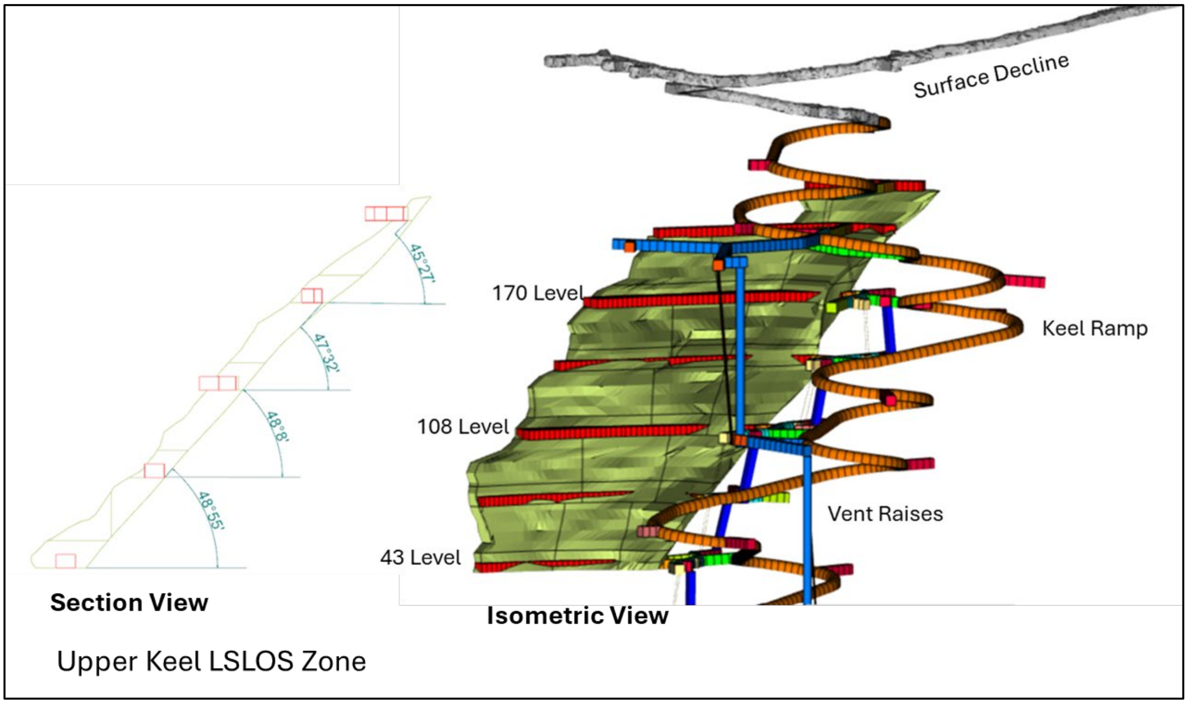


Figure 16.23: Upper Keel LSLOS Stopes

16.6.3 Transverse Sublevel Open Stoping (TSLOS)

Figure 16.24 and Figure 16.25 illustrate the application of the TSLOS mining method at Eagle mine. The portion of the deposit between two sublevels is mined by dividing the ore into alternating primary and secondary stopes, extending in parallel from the footwall to the hangingwall.

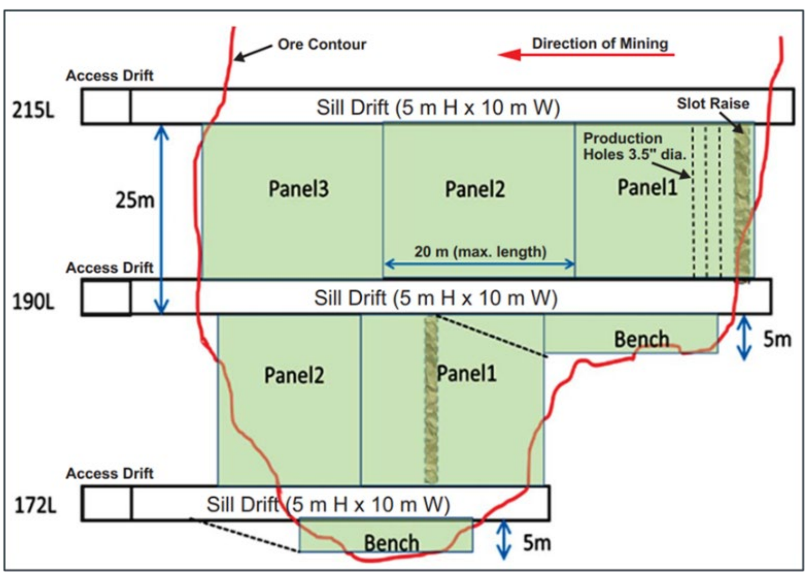


Figure 16.24: Transverse Sublevel Open Stoping Method at the Eagle Mine – Cross-Section

The stopes are accessed by driving crosscuts to the orebody from footwall drives on the upper and lower sublevels. The crosscuts are typically driven at 7m wide on top and bottom.

The dimensions of the sublevel open stopes are presented in Table 16.12 in the Mine design section. In wider parts of the deposits, the stopes are subdivided into sub-panels, thereby limiting the length of the opening to a maximum of 20m for primary and 35m for secondary stopes. Multiple panels are mined one after the other in a retreating fashion from the hangingwall to the footwall.

The primary stopes are mined first, leaving ore pillars of varying dimensions between primary stopes that will subsequently be mined as secondary stopes. The mined-out panels of primary stopes are backfilled with cemented rockfill, forming engineered pillars on either side of each secondary stope. The mined-out secondary stopes are backfilled with uncemented rockfill. Backfill is placed by backing up mine trucks equipped with ejector boxes at the upper sublevel and dumping the material into the opening. The primary sills are jammed with CRF before beginning adjacent secondary sills.

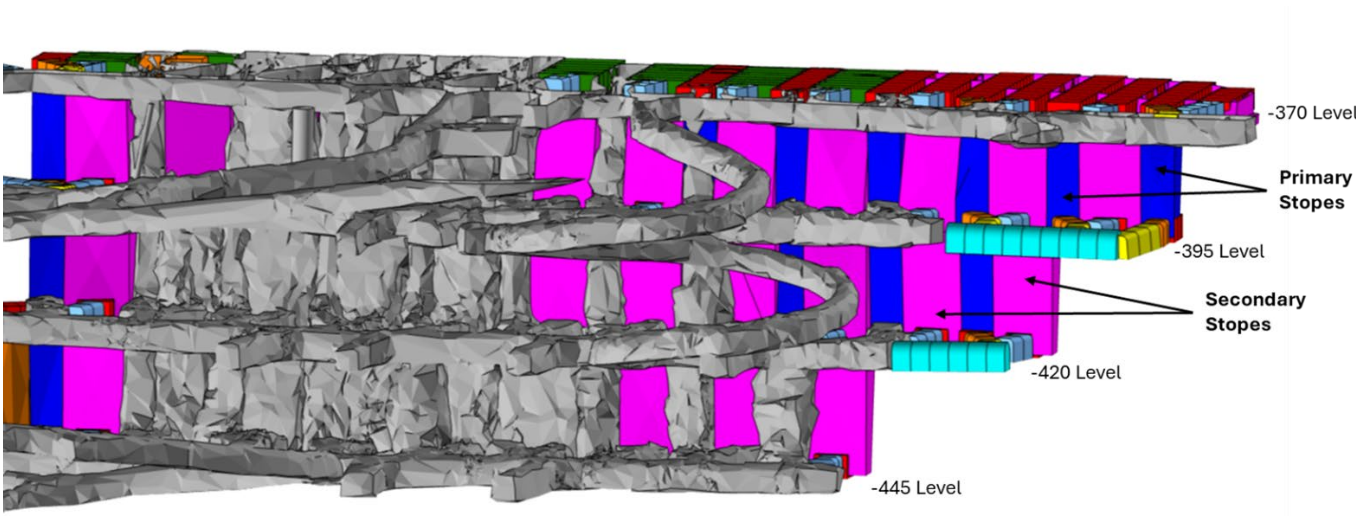


Figure 16.25: Transverse Sublevel Open Stoping Method at the Eagle Mine – Longitudinal Section

The primary and secondary stopes are mined by drilling and blasting longholes. Figure 16.26 shows a typical drilling layout. The longholes are 88 mm in diameter and are drilled as downholes from the upper sublevel with an ITH production drill rig. Primary stopes are drilled off with rows of vertical longholes. Secondary stopes, on the other hand, are drilled off with inverted fans due to the limited width of the top-sublevel drift. Each panel is blasted in two steps using emulsion explosives and millisecond detonators. First, a drop raise is advanced to provide a slot, and then the remainder of the panel is blasted, usually in a single shot.

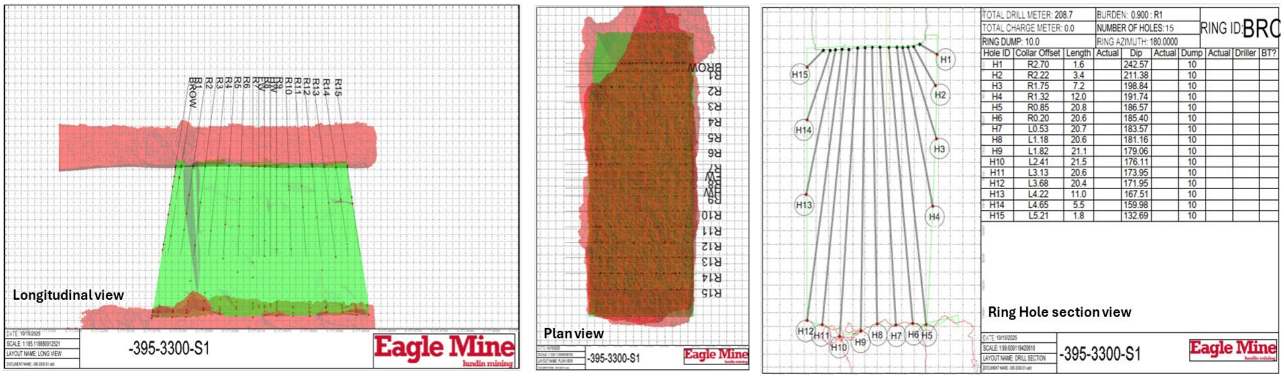


Figure 16.26: Typical Longhole Drilling Layout

An LHD mucks the broken ore from the access crosscut on the lower sublevel. A portion of the broken ore can be mucked with the operator on the machine; however, the majority of blasted ore must be mucked by teleremote control when the LHD operates inside the stope opening. The broken ore is hauled out of the stope and is either stockpiled in a muck bay or loaded directly into mine trucks.

16.6.4 Stope Sequencing

In general, transverse stopes are mined using an inverted V sequence. The mineralized zone is divided in primary and secondary stopes. Primary stopes are extracted from the bottom up and slowly extend outward, creating a pyramidal shape (Figure 16.27). Secondary stopes follow the sequence and are extracted once the two closest primary stopes on the same horizon have been filled (CRF) and cured.

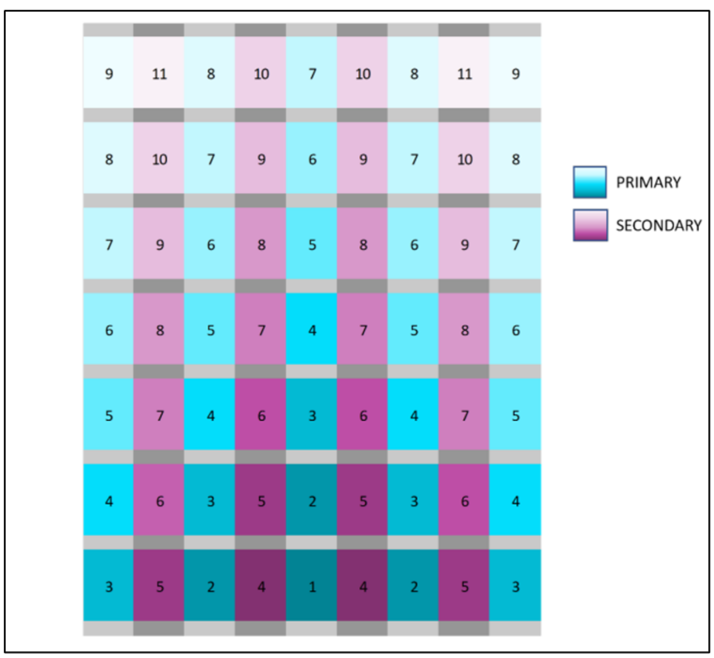


Figure 16.27: General Progression of Open Stope Mining According to Pyramidal Shape

The mining sequence is also dependent on backfill placement, as blasting in proximity to CRF, which is not fully cured, can negatively impact the ultimate strength of the fill. Eagle has developed required cure times based on site-specific data for typical cement content and blasting charge weights. Figure 16.28 shows the cure time delay visualizer for backfill containing 5% cement for a production blast in a stope (left), and a smaller slot blast (right).

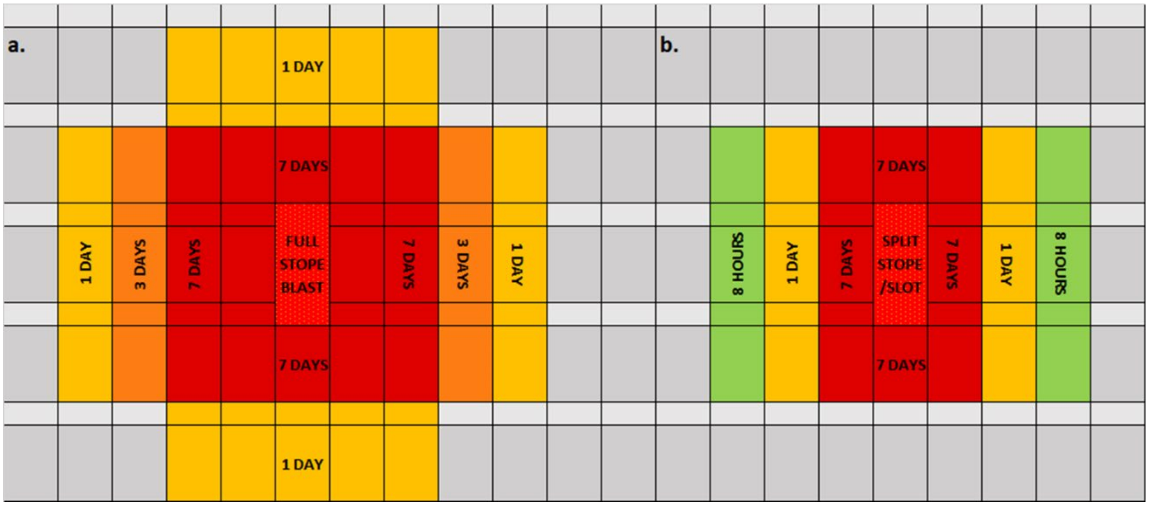


Figure 16.28: CRF Cure Time Delays for (a) Full Stope blast and (b) Slot blast

16.6.5 Mining Equipment

Table 16.17 lists the mobile equipment operating in the underground mine. The Eagle Mine is a mechanized mine employing rubber-tired diesel equipment for all phases of mining operations. CAT R1700 and R2900 LHDs are equipped for radio remote control operation, which is required when the units muck in TSLOS stopes. Seven of the 13 CAT AD45 mine trucks are equipped with ejector boxes, and the remaining 6 are equipped with end dump boxes. This allows for increased payload capacities when hauling ore to the surface while also bringing fill down to help with the long haulage cycle times to Eagle East.

For rock support, the mine has a cable bolter and rock bolting rigs, which install mesh, swellex bolts, and resin rebar bolts. All of the rock bolting rigs have been converted to install both resin-grouted rebar bolts using resin shooters and inflatable Swellex bolts.

Light-duty vehicles, including pickup trucks and vans, are used to transport miners underground.

The QP reviewed the underground equipment fleet and observed many of the machines in operation. The QP is of the opinion that the number of equipment units in the fleet and the types, makes, and models are appropriate for the mining methods and development requirements at the Eagle Mine.

Table 16.17: Underground Mobile Equipment

Fleet	Make	Model	Operating Units
Mucking and Haulage			**19**
UG LHD	Caterpillar	R1700G	3
UG LHD	Caterpillar	R2900G	3
UG Trucks	Caterpillar	AD45B	13
Drilling and Blasting			**11**
LH Production Drills	Epiroc	Simba M7C	1
LH Production Drills	Epiroc	Simba E7C	1
LH Drills	Epiroc	Cabletech LC	2
Jumbo Drills	Sandvik	DD420-40C	2
Jumbo Drills	Sandvik	DD420-60C	2
Explosives charger	Getman	A64 2-500S	1
Explosives charger	Getman	A64 Ex-C 2-500	2
Ground Support			**9**
Jumbo-Bolter	Sandvik	DD411-C	3
Jumbo-Bolter	Sandvik	DS311DE	1
Jumbo-Bolter	Sandvik	DS410-C	2
Trans Mixer	Normet	Utimec LF500	2
Shotcrete Sprayer	Normet	Spraymec 1050 WP	1
Utility vehicles			**5**
Fan Hanger	Getman	A64	1
Pallet Handler	Getman	A64	2
Scissor Truck	Getman	A64	1
Lube Truck	Getman	A64	1

16.6.6 Mine Development

Table 16.18 presents the LOM development plan. Figure 16.29 to Figure 16.31 show the LOM development as bar charts for lateral and vertical development.

The life of mine development plan comprises a total of 15,541 meters of lateral development and 2,297 vertical meters of development. Keel accounts for a total of 69.8% of total development, followed by Eagle East (29.7%) and Eagle (0.4%).

Capital development is primarily scheduled between 2026 and 2028, with the majority allocated to the Keel to support the timely establishment of production access. This includes development required to access planned production levels and establish primary infrastructure. Development at Eagle East is required to access the remaining transverse and longitudinal stopes, while development in the Eagle is limited to access for the final two stopes.

The Keel development strategy focuses on accelerating access to production horizons through concurrent ramp and infrastructure development. The Lower Keel ramp development has been advanced from both upper and lower access points to approximately 80% completion, concurrently with vent raise development. The ramp will continue to be mined as priority until breakthrough, with footwall level development providing an additional mining face to maintain progress during intermittent infrastructure construction delays. This approach supports the timely initiation of production. Upon completion of the Lower Keel ramp, development will transition to level accesses and footwall development within Lower Keel, while advancing Upper Keel ramp and level development to support production beyond 2028. A similar approach will be applied to the Upper and Middle Keel , with ramp advancement prioritized while concurrently establishing sublevel access.

The Keel will require the following development:

- Ramp: A ramp will be developed on the Northeast side of the deposit rather than in the footwall. It will extend from the Eagle main ramp to the West Extension of the Eagle East. The ramp will be developed with a switchback configuration, minimizing development meters to gain access to the sublevels.
- Sublevels: Twenty sublevels will be developed at 28 m sublevel intervals. Each sublevel will consist of a drift providing access to the attack ramp for sub-level stope access.
- Ventilation Raises: The development plan has 6 ventilation raises consisting of 4.5m diameter boreholes. Two of the raises will be developed in 2026, with subsequent raises being developed as areas are opened up in Upper to Middle Keel.
- Escape Raises: Four escapeway raises will be required, each consisting of a 1.2m diameter borehole equipped with a laddertube manway. These raises will be developed in parallel to the ventilation raises, with the uppermost one connecting to the ventilation drift and the lower three connecting to other sublevels.
- Ventilation drifts: Access drifts connect the Keel Ramp to the ventilation and escape raises. In Upper and Middle Keel, access drifts and associated raises are located at approximately 90m vertical spacing, with each serving 3 to 4 sublevels, which can be brought into production upon raise completion. In Lower Keel, shorter ventilation drifts will break into the vent raise from the ramp to supply the required air to complete the development and future stope mining.

Table 16.18: LOM Mine Development Plan

Zone	Development type	2026	2027	2028	2029	2030	Total
Eagle	Lateral Capex meters	-	-	-	-	20	**20**
	Lateral Opex meters	-	-	-	-	44	**44**
	Vertical meters	-	-	-	-	-	**-**
Eagle East	Lateral Capex meters	484	487	219	78	14	**1 282**
	Lateral Opex meters	1 667	1 386	158	131	-	**3 341**
	Vertical meters	-	-	-	-	-	**-**
Keel	Lateral Capex meters	2 071	2 754	2 828	40	32	**7 724**
	Lateral Opex meters	421	847	1 139	400	322	**3 130**
	Vertical meters	349	832	1 027	89	-	**2 297**
Total	**Lateral Capex meters**	**2 555**	**3 241**	**3 047**	**118**	**66**	**9 026**
	Lateral Opex meters	**2 088**	**2 233**	**1 297**	**531**	**366**	**6 515**
	Vertical meters	**349**	**832**	**1 027**	**89**	**-**	**2 297**

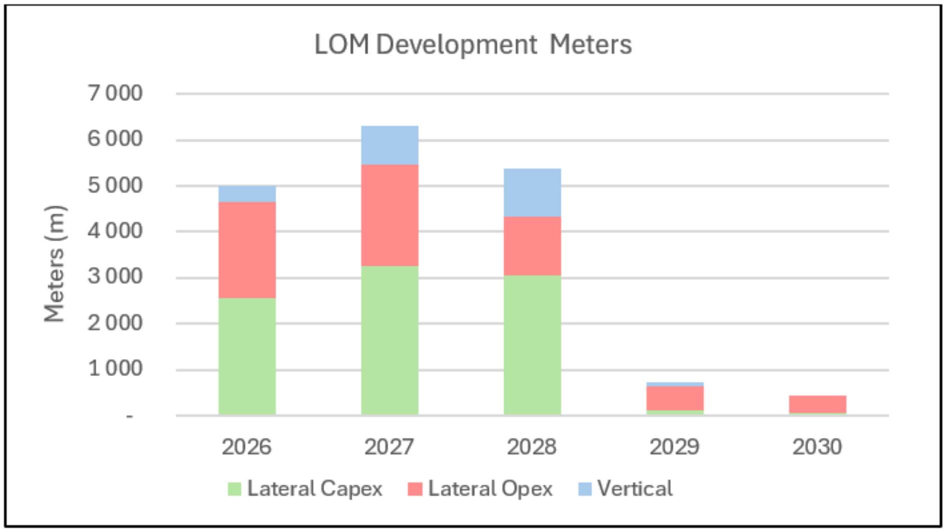


Figure 16.29: The LOM Development Meters by Category

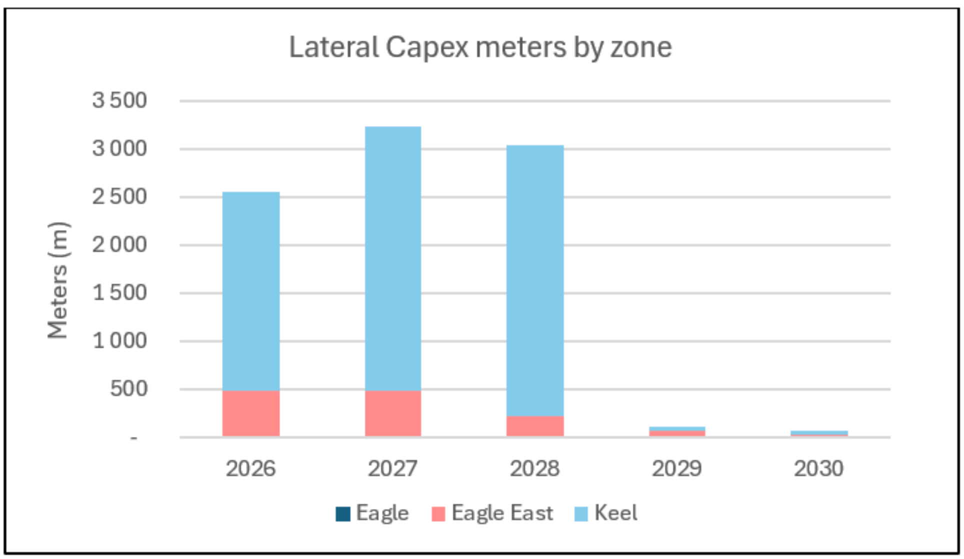


Figure 16.30: Lateral Capex LOM Meters by Zone

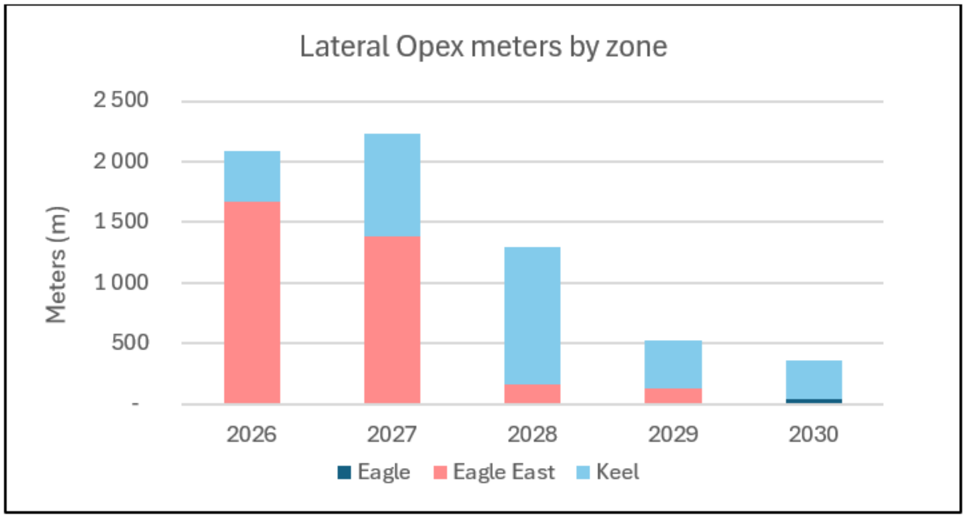


Figure 16.31: Lateral Opex LOM Meters by Zone

16.6.7 LOM Production Schedule

2026 represents the final year in which Eagle Mine is planned to operate at a production rate of 2,000 tonnes per day. Beginning in early 2027, the mine plan increases to 2,200 tonnes per day. As the Eagle East is depleted, production transitions to the Keel, which is expected to contribute more than 80% of total ore tonnage by 2028.

This increase in mining rate is intended to offset declining grades and sustain overall metal production. Table 16.19 presents the LOM production schedule and Figure 16.32 illustrates the production plan in orthographic view, outlining this strategy. Based on current Mineral Reserves estimates, mining operations are projected to continue through the second half of 2030 at the 2,200 tonnes per day rate.

The timing of the production increase is supported by improved cycle times associated with the Keel, the use of inter-level ore passes within the Keel, as well as the implementation of paste backfill. Together, these operational enhancements are expected to enable a consistent 2,200 tonnes per day production rate.

The Eagle has been fully depleted except for 45,000 tonnes of ore which is within close proximity to the Alimak egress raise. These stopes have been scheduled as the last two stopes in the mine plan so that if there are any issues during blasting these stopes it does not compromise any other tonnes that remain within all mining zones.

Table 16.19: LOM Production Schedule

		2026	2027	2028	2029	2030	Total
Eagle	Tonnes	-	-	-	-	40 532	**40 532**
	Ni%	-	-	-	-	1.12	**1.12**
	Cu%	-	-	-	-	1.27	**1.27**
Eagle East	Tonnes	509 487	329 675	136 394	179 759	-	**1 155 315**
	Ni%	1.60	1.12	1.06	1.02	-	**1.31**
	Cu%	1.33	0.94	0.92	0.85	-	**1.09**
Keel	Tonnes	118 982	457 720	650 204	607 520	456 207	**2 290 633**
	Ni%	0.86	0.85	1.00	0.96	0.94	**0.94**
	Cu%	0.65	0.64	0.70	0.69	0.67	**0.68**
Total	**Tonnes**	**628 469**	**787 396**	**786 598**	**787 279**	**496 739**	**3 486 481**
	Ni%	**1.46**	**0.97**	**1.01**	**0.97**	**0.95**	**1.06**
	Cu%	**1.20**	**0.76**	**0.74**	**0.73**	**0.72**	**0.82**
Metal	Ni t	9,201	7 638	7 945	7 637	4 719	**37 114**
	Cu t	7 542	5 984	5 821	5 747	3 577	**28 670**

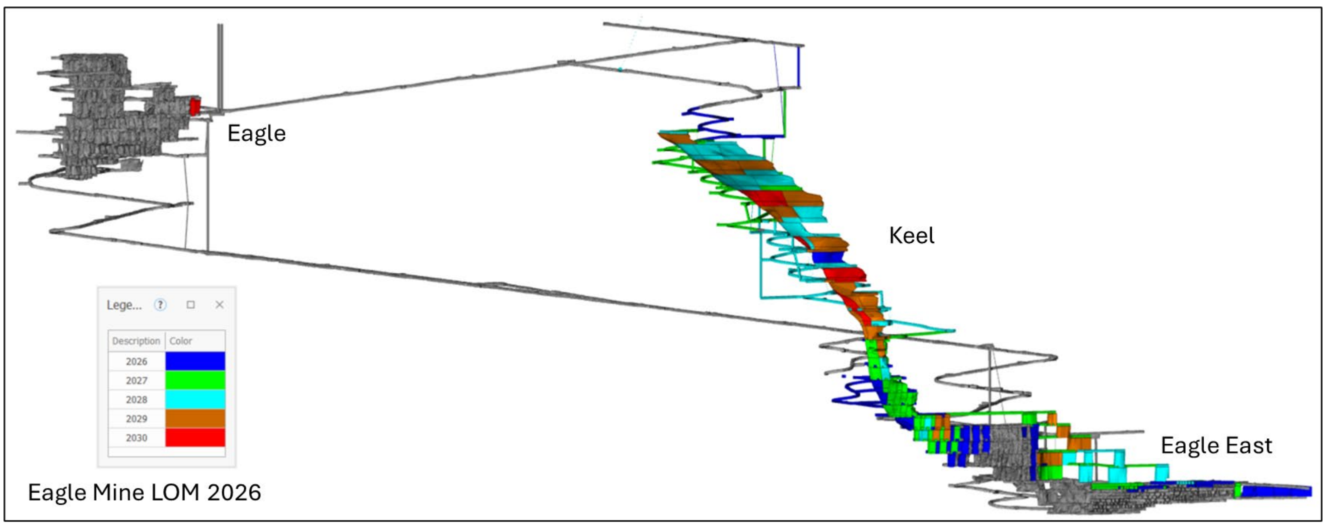


Figure 16.32: LOM Production Plan – Orthographic View

Figure 16.33 displays the LOM ore production by zone, while Figure 16.34 illustrates the production of nickel and copper metals. Figure 16.34 highlights the steady delivery of Nickel and Copper metals during mining activities in the Eagle East and Keel at a 2,200 tonnes per day production rate.

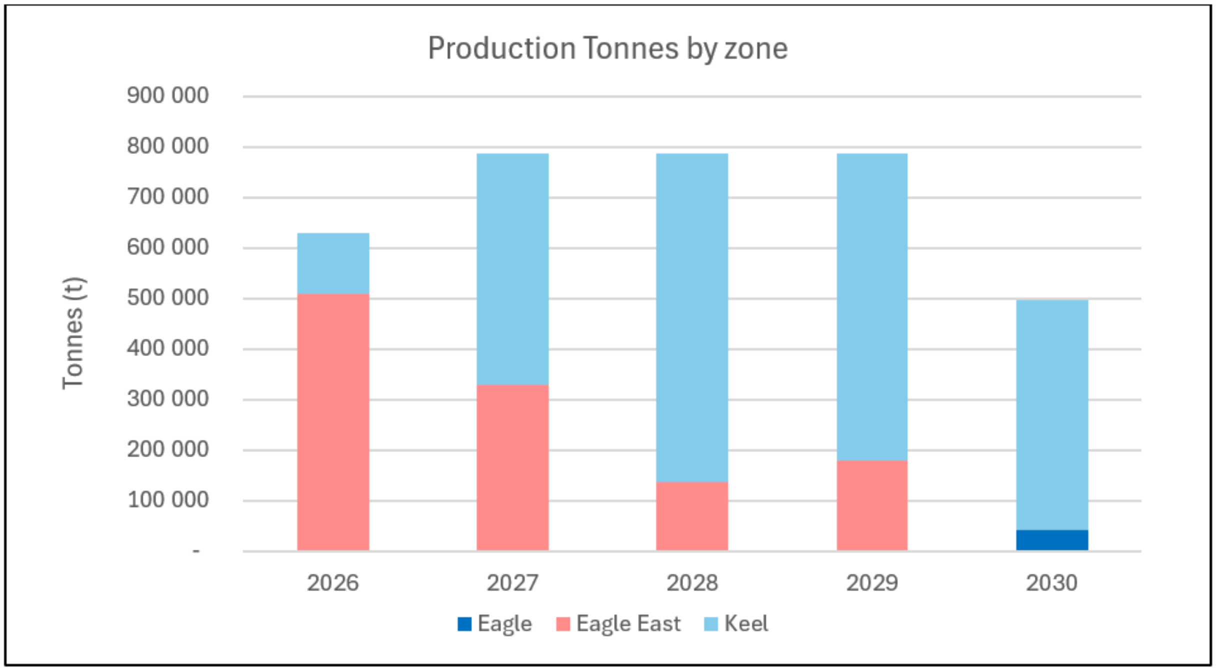


Figure 16.33: LOM Production Plan – Ore Production by Zone

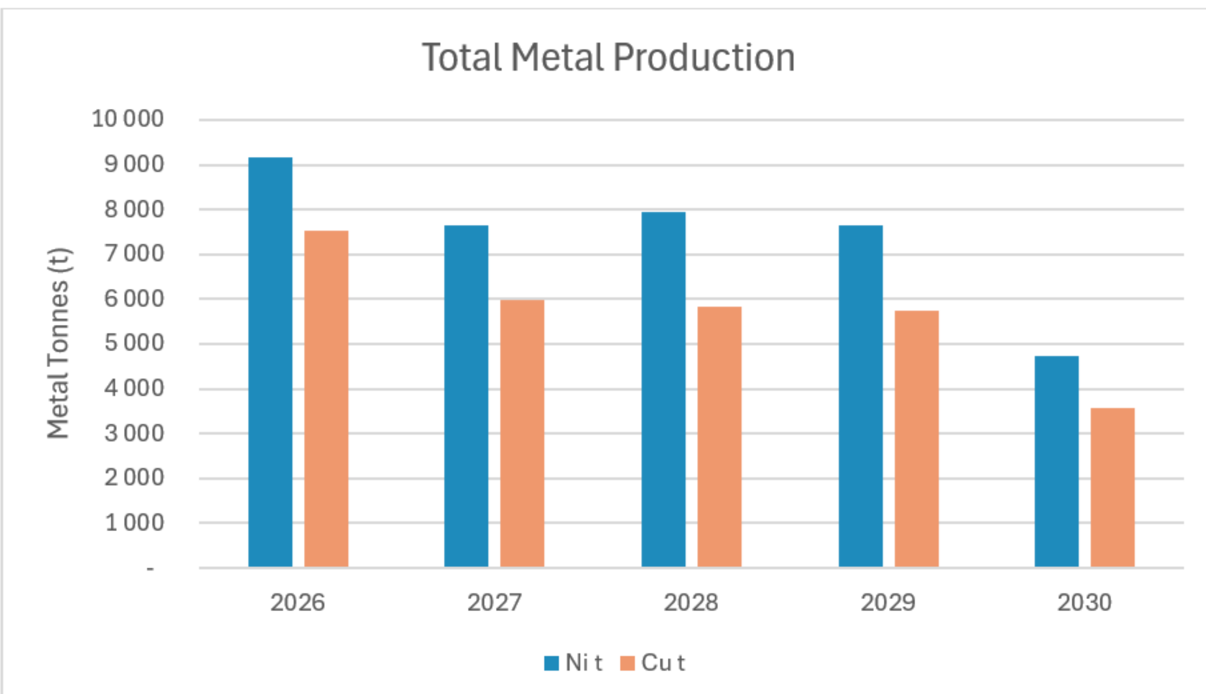


Figure 16.34: LOM Production Plan – Nickel and Copper Metal Production

Table 16.20 presents the LOM production schedule by mining method. The schedule indicates a progressive reduction in drift and fill tonnage as production shifts entirely to the extraction of the remaining stopes in the Eagle East and Keel. Overall production from the two longhole mining methods is similar over the LOM, with slightly higher tonnes being attributed to the transverse longhole method than the longitudinal method.

Table 16.20: LOM Production Plan by Mining Method

Zone	Type	2026	2027	2028	2029	2030	Total
Eagle	Transverse Stope	-	-	-	-	37 852	37 852
	Longitudinal Stope	-	-	-	-	-	-
	Cut and fill	-	-	-	-	-	-
	Dev Ore	-	-	-	-	2 681	2 681
Eagle East	Transverse Stope	274 926	154 928	39 131	89 528	-	558 513
	Longitudinal Stope	76 918	59 303	83 116	75 305	-	294 642
	Cut and fill	94 430	34 847	9 670	-	-	138 946
	Dev Ore	63 214	80 598	4 476	14 927	-	163 214
Keel	Transverse Stope	63 551	348 977	131 964	245 783	252 733	1 043 007
	Longitudinal Stope	-	17 284	413 244	316 078	165 570	912 176
	Cut and fill	-	-	-	-	-	-
	Dev Ore	55 432	91 459	104 996	45 659	37 905	335 450
Total Ore	**Transverse Stope**	338 476	503 905	171 096	335 311	290 584	1 639 372
	Longitudinal Stope	76 918	76 587	496 360	391 383	165 570	1 206 818
	Cut and fill	94 430	34 847	9 670	-	-	138 946
	Dev Ore	118 645	172 057	109 472	60 585	40 585	501 345
Total Ore tonnes		**628 469**	**787 396**	**786 598**	**787 279**	**496 739**	**3 486 481**

Figure 16.35 shows the partition of the total ore production tonnes by mining method, while Figure 16.36 illustrates the LOM production ore tonnes by mining method.

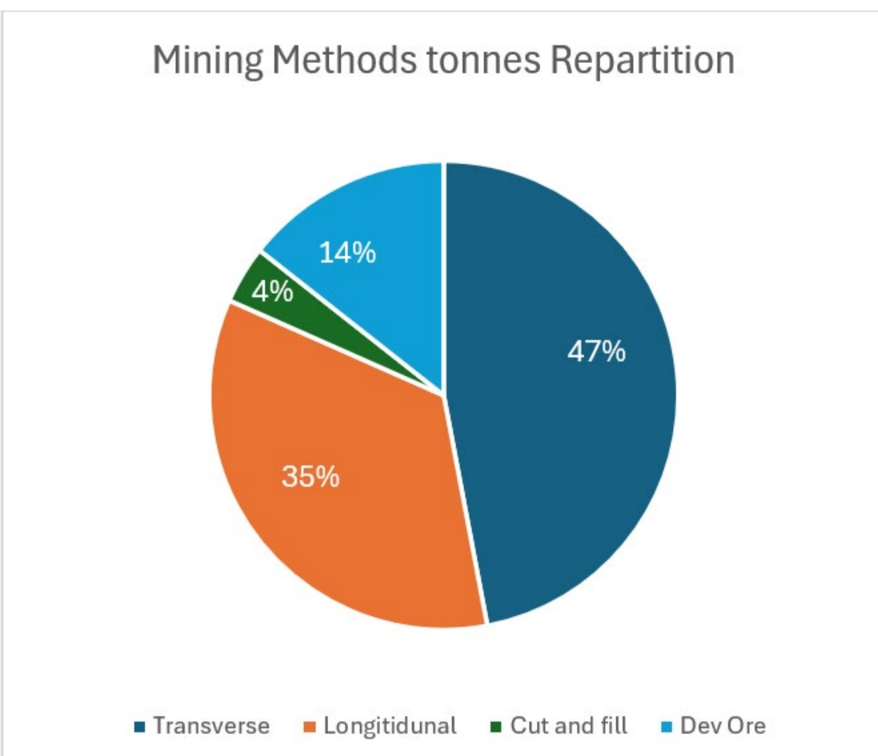


Figure 16.35: Total Ore Production by Mining Method

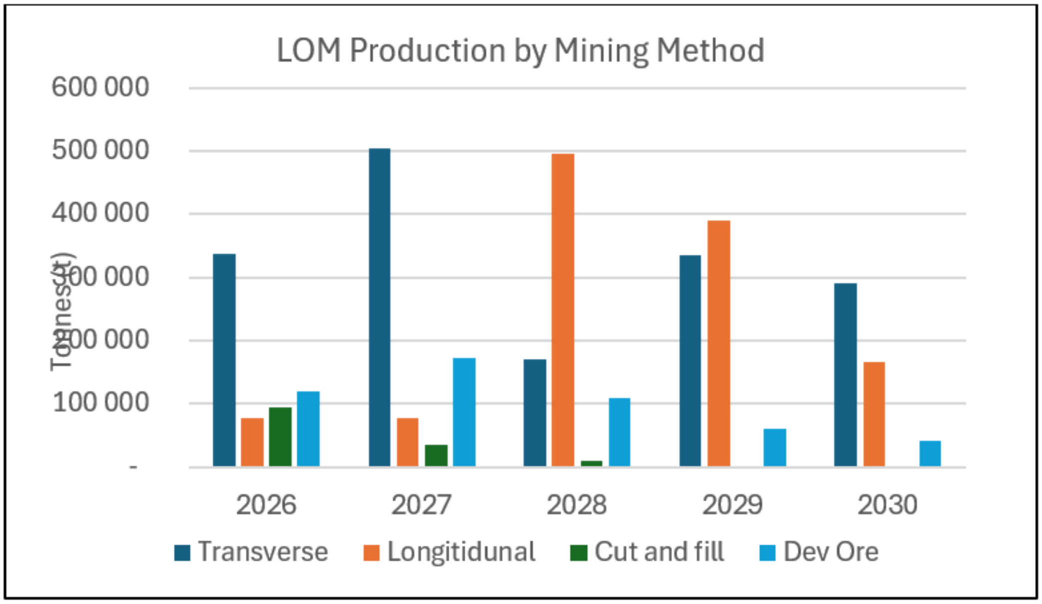


Figure 16.36: LOM Production by Mining Method

16.7 Mine Operations and Management

Table 16.21 lists the personnel dedicated to underground mining operations. Staff personnel, including management and technical services, are Eagle Mine employees who generally work a four-day work week, ten hours daily, from Monday to Friday.

Table 16.21: Personnel Dedicated to Underground Mine Operations

Area	Eagle	Contractors
Management/ Supervision/Safety	23	0
Geology & Technical Services	17	0
Underground Operations	97	0
Mine Maintenance	53	0
Over Road Haulage	0	24
Security	12	0
Surface Operations	21	0
Total	**223**	**24**

Eagle Mine operations personnel include underground miners and surface operators. Operations personnel work 12-hour shifts, seven days a week, on a seven-days o,seven-days off rotating schedule. There are four rotating crews such that the mine operates continuously on a 24/7 basis. Eagle maintains a policy of prioritizing the hiring of residents from local communities. There is no cafeteria or camp at the mine, and the Company does not provide transportation to the site. Eagle employees provide their own transportation to travel to and from the mine site every day. Eagle provides light vehicles for transportation of its employees to underground, and contractors manage their own vehicles. There is ample parking space available for private vehicles on the surface. Most of the personnel reside in Marquette or other local communities and bring their lunches to work. The personnel at the mine are non-union.

The QP reviewed the personnel organization and is of the opinion that it is appropriate for the scale of an underground mining operation, such as the Eagle Mine.

17. Recovery Methods

17.1 Processing

The Humboldt Mill is a former iron ore processing plant that was converted to process Eagle ore. The ore is transported from the Eagle Mine to the Humboldt Mill (Figure 17.1) in special highway haul trucks and is delivered to the Coarse Ore Storage Area (COSA) near the Humboldt Mill (Figure 17.2). Here, it undergoes a conventional three-stage crushing process and is then stored in bins. The ore then progresses through a single-stage ball milling process followed by bulk flotation, and separation flotation to produce separate nickel and copper concentrates. Metallurgical recoveries of nickel and copper average 85% and 97%, respectively, for Eagle Mine ore. Tailings from the plant are deposited sub-aqueously in the adjacent former Humboldt iron ore mine open pit, now known as the HTDF.

Nickel and copper concentrates are stored in a covered concentrate building on site prior to being transported via rail car to smelter facilities within North America.

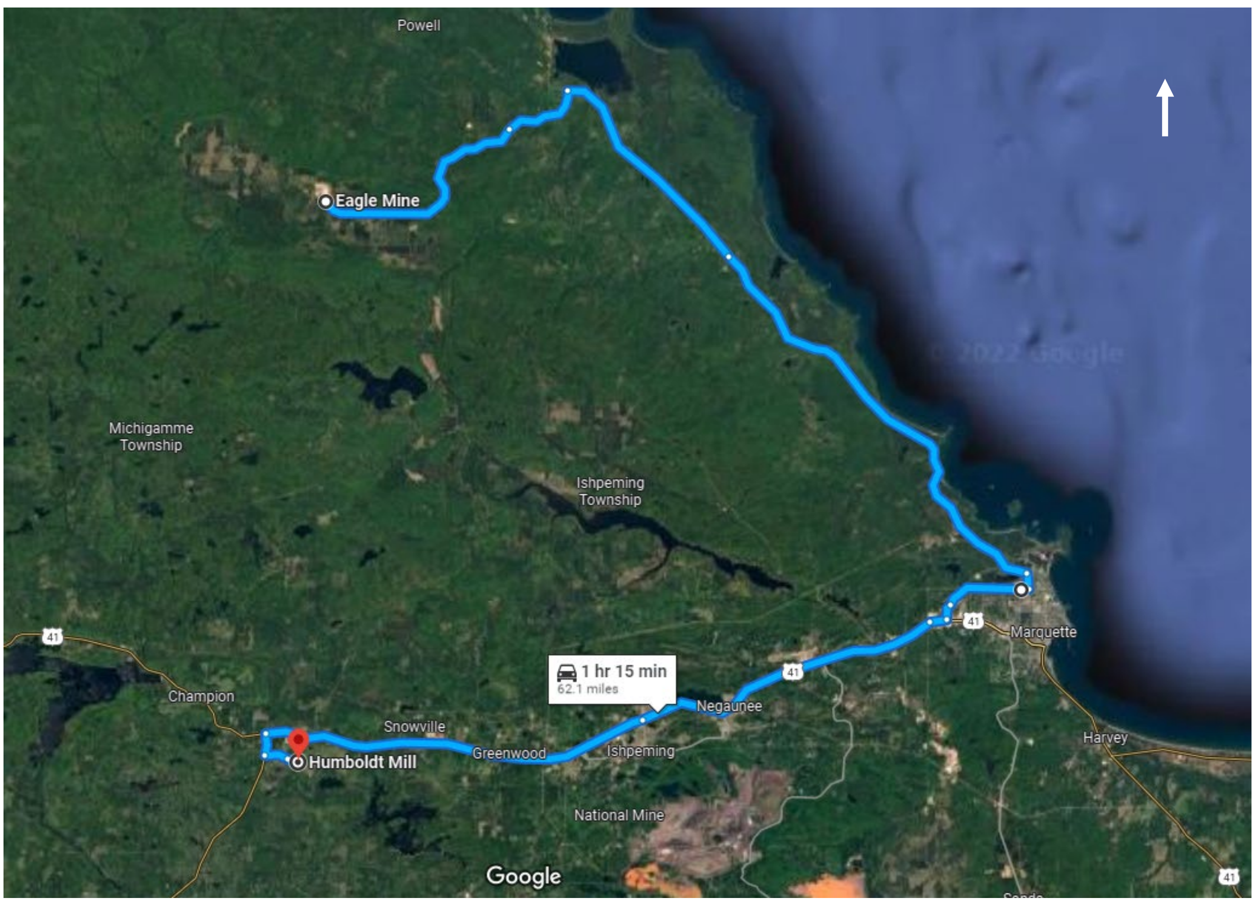


Figure 17.1: Humboldt Mill in Relation to the Eagle Mine

Source: Talon Metals (2026)

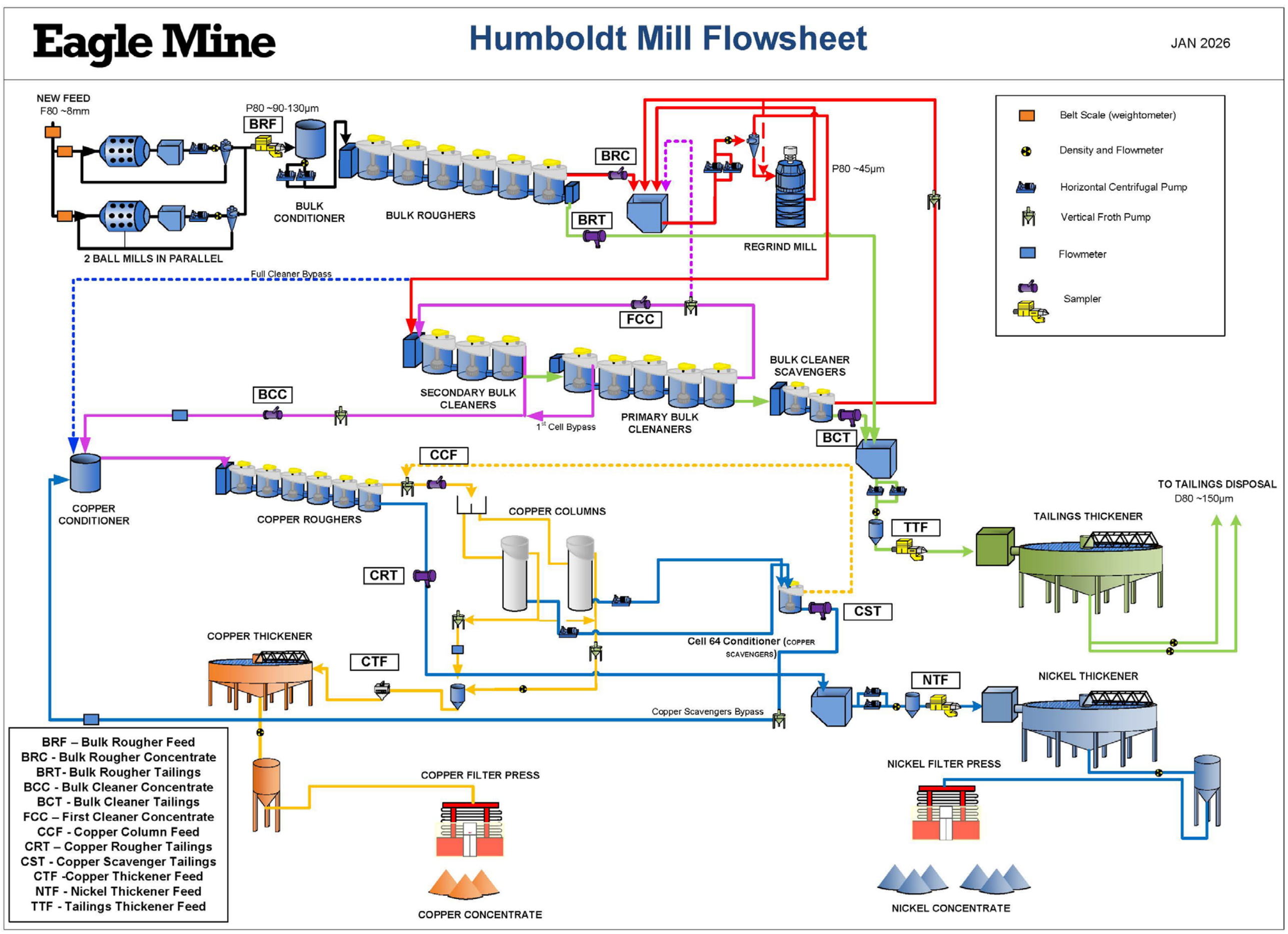
Figure 17.2: Humboldt Mill Complex

The Eagle process flowsheet has remained virtually unchanged and uses conventional technologies to produce separate copper and nickel concentrate with a nameplate throughput of 2,000 tpd (730,000 tpa). A simplified process flowsheet is shown in Figure 17.3. Key processes at the Humboldt Mill are summarized below:

ROM ore in the mine is loaded by a front-end loader into road haul trucks to transport ore to the milling facility. There are approximately 10,000 tonnes of storage capacity in the COSA at the mill:

- Initial size reduction of the ore is carried out by a primary jaw crusher to reduce the ore size from nominal minus 450 mm ROM to a P_{80} = 100 mm.
- Further size reduction of primary crushed ore is carried out in a secondary and tertiary cone crushing circuit to reduce the ore size from F_{80}= 100 mm to P_{80} = 8 mm.
- The tertiary crushed ore is stored in bins and then reclaimed by feeders to feed the grinding circuit.
- The ball mill feed is processed in two parallel, single-stage ball mill grinding circuits. Each circuit operates in closed configuration with hydrocyclones, targeting a product P_{80} of 130 microns. Sodium carbonate is added to the mills for pH and water chemistry control.
- A bulk copper-nickel concentrate is produced by separating the copper and nickel minerals from gangue material by rougher flotation. The copper-nickel bulk concentrate is reground, followed by cleaning stages to further reject gangue minerals. The bulk cleaner concentrate is then subjected to a final flotation stage where the copper and nickel minerals are separated from one another through the addition of lime. Final concentrate grades are 13% Ni and 2% Cu in the nickel concentrate and 31% Cu and 0.8% Ni in the copper concentrate.

- An on-stream analyzer provides real-time analysis from 12 streams in the mill and collects a 12-hour shift composite sample for analysis at the onsite analytical laboratory operated by SGS.
- Copper and nickel concentrates are dewatered to 8% to 10% moisture content using dedicated thickening and filter press systems before being loaded into railcars for transport. These concentrates are then shipped by rail directly to smelting facilities.
- Flotation tailings are thickened, and the slurry is pumped to the existing HTDF for sub-aqueous deposition.
- Facilities are also present for storing, preparing, and distributing reagents used in the process. Reagents include sodium isopropyl xanthate (SIPX), methyl isobutyl carbinol (MIBC), soda ash, lime, flocculant, and carboxymethylcellulose (CMC).
- Water from the concentrate dewatering operations, tailings dewatering, and the HTDF are recycled for reuse in the plant process. Plant water stream types include process water, fresh water, reclaim water, and potable water.



Source: Talon Metals (2026)

Figure 17.3: Humboldt Mill Flowsheet

17.1.1 Production Rate and Product Quality

During the period from January 2025 to February 2026, the mill average throughput was 56,783 tonnes per month versus 61,091 budgeted. Table 17.1 provides additional performance indicators.

Table 17.1: Average Monthly Performance for the Humboldt Mill – January 2025 to February 2026

Item	Units	Actual	Budget
Throughput	tonnes	56,783	61,091
Ni concentrate grade	%	12.0	12.0
Cu concentrate grade	%	28.6	30.5
Ni Metal production	tonnes	803	910
Cu Metal production	tonnes	730	809
Ni Recovery	%	83.2	84.4
Cu Recovery	%	95.3	95.7

Figure 17.4 illustrates the monthly variations in both the production volume and the grade of nickel and copper concentrates from January 2025 to February 2026.

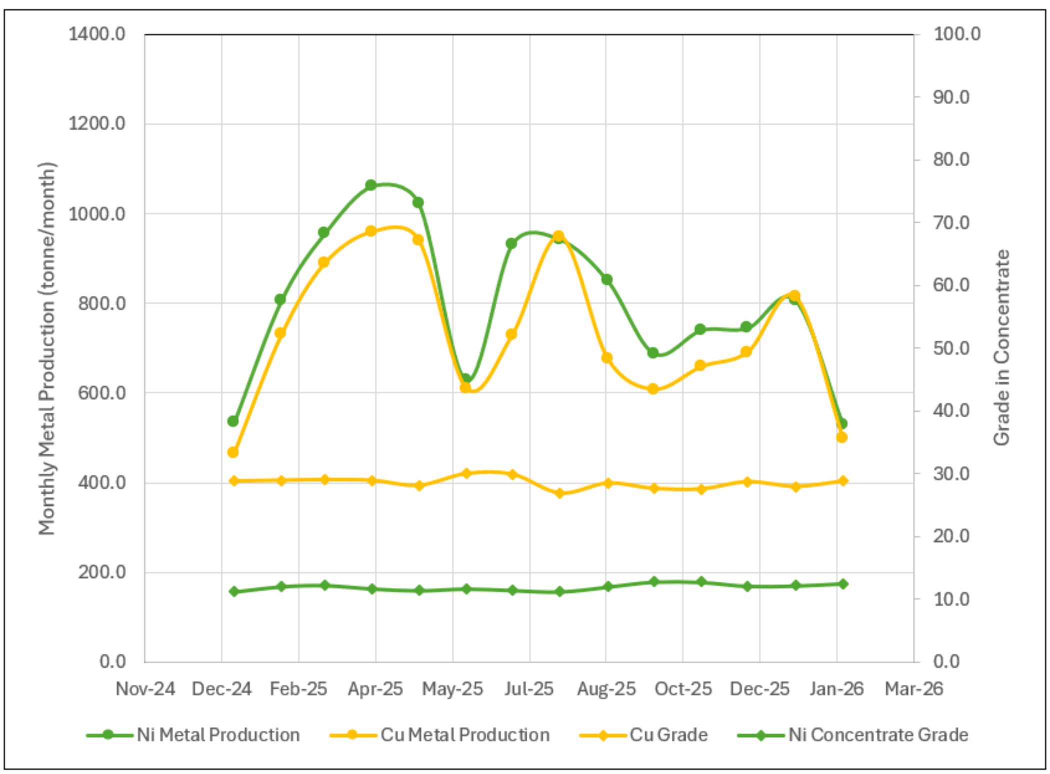


Figure 17.4: Nickel and Copper Monthly Production and Grades (January 2025 ~ February 2026)

17.2 LOM Production Schedule (2026-2030)

Table 17.2 presents the forecasted LOM production of metals in concentrate based on the most recent mine plan. The data for 2026 does not include actual production figures for January and February in the table.

Table 17.2: LOM Processing Plan – Eagle Mine

Item	Unit	2026	2027	2028	2029	2030
Feed	kt	628	787	787	787	497
Ni	%	1.46	0.97	1.01	0.97	0.95
Cu	%	1.20	0.76	0.74	0.73	0.72
Co	%	0.03	0.03	0.03	0.03	0.03
Au	g/t	0.13	0.09	0.08	0.08	0.08
Pt	g/t	0.33	0.22	0.20	0.18	0.18
Pd	g/t	0.22	0.15	0.14	0.13	0.12
MgO	%	18.06	19.69	18.59	18.94	17.80
Contained Metal						
Ni	t	9,176	7,599	7,927	7,644	4,739
Cu	t	7,542	6,010	5,814	5,709	3,560
Co	t	251	218	218	208	125
Au	g	92,314	71,431	66,587	63,175	40,300
Pt	g	226,055	176,243	154,522	144,518	90,920
Pd	g	153,586	118,146	107,562	102,372	60,951
Overall Recovery						
Ni	%	83.33	78.55	79.13	78.63	78.40
Cu	%	95.55	93.59	93.41	93.31	93.24
Co	%	84.53	79.75	79.83	79.83	79.60
Au	%	71.66	70.19	70.06	69.98	69.93
Pt	%	74.99	70.70	71.22	70.77	70.56
Pd	%	83.33	78.55	79.13	78.63	78.40
Metal Recovered to Nickel Concentrate						
Ni	t	7,585	5,979	6,256	6,008	3,751
Cu	t	1,284	1,012	1,059	1,017	635
Co	t	192	171	172	164	98
Pt	g	124,319	89,352	79,140	73,373	45,967
Pd	g	81,904	57,364	52,845	49,788	29,499
Metal Recovered to Copper Concentrate						
Cu	t	5,936	4,632	4,385	4,326	2,700
Au	g	54,499	41,289	37,672	35,901	22,929
Nickel Concentrate Grade						
Ni	%	13.0	13.0	13.0	13.0	13.0
Copper Concentrate Grade						
Cu	%	30.5	30.5	30.5	30.5	30.5

17.3 Mill Annual Throughput and Concentrate Grade (Actual and Forecast)

Figure 17.5 illustrates the actual annual mill production throughput from 2015 to 2025, as well as forecasts for 2016 through 2030. The grades of nickel and copper concentrate, both actual and forecasted, are also included. The decline in production during 2024 was attributable to a mine-related incident that adversely affected mill performance. The drop in production in 2030 results from the final year of the mine plan, which yields less ore.

The historical average for annual mill throughput was calculated using data from typical operating years between 2016 and 2023, as well as 2025. Given that Keel ore possesses a higher hardness, it may negatively affect mill throughput in comparison to historical performance.

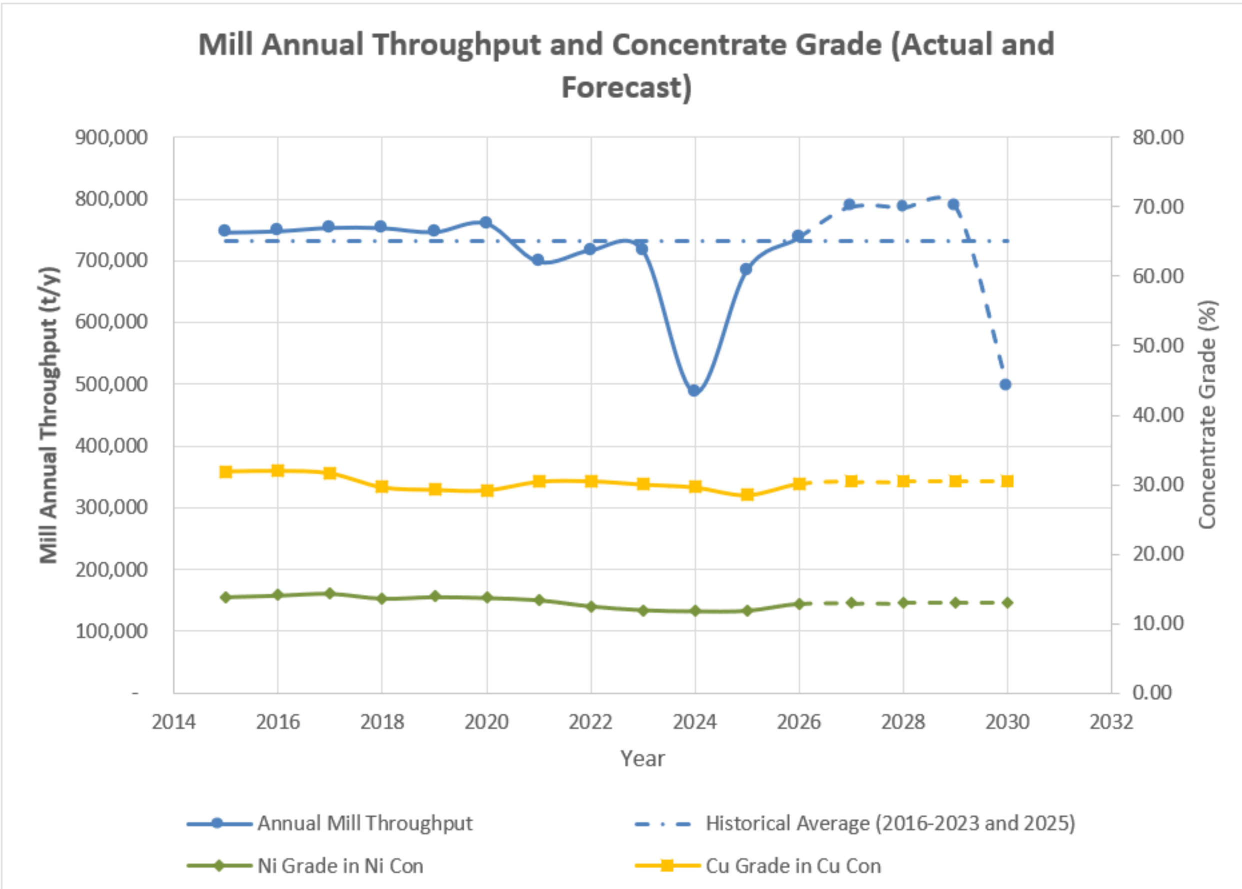


Figure 17.5: Actual and Forecast Annual Throughput

17.4 Concentrate Quality

The recent production results can be used to extrapolate into the future. The copper concentrate is of high quality with an average grade around 30% copper, which is nearly 90% chalcopyrite. The nickel concentrate produced contains a nickel grade at 12% on average. The concentrate target is reviewed regularly to account for nickel price and smelting conditions to optimize revenues. There have been no issues with talc in the concentrate.

18. Project Infrastructure

18.1 Tailings Disposal

The Humboldt Tailings Disposal Facility (HTDF) is used for permanent disposal of the tailings produced at the Humboldt Mill. The HTDF is a pit lake that formed in the open pit of a former iron ore mine (the Humboldt Mine) when mining operations ceased in the late 1970s. It was used in the 1980s for sub-aqueous disposal of tailings produced from ore mined at the Ropes Mine, a historical gold mine. Since 2014, tailings produced by Eagle at the Humboldt Mill have been deposited sub-aqueously into the HTDF. Disposal of sulfidic tailings beneath a water cover limits their exposure to oxygen, preventing the generation of acid mine drainage, and represents an industry best practice. In addition, Eagle recycles water from the HTDF in the milling process and manages process water produced at the site in the HTDF. Water management includes treatment and discharge under an NPDES permit.

The key components of the HTDF are:

- Tailings delivery system
- Tailings vault and deposition system
- Pit lake
- Water reclaim system
- Cut-off wall
- Water treatment plant (WTP)
- Zero liquid discharge (ZLD) plant

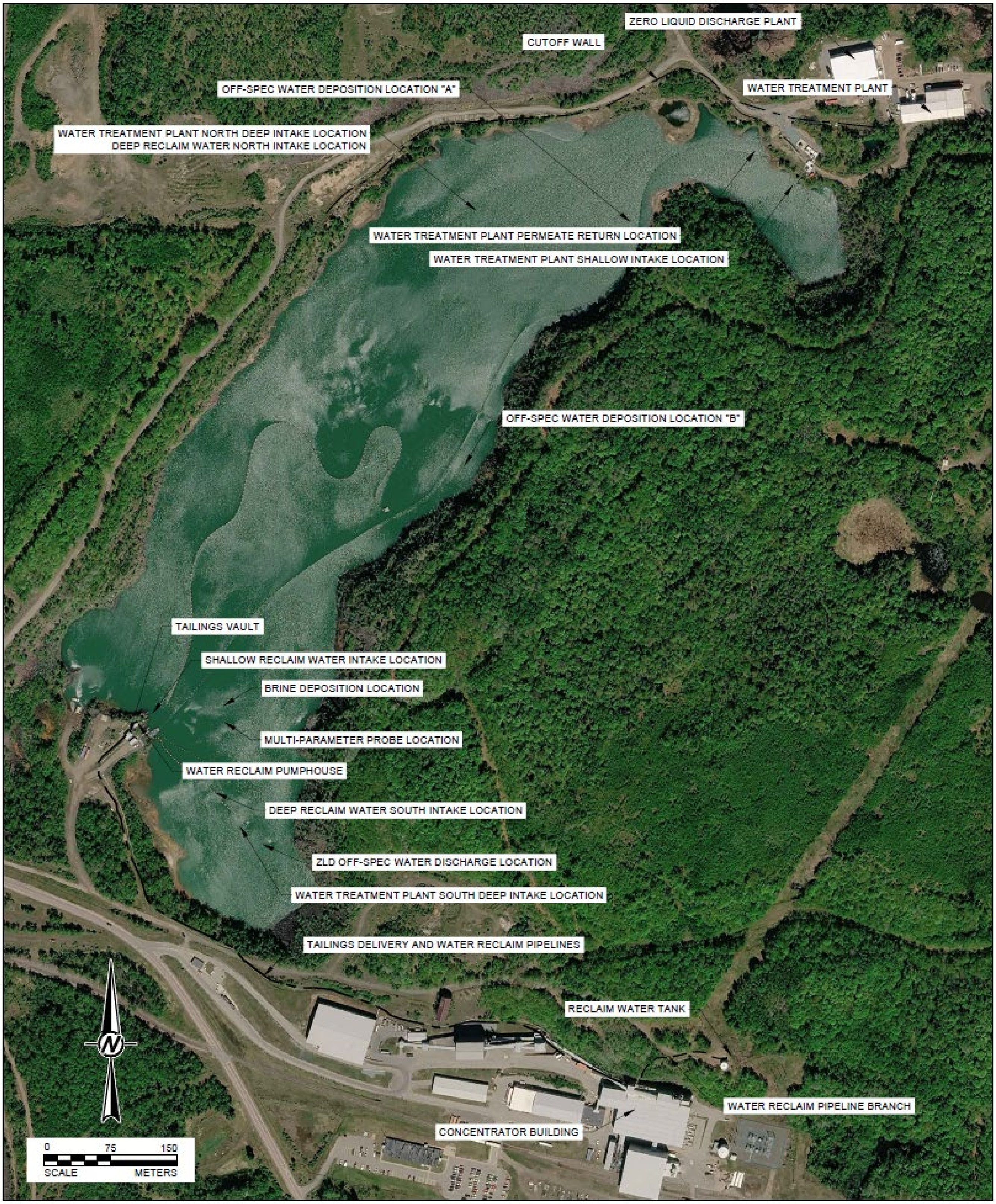


Figure 18.1: Humboldt Tailings Disposal Facility and Related Features (as of April 2026)

18.1.1 Tailings Delivery System

Flotation tailings are collected and pumped to the tailings thickener at the concentrator building. Thickener underflow is pumped from the tailings thickener to the tailings vault, which is situated along the southwestern perimeter of the pit lake. The tailings slurry is delivered in one of two double-containment high-density polyethylene (HDPE) pipelines (one duty, one standby). For each pipeline, the outer containment pipe is approximately 203 mm (8 inches) in diameter, and the carrier pipe is approximately 102 mm (4 inches) in diameter. The pumps (one duty, one standby) are Warman centrifugal slurry pumps with the design point at a flow rate of 83 cubic meters per hour (365 US gallons per minute) and a head of 42.7 m (140 feet), driven by TECO motors. For redundancy, either pump can deliver tailings through either pipeline. The tailings delivery pipelines are routed across the ground surface (and through a culvert at an access road crossing) from the mill to the HTDF. The approximate alignment of the pipelines is shown in Figure 18.1.

18.1.2 Tailings Vault and Deposition System

The tailings vault is a small building located along the southwestern perimeter of the HTDF that houses piping, valves, instrumentation, and electrical equipment used for tailings deposition within the HTDF. The tailings delivery pipelines from the mill enter the tailings vault below grade from the south. Knife gate valves can be configured to route tailings into any of three tailings deposition pipelines. Tailings flow in the pipeline from the tailings vault to the selected sub-aqueous deposition point. The pipelines consist of DR 17 HDPE pipe with a diameter of approximately 152 mm (6 inches). Typically, one of the pipelines routes to a barge that allows downward deposition, one of the pipelines routes to a winter deposition point on the floor of the HTDF, and one of the pipelines routes to a backup deposition point on the floor of the HTDF for use in the event of an upset condition. A second barge is available in case an additional downward deposition point is desired. Specific deposition locations are prescribed in the tailings deposition plan, which is updated periodically as needed (typically about once per year).

18.1.3 Pit Lake

The pit lake is a former open-pit iron ore mine that filled with water when mining operations ceased in the 1970s. It was used in the 1980s for sub-aqueous disposal of tailings produced from ore mined at the Ropes Mine, a historical gold mine. Since 2014, it has been used for sub-aqueous disposal of tailings produced at the Humboldt Mill and for management of process water associated with the milling operation, as well as precipitation, surface water runoff, and groundwater. Because the process water streams and groundwater and surface water managed in the HTDF range in density due to differences in water chemistry, several strata exist through the water column. These strata, or layers, are described in Section 20.1.2. Inputs and outputs (i.e., water and tailings) are carefully managed and monitored to help maintain this stratification, preserve the quality of the near-surface water, and limit the potential for impacts to groundwater around the HTDF.

The surface area of the pit lake is approximately 27 ha (67 acres), and the maximum depth of water is approximately 30 m (100 feet) as of December 31, 2025. The volume in the HTDF occupied by tailings deposited by Eagle is approximately 3.5 million cubic meters (4.6 million cubic yards) as of December 31, 2025.

18.1.4 Water Reclaim System

The water reclaim system includes a water reclaim pumphouse, situated adjacent to the tailings vault, that houses two Pioneer PP63C17-75-4 pumps, which are used to return water from the HTDF to the mill for reuse in the milling process. The suction pipeline for one of the pumps is situated at a shallow depth in the HTDF, while the suction pipeline for the other pump is situated deeper. Piping and valves are in place between the discharge side of the deep-water pump and the suction side of the shallow-water pump to enable blending at the desired ratio based on the water chemistry at the two depths and the needs of the mill. The blend between the shallow water and the deep water is controlled with a proportional-integral-derivative (PID) loop on the distributed control system (DCS) for the mill. Shallow reclaim water is typically the predominant source for reuse in the mill. Reclaim water is routed from the reclaim pumphouse to the mill in a DR 11 HDPE pipeline that has a diameter of approximately 203 mm (8 inches), with a branch that can also route reclaim water to the reclaim water tank, which is situated on a hill adjacent to the mill. The water reclaim pipeline is routed across the ground surface along the same alignment as the tailings delivery pipelines, with the branch to the reclaim water tank routing along an access road up the hill. The approximate location of the pipeline is shown in Figure 18.1. The deep-water pump is also used to provide a continuous flow of approximately 6.9 to 11.3 cubic meters per hour (30 to 50 US gallons per minute) to the unused tailings deposition pipelines to prevent tailings from plugging the outlets and to prevent the tailings deposition pipelines from freezing in the winter months.

18.1.5 Cut-off Wall

A cut-off wall, approximately 685 m (2,247 feet) in length, was constructed adjacent to the pit lake along its northwestern perimeter in 2014. The purpose of the cut-off wall is to reduce the potential for migration of water from the HTDF into the shallow groundwater aquifer north of the HTDF. The cut-off wall included construction of a 1-meter-wide (3-foot-wide) soil-bentonite slurry wall in the overburden materials and construction of a grout curtain below portions of the soil-bentonite slurry wall. The location of the cut-off wall is shown in Figure 18.1.

18.1.6 Water Treatment Plant

A WTP is operated for the removal of total dissolved solids (TDS), metals, and suspended solids prior to discharge in accordance with an NPDES permit. An oxidation reactor is available as the initial treatment step to destruct thiosulphates and reduce the chemical oxygen demand. However, the oxidation reactor has been idled in recent years, due to lower thiosulphate levels in the HTDF. Following this step, neutralization and metal precipitation occur in a coagulation reaction tank. Then, particulates are removed using a lamella clarifier with polymer aid and an ultrafiltration system. Finally, a reduction in TDS concentration is accomplished with a Brackish Water Reverse Osmosis (BWRO) system. The BWRO system produces brine with elevated TDS concentrations. The brine is preferentially sent to the ZLD plant described in Section 18.1.7, but it can alternatively be deposited at depth near the southern end of the HTDF at the location shown in Figure 18.1 (as of April 2026). Unless it is agitated, the brine remains deep in the water column because it is relatively dense. The WTP also produces off-spec water that is currently deposited along the eastern edge of the HTDF at the location shown in Figure 18.1 (as of April 2026).

18.1.7 Zero Liquid Discharge Plant

In 2025, Eagle completed commissioning of a ZLD plant that uses mechanical vapor recompression technology to evaporate and crystallize the brine from the BWRO system. Brine is fed directly from the WTP to the ZLD plant. The purpose of the ZLD plant is to decrease the volume of brine that is managed in the HTDF, helping to reduce TDS concentrations and the anticipated closure duration. Salt solids are the primary byproduct of the ZLD plant. The solids are hauled offsite and are currently disposed of in a landfill in Whitelaw, Wisconsin.

18.1.7 Tailings Deposition Strategy

The primary design requirements for the HTDF are:

- Provide sufficient volume to contain the tailings produced during the mine life:
- The maximum permitted tailings elevation is 461.8 m (1,515 feet) amsl (Michigan Department of Environmental Quality 2018).
- For preservation of near-surface water quality, sequence tailings deposition to fill spaces as low as possible in the water column for as long as possible.
- Provide a tailings ridge of sufficient height across the HTDF in an east-west direction to establish a southern basin that can contain brine produced by the WTP below the lowest section of the ridge (i.e., without migrating into the northern basin or mixing appreciably with the near-surface water).
- Maintain a water surface elevation that provides adequate freeboard and establishes an inward hydraulic gradient from the groundwater regime surrounding the HTDF (i.e., a condition where groundwater flows into the HTDF, rather than flowing outward from the HTDF into the surrounding environment) during operation. The water level is primarily managed through the discharge of water treated by the WTP. Thus, the ability of the WTP to consistently treat water from the HTDF and achieve discharge requirements throughout the LOM is important for maintaining a suitable water balance and water level.
- For the freeboard requirement, the maximum water elevation is 469.24 m (1,539.5 feet) amsl.
- For the establishment of an inward hydraulic gradient, the maximum water elevation is typically about 468.5 m (1,537 feet) amsl.
- Eagle generally targets a water elevation of about 466.7 to 467.3 m (1,531 to 1,533 feet) amsl to provide a margin of safety and enhanced operational flexibility.

Table 18.1 summarizes the dry tonnage of tailings expected to be produced in each year of the mine life. Projections are based on the mine plan provided by Eagle.

Table 18.1: Tailings Deposition Schedule for the HTDF

Year	Tailings Production (dry tonnes)
2026	645,120
2027	726,474
2028	724,042
2029	726,957
2030	459,373

Tailings deposition modeling is predicated on an in-place (long-term, consolidated) tailings dry density of 1.90 tonnes per cubic meter (119 pounds per cubic foot), which is based on densities calculated from bathymetric surveys over time and the results of laboratory slurry consolidation testing (Golder Associates Ltd. 2020). Sub-aqueous tailings deposits, which form as “cones” at the deposition points, are modeled with a slope of 15 percent based on typical slope angles observed from bathymetric surveys.

Generally, one of two tailings deposition methods can be used. These are referred to as the winter deposition method and the summer deposition method. The presence of lake ice (generally from early to mid-November through late April or early May) prevents or hinders the repositioning of tailings deposition pipelines to change the deposition location over the winter. Therefore, the goal of the winter deposition method is to utilize a single deposition location (or sometimes two deposition locations) that can accommodate the tailings volume produced during the entire winter deposition period. To accomplish this, a tailings deposition pipeline is installed along the floor of the HTDF to the deposition point, and tailings are deposited such that a cone forms upward from the outlet. The tailings deposition pipeline is weighted with concrete cylinders to prevent it from moving or floating. A new pipeline is installed for each winter deposition point, typically the summer before it is needed. A backup deposition point is also established prior to each winter deposition period based on conditions at that time. Backup points are established in the same way, with previous or planned future winter deposition points sometimes serving as backup points. The goal of the summer deposition method is to fill between the cones generated during the winter deposition period to maximize the tailings disposal capacity of the HTDF. Eagle uses floating pipelines to deposit tailings at targeted locations during the summer deposition period, which enables more rapid changes between deposition points and more efficient filling of the HTDF without leaving large gaps between cones.

Other operational constraints considered in the tailings deposition plan include:

- Tailings deposition is kept as low in the water column as possible to limit thermal effects from the elevated temperature of the tailings slurry in the upper layers of the HTDF.
- Tailings deposition is kept far enough away from the WTP intake location to limit agitation and suspension of particulates that could be caused by nearby tailings deposition.
- As an added precaution to limit potential seepage rates from the HTDF into surrounding groundwater, the deposition points adjacent to the cut-off wall alignment are located so that tailings material will only come into contact with the pit wall where there is interpreted to be low-permeability bedrock. The lowest elevation where the top of the low-permeability bedrock unit intersects the pit wall is estimated to be approximately 457.2 m (1,500 feet) amsl along the cut-off wall alignment. Tailings deposition is planned to occur far enough away

from the pit wall that the tailings deposit should not contact the pit wall above an elevation of 455.7 m (1,495 feet) amsl.

The tailings deposition modeling shows that sufficient capacity exists in the HTDF to dispose of tailings produced at the Humboldt Mill through the LOM with tailings deposited at or below the maximum permitted elevation of 461.8 m (1,515 feet) amsl. Specifically, about 2.0 million cubic meters (2.6 million cubic yards) of capacity is available up to an elevation of 461.8 m (1,515 feet) amsl as of December 31, 2025, with a reasonable allowance made to account for inefficiency in tailings placement due to the conical shape of the deposits and the space left between cones. This volume is sufficient to accommodate the estimated in-place tailings volume of 1.7 million cubic meters (2.2 million cubic yards) to be produced from December 31, 2025, through the remaining LOM at an assumed in-place dry density of 1.9 tonnes per cubic meter (119 pounds per cubic foot).

18.1.9 Monitoring

The monitoring program for the HTDF involves routine inspection and obtaining measurements related to the operation, structural integrity, safety, and environmental performance of the facility. It is intended to identify deviations from expected performance and facilitate the evaluation, selection, implementation, and monitoring of mitigation measures if needed. It consists of both qualitative and quantitative comparisons of actual versus expected conditions.

Routine visual observations are conducted by trained Eagle personnel. Some facility components are observed daily or weekly, while others are observed monthly (at a minimum). Visual observations are conducted each day, with different components observed on different days such that each key component is observed no less frequently than once each week, to the extent that safe access is possible based on weather, ground, and/or road conditions. Observing the HTDF on a daily basis from a variety of vantage points provides opportunities to identify deviations from typical conditions that may indicate a developing issue. Additionally, a camera is mounted inside the tailings vault and can be monitored from the on-site control room, which is staffed at all times.

Instrumentation for monitoring of tailings delivery includes sensors to measure the tailings flow rate and pressure, as well as sensors at the tailings vault to detect moisture in the annular spaces of the double-containment pipelines. These instruments are connected to the DCS and can be monitored from the on-site control room. Instrumentation for the HTDF includes a water level sensor. This instrument is connected to the DCS and can be monitored from the on-site control room. Instrumentation for the water reclaim system includes sensors to measure flow rates. These instruments are connected to the DCS and can be monitored from the on-site control room. Eagle has also installed sonar heads beneath the water surface that enable real-time imaging and visual monitoring of tailings deposition.

A multi-parameter probe is moored near the southern end of the HTDF and is raised and lowered four times per day when there is no ice across the surface of the HTDF (generally from May into November each year). The probe measures temperature, specific conductance, pH, dissolved oxygen content, oxidation-reduction potential, turbidity, fluorescent dissolved organic matter content, chlorophyll *a* content, and blue-green algae content with depth. These parameters are used for geochemical analysis. The location of the probe is shown in Figure 18.1 (as of April 2026).

Eagle personnel routinely lower a conductivity-temperature-depth (CTD) probe through the water column near the southern end of the HTDF when there is no ice across the surface (generally from May into November each year) to support geochemical analysis. Additionally, Eagle personnel lower the CTD probe along a transect across the

HTDF at least once per year to support analysis of spatial variability in geochemical conditions. Eagle personnel sometimes lower the CTD in other locations in response to specific requests for additional data.

Groundwater quality is monitored quarterly for compliance with Nonferrous Mineral Mining Permit MP 01 2010 (Michigan Department of Natural Resources and Environment 2010) through a network of 24 monitoring wells in 14 physical locations (several of the wells are nested). Ten of the well locations are positioned to monitor the performance of the cut-off wall, with two of them situated inside the cut-off wall to enable comparison between groundwater conditions inside and outside the cut-off wall. Four of the well locations are positioned around the mill infrastructure.

Bathymetric surveys are conducted semi-annually to map the tailings surface within the HTDF and allow for comparison of actual conditions against the tailings deposition plan. Bathymetric surveys are generally conducted in late spring (May or early June) and early fall (late September or October). Analyses are carried out to evaluate the apparent tailings volume placed since the previous bathymetric survey, the apparent in-place density associated with the deposited volume (based on the tailings tonnage deposited during the same period), and the apparent range of slope angles associated with recent tailings deposition. The actual tailings surface is also compared against the planned tailings surface to enable evaluation of whether adjustments to the tailings deposition plan are needed.

18.1.10 Regulatory Compliance

The HTDF is regulated by the Michigan Department of Environment, Great Lakes, and Energy (EGLE). The HTDF does not include a regulated dam under EGLE regulations. Eagle is authorized to discharge from the HTDF through a pipeline to a wetland contiguous to the Middle Branch Escanaba River and directly to the Middle Branch Escanaba River in accordance with NPDES effluent limitations and monitoring requirements included in Permit No. MI0058649 (Michigan Department of Environment, Great Lakes and Energy 2022). Nonferrous Metallic Mineral Mining Permit No. MP 01 2010 (Michigan Department of Natural Resources and Environment 2010) also includes provisions related to tailings disposal in the HTDF, as well as groundwater monitoring around the HTDF.

18.1.11 Corporate Governance

Eagle has established policies, technical standards, and guidance for tailings management that are generally aligned with global industry standards and guidance. Eagle has appointed a Responsible Tailings Facility Engineer for the HTDF, as well as an external Engineer of Record (EOR). Eagle and the EOR have established a consequence classification of Low for the HTDF in accordance with the Global Industry Standard on Tailings Management (GISTM) framework (Eagle Mine LLC 2021). Eagle achieved full compliance with the GISTM in August 2025.

18.2 Site Roads

The Mill site is located approximately 61 km west of the town of Marquette and is accessible by US Highway 41. The Mill is connected to the Eagle Mine, located to the north-northwest, via a 105 km road system that includes the stretch of US Highway 41 from Maquette, County Roads 510 and 550, and Triple A Road. The Mill is also connected to the CN Rail system at Ishpeming (see Figure 18.2).

Within the Mine and Mill sites, internal roads of adequate quality connect facilities and provide reliable year-round access.

Figure 18.2: Aerial View of the Humboldt Mill

Figure 18.3: Aerial View of the Eagle Mine

18.3 Power Supply

The mine site is serviced by grid power provided by the Alger Delta Electric Co-operative (ADEC). An agreement was signed between ADEC and KEMC on January 15, 2008, to provide power to the mine site. ADEC provides power from the city of Marquette to the town of Big Bay, and the overhead lines and associated substation were upgraded to provide 24.9/14.4 kV service to the mine site. The new line from the Big Bay line tap to the mine site is an underground line that supports the estimated 6.3 MVA requirement of the site. A powerhouse constructed at the mine site to step down the 24.9/14.4 kV utility power to 4.16 kV to support mine surface distribution and 13.8 kV to support mine portal, underground, and vent raise distribution. Emergency backup power is provided to portions of the mine by a 4.16 kV, 2,500kVA diesel generator. This generator supplies backup power to the mine administration offices, mine dries, and maintenance sprung building; and supplies the 13.8kV to the mine portal, underground, and vent raise through a step-up transformer located at the powerhouse.

The Humboldt Mill site is predominantly serviced by the Upper Peninsula Power Company, with some power being supplied from WE Energies. The Upper Peninsula Power Company service is fed from a 69 kV American Transmission Company transmission line to an on-site, utility-owned substation. The substation steps down the incoming 69 kV power to 13.8 kV through two 10.5 MVA transformers situated in two redundant banks. This 13.8 kV is fed into the main concentrator building's 13.8 kV switchgear. This switchgear feeds 13.8 kV distribution to the reclaim water area for the mill, as well as pad-mounted transformers that step down the voltage to 4.16 kV and 480 V to support the mill process in a fully redundant design. Critical mill equipment is backed up by a 480 V, 1250 kVA diesel generator to prevent flooding and freezing during the event of a power outage. The mill reclaim area is also backed up by a 480 V 500 kVA diesel generator to ensure proper water supply to the mill and the Water Treatment Facility. The Mill Services Building, Mill Administration Building, Mill Guard House, and Water Treatment Plant Facilities on the mill site property are fed from 24.9/14.4 kV distribution supplied by WE Energies and are stepped down to the various building nominal voltages through various pole-mounted and pad-mounted transformers.

In 2021, Eagle Mine consumed approximately 64.98 GWh of electrical energy.

18.4 Water

An existing non-potable well, in conjunction with a potable well, provides service and drinking water to the mine site. Each is capable of delivering 150 USgpm. There are two wells at the mill: a potable well and a non-potable industrial well. Each is capable of delivering 100 USgpm. Currently, mill operations are supplied by recycled water from the HTDF, but can utilize the industrial well as needed. Hydrology studies at both sites indicate viable long-term aquifers. Both the mine and mill sites utilize septic systems.

18.5 Ancillary Facilities

The Eagle Mine and Humboldt Mill sites are equipped with ancillary facilities necessary to support and sustain reliable operations. These include:

- Water infiltration system for slow release of treated water into the environment at the mine site
- A reverse osmosis water unit for the treatment of water to allow the discharge of water at the mine site
- Powerhouses that include the grid primary connection, emergency generation, and distribution networks

- Mine and Mill, administration, laboratory, and service buildings
- Mine and Mill dry facilities
- Maintenance shops
- Consumables, spares, and supplies warehouses
- Truck Wash
- Storage basins for contact and non-contact surface water
- Cemented crushed rock batch plant for mine backfill
- Mine ventilation fans and heating system
- Mine and Mill security gatehouses
- Rail siding and marshaling yard, complete with concentrate storage and loadout
- Surface tailings disposal facility complete with reclaim water return system

18.6 Concentrate Shipping

The nickel and copper concentrates are stored in a concentrate storage/loadout building immediately adjacent to the mill. The storage capacity of the building is approximately 3,000 wet metric tonnes (wmt) for nickel concentrates and 1,000 wmt for copper concentrates.

A rail spur connecting the mill site to the CN railway network runs through the concentrate storage/loadout building. Railcars are loaded by front-end loaders inside the loadout building, and the railcars are covered by a fiberglass lid. There are additional rail tracks used to store empty and loaded railcars.

An independent contractor is the rail service provider, managing the rail spur and railing the concentrates to the west side of the city of Ishpeming, where they are transferred to the CN rail network for onward railing to Canadian non-ferrous smelters.

19. Market Studies and Contracts

The principal commodities at Eagle are nickel, copper, cobalt, and precious metals contained in nickel and copper concentrates. These products are freely traded at prices that are widely known.

The Eagle nickel and copper concentrates have been sold under long-term contracts directly to smelters or to traders in North America, Europe, and Asia since the start of production.

Both the nickel and the copper concentrates are of clean quality with low levels of impurities and good by-product credits.

Currently, Eagle has nickel concentrate contracts in place with one smelter in Canada to accept 100% of the production until December 31, 2029.

Management is of the opinion that the Eagle concentrate quality makes the concentrate saleable if current contracts are not extended.

All the copper concentrate is sold to a single smelter in Canada for the LOM. The smelter's contract terms are consistent with industry standards.

20. Environmental Studies, Permitting, and Social or Community Impact

This Item contains forward-looking information related to applications, permits, approvals, and consents required, and the time to receive approvals for the Project. The material factors that could cause actual results to differ from the conclusions, estimates, designs, forecasts, or projections in the forward-looking information include any significant differences from one or more of the following material factors or assumptions that were applied in drawing the conclusions or making the estimates, designs, forecasts, or projections set forth in this Item:

- The regulatory framework is unchanged for the Study period.
- No unforeseen environmental, social, or community events disrupt timely approvals.

The Eagle Mine consists of two sites, separated by approximately 18 miles, where environmental studies have been conducted, permits have been issued, and potential social and community impacts are managed:

1) "Mine site" refers to the Eagle underground nickel-copper mine located on Triple A Road in Big Bay, Michigan. The Mine is located within the Salmon Trout River subwatershed of the Yellow Dog Watershed, which drains north into Lake Superior. Environmentally and socially significant features of the Mine site include:
   - Eagle Rock.
   - Mine portal.
   - Underground workings, inclusive of stopes, access declines, and vertical vent raises associated with the Eagle, Eagle East, and upper Eagle East deposits.
   - Temporary development rock storage area (TDRSA).
   - Contact water basins (CWBs).
   - Mine water treatment plant (Mine WTP).
   - Treated water irrigation system (TWIS), a rapid infiltration basin to the Quaternary aquifer and the regulatory point of compliance for Mine WTP effluent during operations.
2) "Mill site" refers to the Humboldt Mill located at 4547 County Road 601, Champion, Michigan, approximately 18 miles south of the Mine. The Mill site is located within the Escanaba River watershed, one of the largest watersheds in Michigan's Upper Peninsula, which drains southeast into Lake Michigan. Environmentally significant features of the Mill site include:
   - Humboldt Mill, which produces nickel and copper concentrates.
   - Humboldt Tailings Disposal Facility (HTDF), a mine pit lake that developed in the 1970s following the closure of an open-pit iron mine operated by Cleveland-Cliffs. In the late 1980s to early 1990s, the HTDF was used for the disposal of cyanide-leached tailings from the Ropes Gold Mine, which was owned and operated by Callahan Mining Company. Since the start of operations in 2014, Eagle has sub-aqueously injected a slurry composed of thickened, sulfide-rich (e.g., pyrrhotite) tailings and process water from the Humboldt Mill into the HTDF.
   - Cut-off wall. Located along the northwest perimeter of the HTDF, this vertical hydrogeologic feature, a soil-bentonite slurry and cement-based grout wall, extends from the ground surface to approximately the bedrock contact. It provides a low-permeability barrier between the glacial sediments in direct

contact with HTDF water and the adjacent Quaternary aquifer.

- Mill water treatment plant (Mill WTP).
- Outfall 004, the end of a pipe routing from the Mill WTP to the Middle Branch of the Escanaba River, and the regulatory point of compliance for Mill WTP effluent during operations.
- Zero liquid discharge (ZLD) plant, which processes a sodium-sulfate reverse osmosis (RO) brine generated by the Mill WTP and produces a solid waste that is disposed in an ash monofill landfill.
- Outfall 003, the discharge point from the HTDF to the adjacent wetland after rehabilitation of HTDF water quality and water level rise, and the anticipated regulatory point of compliance for HTDF discharge following closure.

Since the last NI 43-101 Technical Report in 2023, Eagle has completed the following:

- Geochemical reactivity of low-sulfur paste tailings to support Eagle's 2024 Mine Permit Amendment (WSP 2024, Eagle Mine, 2024).
- Closure study of the underground mine predicting water balance, hydrogeology, and water quality based on the previous LOM.
- Updated limnologic models of the HTDF using the 2-D hydrodynamic model CE-QUAL-W2. The model estimates the physics and conservative chemistry of the HTDF under various operational conditions, as well as the expected remediation timeframe.
- Tailings deposition plans were updated periodically to optimize the use of available storage in the HTDF, accounting for either covering or leaving sub-aqueous pyrrhotite storage areas associated with a potential desulfurization process available for future processing.
- A study of the recommended water cover thickness for sub-aqueous pyrrhotite (WSP 2023).
- Routine evaluations of the management of the tailings disposal facility under the Global Industry Standards on Tailings Management (GISTM) framework.
- Community pulse surveys.

Based on the studies completed to date, existing permits, and ongoing monitoring and management programs, there are no known environmental or social factors that are expected to materially impact the ability to operate or close the Project.

20.1.1 Mine Site

The following points summarize the findings of major studies for the Mine site:

- Under the previous LOM, the underground mine was estimated to take 4.5 years after closure to flood using water pumped from the utility well. After flooding, there will be a downward groundwater gradient within the mine workings. No impacts to the Quaternary aquifer at the Mine site were predicted.
- Due to the very low hydraulic conductivity of mine wall rock, it was estimated for the previous LOM that it will take over 700 years for mine water to discharge to the Salmon Trout River, the nearest downgradient surface water feature.
- Laboratory tests on cemented paste tailings (investigated for possible placement in the underground mine)

found samples to be non-acid generating, except for one sample, which had the highest sulfur content and the lowest binder content. High initial pH values may be expected from the cemented paste tailings, but pH may become circum-neutral in the long term (WSP 2024b).

- The addition of high-sulfur (5.5 to 6.0 weight percent, wt.%) cemented paste tailings to Lower Eagle East and Upper Eagle East slightly increased predicted concentrations of aluminum, fluoride, iron, strontium, and total dissolved solids (TDS). However, for most constituents, the addition of cemented paste tailings caused little to no change in predicted mine water chemistry. This was due to the relatively small contribution of paste tailings pore water relative to other water sources (WSP 2024a).

- Under the previous LOM, due to the predicted low rate of discharge from the flooded mine workings to the downgradient Quaternary aquifer and substantial mixing with background groundwater in the aquifer, no impacts on drinking water quality were expected in the downgradient Quaternary aquifer during and after closure. Due to dispersion along the flow path, no measurable impact on water quality in the Quaternary aquifer or the Salmon Trout River was predicted.

20.1.2 Mill Site

Results of major studies for the Mill site include the following:

- The HTDF is a density-stratified water body with three distinct layers (as of February 2026): Surface, Chemocline, and Deep. No mixing occurred between the Surface Layer and the Deep Layer as of 2025. Tailings are generally deposited within the anoxic Deep Layer and are isolated from the surface environment (WSP 2026).

- A water cover of 3.3 feet is generally considered sufficient to prevent oxygen diffusion through the water cover to the tailings-water interface. Industry guidance recommends a water cover of 10 feet to effectively prevent resuspension of fine-grained tailings upward into the water column by wave action or surface disturbance (WSP 2023c).

- Simple mass balance modeling found that the TDS concentration in the Surface Layer of the HTDF would decrease below 500 mg/L between 4 and 7 years after active tailings deposition ceases.

- A full hydrogeologic barrier cannot be demonstrated in the lower zones of the cut-off wall near the bedrock contact. Eagle manages this by maintaining an inward hydraulic gradient during operations. A fate-and-transport model examined seepage from the HTDF through the cut-off wall and into the downgradient Quaternary aquifer after closure. The model identified a few constituents that are estimated to exceed drinking water criteria at or beyond the property boundary after the 20-year post-closure period (Henderson 2026). Eagle is evaluating options for further modeling to reduce uncertainty in this analysis.

- The Lundin Corporate Tailings Group determined that the site met the requirements of the GISTM as of August 2025 (Henderson 2026).

Pending regulatory approval of current applications for permits and permit amendments (see Section 20.3), WSP is not aware of any environmental issues that could materially impact the issuer’s ability to extract the Mineral Resources or Mineral Reserves.

20.2 Waste Disposal, Monitoring, and Water Management Requirements

20.2.1 Waste and Tailings Disposal

20.2.1.1 Mine Site

At the Mine site, waste rock from the underground mine is stored in the TDRSA. During operations, a portion of the waste rock from the TDRSA is combined with cement and placed underground as cemented rock fill.

Additional waste rock is placed underground as non-cemented rock fill. At closure, all remaining waste rock stored in the TDRSA will be placed underground.

Eagle has received permits to place tailings in the underground mine as paste backfill (MDEQ 2007, amended; EPA 2025). Laboratory geochemical testing on the reactivity of paste tailings has been completed (WSP 2024b), and the impacts of paste backfill on the mine pool water chemistry compared to the originally permitted closed water quality were found to be negligible (Eagle Mine, 2024).To implement paste backfill, a paste plant would need to be constructed, and tailings would need to be transported from the Mill site to the Mine site for underground disposal. Although this is not in the current Life of Mine (LOM) plan considered herein, it is a permitted option for backfill.

Ore is stored in the Coarse Ore Storage Building (COSA) prior to shipment to the Mill. Ore is trucked from the Mine to the Mill for processing. The transportation process is a component of overall operational greenhouse gas emissions and forms part of local traffic activity, including vehicle-related health and safety considerations in the county.

20.2.1.1 Mill Site

The Humboldt Mill produces a slurry of thickened tailings composed of fine-grained solids and liquid process water. Between approximately mid-May and mid-November (called “summer deposition”), the slurry is sub-aqueously deposited into the Deep Layer of the HTDF from a pipe suspended below a floating barge.

Between approximately mid-November and mid-May (“winter deposition”), the slurry is sub-aqueously deposited through a pipe on the floor of the HTDF. Both methods generate cones of tailings that rise above the surrounding tailings surface on the floor of the HTDF. Bathymetric images of the HTDF show a dimpled tailings surface, a product of cone deposition.

Under the current mine permit (MDEQ 2018), the maximum elevation of the top of tailings cones in the HTDF is limited to 1,515 feet above mean sea level (ft amsl), or 17 feet below the normal operational water surface elevation (1,532 ft amsl). Under the proposed LOM Rev. 6, tailings are deposited to an elevation of 1,515 ft amsl or less; therefore, a permit amendment related to tailings deposition elevation is optional.

This tailings deposition plan includes a voluntary management decision by Eagle that leaves a gap between the tailings and the pit wall adjacent to the cut-off wall, which slightly reduces the maximum volume of tailings that can be stored in the HTDF.

20.2.2 Monitoring

20.2.2.1 Mine Site

Eagle conducts both required compliance monitoring and voluntary monitoring at the Mine and the Mill sites. During Mine operations, Eagle is required to monitor the following under Groundwater Discharge Permit GW1810162 (EGLE 2024a):

- Influent water chemistry to the RO system in the Mine WTP (generally monthly).
- Water chemistry of effluent discharge mine contact water added at point EQ-1 prior to infiltration to the Quaternary aquifer (generally weekly).
- Use of additives containing ethylenediaminetetraacetic acid (EDTA) in the Mine WTP; this would require submission of a monitoring program specific to EDTA if the cleaning chemical is used.
- Flow rate to the TWIS (daily).
- Static water level and groundwater chemistry in nine wells upgradient of the TWIS screened in the Quaternary aquifer (quarterly).
- Water chemistry of samples collected from the TDSRA sump.

Static water level and groundwater chemistry in twelve wells downgradient of the TWIS screened in the Quaternary aquifer (quarterly).

Since 2014, Eagle has also monitored groundwater elevations from an extensive network of compliance wells surrounding the Mine site as part of the regulatory monitoring program. Sample points include: (1) surface water elevations in the wetland located above the underground mine, (2) groundwater elevations in the Quaternary glacial aquifer, and (3) groundwater levels in the upper bedrock hydrogeological unit.

Eagle adheres to fugitive dust controls and operates and maintains the required emissions control equipment under its air permit to install.

Additional voluntary monitoring at the Mine site includes:

- Water chemistry of samples collected from underground sumps and jump tanks (monthly).
- Water chemistry of samples collected from the CWBs.
- Water chemistry of samples collected from the utility well; water from this well is used for drilling, scaling, and mucking in the underground mine.
- Water elevation of the mine pool in Eagle East.

As discussed in Section 20.2, multiple exceedances of the groundwater discharge permit limits with respect to pH, arsenic, and vanadium occurred from 2023 to 2025. Eagle is actively addressing this issue with the Michigan Department of Environment, Great Lakes, and Energy (EGLE).

During closure, Eagle is required to monitor groundwater quality and water levels for 20 years. No new wells are required to be installed under the current mine permit (DNRE, 2010).

20.2.2.2 Mill Site

During Mill operations, Eagle is required to monitor the following under National Pollutant Discharge Elimination System (NPDES) permit MI0058649:

- Water chemistry and flow rate of Mill WTP effluent at monitoring point 004A, and at the Middle Branch of the Escanaba River upgradient of the discharge point (generally weekly to monthly).
- Flow rates discharged to Outfalls 001, 003, and 004 (daily).
- Total hardness in the Middle Branch of the Escanaba River (quarterly).
- Water chemistry at Outfalls 001 and 003, which discharge into the adjacent wetland (generally monthly), if effluent is being discharged to these outfalls.
- Flow rate of river water intake leading to Outfalls 001 and 003 (daily), when in operation.
- WTP intake water quality.
- Annual bathymetry mapping.

On a monthly basis, Eagle is required to monitor the groundwater potential and water quality in 24 compliance wells located around the Mill site, including inside and outside of the cut-off wall. Pairs of wells located inside and outside of the cut-off wall are used to evaluate the direction of the groundwater gradient surrounding the HTDF and any chemical changes in the surrounding aquifer (Eagle Mine, 2026a).

Eagle adheres to fugitive dust controls and operates and maintains the required emissions control equipment under its air permit to install.

Voluntary monitoring at the Mill site includes:

- Lake surface elevation (daily).
  - To maintain an inward hydraulic gradient, the surface elevation of the HTDF must remain below 1535 ft amsl. The rate of water pumped to the Mill WTP is voluntarily increased if the HTDF water surface elevation rises above 1533.4 ft amsl, as specified by a Trigger Action Response Plan (TARP).
- Groundwater potential and water quality, which are monitored in four non-regulatory wells located inside and outside the cut-off wall (monthly).
- In situ profiles of electrical conductivity and temperature in the HTDF (approximately monthly).
- Continuous in situ profiles of temperature, electrical conductivity, pH, dissolved oxygen, turbidity, oxidation-reduction potential, fluorescent dissolved organic carbon (a proxy for total organic carbon), chlorophyll *a*, and blue green algae in the HTDF (four profiles per day; May to November).
- Vertical profile of the water chemistry of the HTDF (eight to ten depths, annually in July).
- Process water chemistry from the tailings thickener tank.
- Off-specification water chemistry from the Mill WTP and ZLD.
- RO brine.

- Mercury in rainwater (annually).
- Continuous bathymetric imaging in the HTDF using sonar.

There have been no incidents of the HTDF water elevation exceeding 1535 ft amsl since mid-2020, such that no groundwater discharge could have occurred since that time. No impacts to the inward hydraulic gradient or groundwater quality outside the cut-off wall were reported.

On a quarterly basis, Eagle submits Benchmark Deviation reports to EGLE for the Mill site, comparing observed groundwater chemistry in regulated wells at the Mill site to benchmark values established in 2018 (Eagle Mine, 2026a). Variations in the following parameters are observed and attributed to natural changes in groundwater quality: manganese, pH, mercury, calcium, nickel, and zinc. The application of road salt causes deviations in sodium, chloride, and nitrate in some wells. Importantly, the observed concentrations of sulfate, the dominant anion in HTDF water, are consistently an order-of-magnitude lower in wells outside the cut-off wall than in the HTDF, providing evidence that water in the HTDF is not influencing groundwater outside the cut-off wall.

No reportable exceedances of the surface water discharge permit limits occurred between 2023 and 2025. Minor and infrequent releases of untreated or reclaim water to soil occurred between 2023 and 2025. These events were promptly reported to regulators, contained, and remediated in accordance with site procedures, including excavation and disposal of affected materials where required. No lasting environmental impacts were identified, and these events are not considered material to Project operations.

During closure, Eagle is required to monitor surface water quality, groundwater levels, and groundwater quality in the permitted groundwater well network for 20 years after operations.

20.2.3 Water Management

20.2.3.1 Mine Site

Eagle has completed mining in the deepest level of Eagle East at -542 amsl. As of September 2022, water had accumulated in the lowest portion of Eagle East, inundating the deepest workings. This water is primarily utility water (used for drilling and mucking and scaling ore) combined with groundwater draining downward to the lowest point in the mine. It is expected that Eagle East will not be pumped dry during the remaining operations, and the water elevation will generally remain the same or possibly higher as mining activities retreat to higher elevations.

During operations, two CWBs store water at the Mine site prior to treatment in the Mine WTP. Major inputs to the CWBs include site stormwater and snowmelt, direct rainwater, water pumped from sumps and jump tanks in the underground mine, seepage from the TDRSA, and sump water from the COSA and Truck Wash.

Water is pumped from the CWBs into the Mine WTP. Water passes through a clarifier, multi-media filters, and an ion exchange system before passing through an RO system, followed by an evaporator/crystallizer system. Several times a month, solids from the crystallizer are shipped to the Delta County Landfill in Escanaba, Michigan. Permeate from the RO system is returned to the Quaternary glacial aquifer via the TWIS. When needed, excess RO brine is returned to one of the CWBs for storage prior to treatment. Groundwater quality downgradient of the TWIS is routinely monitored by Eagle (see Section 20.3).

During closure, water will be pumped directly into the underground mine. Under the previous LOM, the time to flood the underground mine was estimated as less than 5 years. If needed, after flooding, the Mine WTP will be used to treat and recirculate treated water to the top of the mine pool. Current closure evaluations indicate that this will likely not be necessary due to the downward hydraulic gradient within the mine pool.

20.2.3.2 Mill Site

During operations, the Mill WTP serves two major roles: maintaining an inward hydraulic gradient to the HTDF by maintaining an operational water level near 1532 ft amsl and treating HTDF water prior to discharge. Liquid inflows to the HTDF include tailings process water, pit wall runoff, direct precipitation, groundwater, RO brine from the Mill WTP, and off-specification water from the Mill WTP.

The Mill WTP removes water from two depths in the HTDF: the Surface Layer via the Shallow WTP intake and the Deep Layer via the Deep WTP intake. From February 2023 until September 2024, water from the Deep WTP intake was first processed using a plug flow reactor (PFR) to remove thiosalts (expressed as total S2O3) using a Fenton's reaction (i.e., lower pH, add iron chloride) before flowing to a coagulation tank. After September 2024, Deep WTP intake water was sent directly to the coagulation tank. Filter cake from the coagulation tank is shipped to the Marquette County Solid Waste Management landfill for permanent disposal. Water from the coagulation tank passes through a clarifier and ultra-filtration (UF) circuit.

Filtrate from the UF passes through an RO system to produce permeate and brine. RO permeate is blended with water from the HTDF's Surface Layer (from the Shallow WTP intake) prior to being discharged from Outfall 004 to the Middle Branch of the Escanaba River (Latitude 46.49817, Longitude -87.88468), the point of environmental compliance for the Mill site (see Section 20.3.1).

Prior to 2025, RO brine was returned to the bottom of the HTDF, which resulted in the formation of a Brine Layer and a Pycnocline, or transitional boundary between the Deep Layer and the Brine Layer. In February 2025, Eagle commissioned a ZLD plant that removes salt from the RO brine. Salts are shipped to the Ridgeview Landfill in Whitelaw, Wisconsin, on a weekly basis. Deposition of tailings into the Brine Layer in mid-2025 caused the Brine Layer, Pycnocline, and Deep Layer to mix, such that only a Deep Layer was observed during monitoring in November 2025 and February 2026.

During operations, Eagle diverts water from the Middle Branch of the Escanaba River and uses this water to irrigate the wetland adjacent to the HTDF. During closure, passive flow between the HTDF and the wetland will be restored, and irrigation will be discontinued.

During closure, the addition of tailings to the HTDF will cease. The Mill WTP will continue to operate until the Surface Layer water quality in the HTDF meets the discharge water quality standards in the active NPDES permit for Outfall 003 (i.e., discharge from the HTDF to the adjacent wetland) that is in place at the time. The current NPDES permit (EGLE, 2022a) specifies a TDS concentration limit of 500 mg/L at Outfall 003. It is estimated that a period on the order of four to seven years may be required to complete reclamation of the facility.

After water quality compliance has been achieved, the Mill WTP will be decommissioned, the water level in the HTDF will rise to 1536 ft amsl, and water from the Surface Layer of the HTDF will discharge through an engineered spillway to the adjacent wetland, and ultimately to the Middle Branch of the Escanaba River.

20.3 Permits and Reclamation Bonds

20.3.1 Permits

Activities at the Mine site and the Mill site are permitted under Michigan's Part 632 Nonferrous Metallic Mining law. EGLE, formerly known as the Michigan Department of Environmental Quality (MDEQ), oversees the environmental regulation of the operations. Table 20.1 lists permits currently held by Eagle as required for Eagle Mine operations, Humboldt Mill operations, and water discharge at both sites. Discussion on current and future permit applications is provided below.

Table 20.1: Permits Held by Eagle Pertaining to Mining, Milling, and Water Discharge

Location	Title	Reference	Description
Mine	Part 632, Nonferrous Metallic Mineral Mining Permit for the Eagle Project, MP 01 2007	MDEQ 2007	Eagle Mine, underground mine permit, with amendments
	Groundwater Discharge Permit GW1810162	EGLE 2024a	Mine WTP effluent to TWIS and downgradient groundwater quality
	Permit to Install 50-06D v 2.0	EGLE 2025	Air quality for the Mine site
	Septage Groundwater Discharge Permit GW1110907	EGLE 2022b	Mine septic groundwater discharge permit
	Underground Injection Control Class V Authorization by Rule for Paste Backfill Well	EPA 2025	Requirements for Class V well for paste injection
Mill	Part 632, Nonferrous Metallic Mineral Mining Permit for the Humboldt Mill Project, MP 01 2010.	DNRE 2010	Humboldt Mill operations, with amendments
	Humboldt Mill Mining Permit Application Amendment Request Final Decision – MP 01 2010	MDEQ 2018	Maximum tailings elevation in HTDF raised to 1,515 ft amsl
	NPDES Permit MI0058649, inclusive of stormwater management	EGLE 2022a	Operational discharge water quality from Mill WTP to the Middle Branch of the Escanaba River
	Permit to Install 405-08C	EGLE 2024b	Air quality for the Mill site

Two permit applications were under review at the time of writing. Pending applications include the following:

1) Renewal of NPDES Permit MI0058649 for the Mill (EGLE 2022a). EGLE requires a five-year renewal cycle for this permit. Eagle applied for renewal in April 2025. No permittee-requested changes were included in the application. The timeframe for processing is typically within two years. The existing permit (EGLE, 2022a) will remain in effect until a new permit is issued.
2) A revision to Groundwater Discharge Permit GW1810162 for the Mine (EGLE, 2024a) was requested to administratively correct arsenic and pH limits set in a 2024-issued version of the permit, and to relocate the point of compliance for two wells as discussed further below. From 2023 to 2025, a limited number of

exceedances of groundwater discharge permit parameters (pH, arsenic, and vanadium) occurred. These exceedances have been evaluated in coordination with EGLE and are attributed to permit limit revisions and site-specific geochemical interactions rather than changes in operational performance. Eagle has implemented, or is in the process of implementing, appropriate corrective actions, including permit revisions where warranted. Details include:

- Vanadium concentrations exceeded the limit in monitoring wells QAL075A and QAL051D. Concentrations did not exceed the drinking water limit. There was no vanadium measured in Mine WTP effluent reporting to the TWIS. The detection of vanadium in wells is attributed to the interaction of oxygen-enriched treated water with vanadium in soil at the TWIS.
- Arsenic concentrations exceeded the limit in monitoring well QAL051D beginning in Q3 2024, coincident with permit reissuance. Exceedances were attributed to a typographical error in limits established in the new groundwater discharge permit issued in July 2024 (EGLE, 2024a). The previous permit limit was 6 µg/L, and the new limit is 5 µg/L. Reported values did not exceed drinking water standards.
- Maximum pH levels exceeded the limit in monitoring well QAL008A beginning in Q3 2024, coincident with permit reissuance. Exceedances were attributed to a typographical error in limits established in the new groundwater discharge permit issued in July 2024 (EGLE, 2024a). The previous permit limit was pH 9.7, and the new limit is pH 9.0.

Eagle reported these exceedances to EGLE, who ultimately directed Eagle to apply for a revised groundwater discharge permit. Eagle submitted the application on January 20, 2026 (Eagle Mine, 2026b). The application requests the following modifications to Groundwater Discharge Permit GW1810162:

- Correct errors in arsenic and pH limits.
- Relocate the point of compliance for vanadium to a newly established well.
- Review background water quality conditions for arsenic and reconsider the site-specific limit.
- Correct miscellaneous typographical errors.

The timeframe for review has not been specified. The existing permit (EGLE, 2024a) will remain in effect until a new permit is issued.

In addition, prior to closure, a revision to the surface water/stormwater discharge limit for mercury at Outfall 003 will likely be needed. Rainwater in the Great Lakes region has contained concentrations of total mercury ranging from 10 to 60 ng/L (Hall et al., 2005). The mercury limit at closure at Outfall 003 is 1.3 ng/L. A portion of the post-closure water balance for the HTDF will be composed of rainwater and pit wall runoff, which is derived from rainwater. Consequently, mercury in the Surface Layer of the HTDF may exceed discharge limits for mercury at closure as a product of direct rainfall landing within the HTDF catchment area and not through processes related to tailings disposal or milling activities.

EGLE is aware of this issue but has stated that it cannot address it until transferring the NPDES surface discharge permit to a stormwater-only permit in the future. To prepare for this, Eagle voluntarily monitors mercury in rainwater at the Mill site on an annual basis.

20.3.2 Reclamation Bonds

Eagle is required to post reclamation bonds (i.e., financial assurances) for closure activities at both the Mine site and the Mill site (EGLE, 2026) and to maintain these until all reclamation has been completed and approved by EGLE. It has maintained these bonds for both sites. Financial assurances are recalculated at least every three years based on revisions to the reclamation plan and post-closure monitoring period since the previous update (Rule 425.308).

Bond values and required closure activities are discussed in Section 20.5.

20.4 Social and Community Requirements

Eagle has no potential social or community requirements for operation or closure. There are no current negotiations or agreements with local communities. The Project operates within an established regulatory and community framework in Michigan and does not require formal social or community agreements as a condition of operation or closure.

A key social consideration for the Project is engagement with Indigenous communities, including the Keweenaw Bay Indian Community (KBIC). The Keweenaw Bay Indian Community (KBIC) has identified Eagle Rock, located at the Mine site, as a culturally significant site. This was a consideration during permitting. KBIC retains access to Eagle Rock during operations, and access is expected to continue following closure in accordance with State land management practices.

Eagle maintains ongoing engagement with local communities and stakeholders through established communication channels, including public information sessions and an information center. Community feedback mechanisms and periodic surveys are used to monitor community perspectives over time.

Certain localized concerns have been identified and managed through standard engagement practices and grievance procedures.

Two community relations issues relate to the Mill site: (1) During an extreme rainfall event, the potential exists for water to overtop the perimeter of the HTDF and inundate (on the order of several inches) State Highway 41 north of the HTDF. Although an event of this magnitude is very unlikely, Eagle has briefed Marquette County emergency response officials of this potential. (2) Odor complaints from the community were lodged at the Mill site between July and November 2025. Though they can be sensed by humans, the concentrations of gases causing these odors (most likely carbon di-sulfide and carbonyl sulfide) are lower than laboratory detection levels in the ambient environment. Gases need to be concentrated using specialized sampling equipment in enclosed spaces to be measurable. Therefore, monitoring of odor issues is made using olfactory observations by Mill staff.

To build community trust and confidence, Eagle operates an Information Center in Marquette and hosts spring and fall community forums to engage the local community. These forums provide a two-way dialogue with the community, provide updates on operations, and introduce attendees to members of the Eagle team.

Eagle Mine has made several investments in the local community intended to generate a local economy outside of mining that will continue to be an economic driver after the end of operations. The Lundin Foundation, Eagle Mine, and Northern Initiatives have partnered to create a program to benefit area entrepreneurs called the Eagle Emerging Entrepreneurs Fund (EEEF). Launched in 2013, EEEF provides loans and technical assistance to micro and small enterprises in Marquette County and has disbursed $2.9 million across 68 loans since its implementation, mainly to support local business development. EEEP is managed by Northern Initiatives, which is responsible for assessing and approving loans. At the time of writing, EEEP is still active with no expiration date. Eagle no longer actively manages the fund nor contributes to it, as it is self-supporting.

Eagle partners with Accelerate UP, an incubator for small businesses in Marquette County. Accelerate UP was founded in 2014 and offers business coaching to small business owners to develop start-up ventures, expand, or diversify. This initiative has mobilized $18.7 million in capital investment since its founding, focusing on 134 businesses. Accelerate UP expires in December 2029 with an option to renew based on LOM and program impact.

Eagle supports Marquette Alger Technical Middle College (MATMC). MATMC enables students from Marquette and Alger counties to earn a high school diploma, a significant number of college credits, and a Technical Certificate from Northern Michigan University at no cost. The goal of the program is to increase technical skills in demand in Marquette County and create jobs for local people. Annual funding is tied to the LOM with an annual percentage ($50,000) held with the Community Foundation of Marquette County to help fund the program after mining operations cease.

Finally, Eagle supports the Community Environmental Monitoring Program (CEMP), which provides transparency on environmental impacts. The CEMP is composed of three local groups:

- KBIC (described above).
- The Superior Watershed Partnership (SWP) is a local non-profit organization serving the Upper Peninsula of Michigan.
- The Community Foundation of Marquette County (CFMC) is a local non-profit that helps people invest in the future of Marquette County.

Through the CEMP, the SWP, and KBIC monitor Eagle's environmental performance and report back to the community. CFMC provides financial oversight of these funds. CEMP is set to expire in December 2027 with an option to renew. The intent is for CEMP to run through the LOM.

Eagle conducts a Social License to Operate (SLO) survey every six months, which is issued by Voconiq Local Voices (2025). The survey is used to monitor perceptions of trust, legitimacy, and acceptance between Eagle Mine and the community over time. Eagle Mine also conducts Human Rights Risk and Impact Assessments every five years to identify salient risks and inform mitigation measures across operational activities and stakeholder interactions.

20.5 Mine Closure

20.5.1 Mine Site

Requirements for closure of the Eagle Mine are provided in the Eagle Project Permit (MDEQ 2007, with amendments). A closure and reclamation implementation plan is described in an internal memorandum by Eagle Mine (2026c). Eagle's Surface Use Lease with the State of Michigan Department of Natural Resources requires that marketable timber be replanted to support the State's land commercial forest program. Following closure and reclamation activities, the Mine site will be returned to the State of Michigan commercial forest land program as it was prior to Eagle's occupancy.

Reclamation of the property will consist of flooding the underground mine workings and reclaiming approximately 131 acres of surface area to a condition corresponding to the pre-mining landscape using native vegetation commensurate with the pre-mining landscape or an alternative type or types of vegetation resulting from the stakeholder consultation process. The reclamation phase is expected to take from 2 to 3 years (not including removal and reclamation of the Mine WTP to be performed after the mine is flooded, assuming the WTP is not needed at that time). The underground approach will begin at the -540 m asl level in Eagle East, progress upwards into the Eagle ore body, and be completed at the mine portal. Inert materials (concrete, asphalt, etc.) may be placed underground.

Water will be pumped into the underground workings using water from the utility well screened in the Quaternary aquifer. Under the previous LOM, the flooding of underground workings was estimated to take 4.5 years. A leak-proof plug will be placed at the mine portal. Vertical connections with the surface must be plugged per the reclamation plan.

The closure timeline for the Mine would proceed as follows:

- Year -1 (one year before the end of operations):
  - Place TDRSA waste rock underground.

Years 1 to 3:

- Underground:
  - Remove ore haul trucks.
  - Remove equipment and utilities.
  - Close ventilations systems.
  - Close the underground mine and mine portal.
  - Install necessary plugs.
  - Begin to flood the mine.
- Surface:
  - Close the TDRSA.
  - Demolish and remove buildings.
  - Reclaim the surface water management system.
  - Maintain the CWBs and Mine WTP under contingency status.
  - Close roads.
  - Remove utilities and infrastructure.
  - Regrade and revegetate the site.
  - Install erosion control measures.
  - Remove fuels, chemicals, explosives, etc.
  - Maintain site safety and security. Years 4 to 29:

- Complete underground flooding.
- Conduct monitoring.
- Conduct maintenance.
- Evaluate contingency measures.
- Remove the Mine WTP.
- Abandon monitoring wells.

Groundwater quality and water level monitoring is required for 20 years after the mine pool reaches steady-state conditions.

The Geologic Resources Management Division of EGLE has determined that the 2025 financial assurance cost estimate met the requirements of R 425.301 and set the total financial assurance to a minimum of $39,158,626 applied to Eagle Mine. Eagle will provide the next financial assurance update no later than December 31, 2028 (EGLE, 2026).

20.5.2 Mill Site

Requirements for closure of the Mill Site are provided in the Humboldt Mill Project Permit (DNRE 2010, with amendments), with modifications described by EGLE (2026). Ramboll (2021) provided a Draft Closure Plan for the Humboldt Mill written prior to considerations by EGLE (2026). At the conclusion of operations, Eagle is required to reclaim the Humboldt Mill project site to establish a self-sustaining ecosystem. The final land use of the site will be compatible with existing uses on adjacent properties (DNRE, 2010).

A summary of required closure activities at the Mill includes the following:

- Eagle will reclaim and decommission select buildings located at the Humboldt Mill in preparation for future sale of the property and industrial reuse, except for the Mill itself; buildings and infrastructure located within the Mill area will not be demolished (EGLE, 2026). Leaving buildings in place in the Mill area for future use is consistent with the approved reclamation plan, local zoning classification, and historic land use and is allowed under Part 632 administrative rules in accordance with proposed final land use (EGLE, 2026).
- HTDF water will be treated using the Mill WTP until water quality meets Outfall 003 discharge permit conditions applicable at the time of rehabilitation. Thereafter, the Mill WTP, ZLD plant, and related structures and infrastructure (e.g., roads) will be removed.
- An outlet (passive spillway) from the HTDF will be constructed at 1536 ft amsl, connecting the HTDF to the adjacent wetland at Outfall 003.
- The water level in the HTDF will be allowed to rise and discharge to the wetland via the passive spillway at 1536 ft amsl. Outflow from the HTDF will provide irrigation to the wetland.
- Surface and groundwater quality in regulated wells and water levels in regulated wells will be monitored for 20 years.

The Geologic Resources Management Division of EGLE has determined that the 2025 financial assurance cost estimate met the requirements of R 425.301 and has set the total financial assurance to a minimum of $16,076,480 for the Humboldt Mill. Eagle will provide the next financial assurance update no later than December 31, 2028 (EGLE, 2026).

21. Capital and Operating Costs

All capital and operating costs are expressed in United States dollars ($). Costs were estimated by Eagle Mine personnel and reviewed. The model reviewed in detail was *Eagle_LOM_financial_model_2026_v6_current.xlsm.* Minor updates were made to *Eagle_LOM_financial_model_2026_v9.xlsm* which was used for final reporting. Costs were compared to the 2025 actuals provided by Eagle Mine personnel.

21.1 Capital

Currently, there are no expansion plans requiring project capital expenditures in the LOM Plan.

21.1.1 Sustaining Capital

The Eagle Mine is in operation. It requires sustaining capital of $69.9 million for continuing underground mine development, mill, and other expenditures from 2026 to 2028.

Sustaining capital cost estimates have been developed from mine experience with underground mine development over the past number of years. The unit cost of all lateral development varies depending upon the size of the headings being excavated and is, on average, $3,782/m over the LOM (materials only). The majority of capital expenditures will be complete by 2028.

Table 21.1 summarizes the capital expenditures planned for the balance of the mine life. The short remaining LOM does not necessitate significant new equipment purchases. The paste plant is scheduled to be completed by 2028.

Underground development cost is directly correlated with development meters with unit rates for lateral and vertical development applied to the number of meters of mine development required in each year. Mine development is scheduled to be substantially complete by 2028, with only 194 m of development in 2029-2030.

Table 21.1: LOM Sustaining Capital, $M

Item	Unit	2026*	2027	2028	2029	2030	Total
Mine Development Meters							
Vertical							
Drop Raise	m	81	154	210	-	-	445
Raisebore Ventilation	m	152	109	211	-	-	471
Raisebore with Escapeway	m	178	90	86	-	-	354
Paste Boreholes	**m**	-	416	610	-	-	1,026
Total Vertical	**m**	**412**	**769**	**1,116**	**-**	**-**	**2,297**
Lateral							
Eagle	m	0	0	0	0	20	20
Eagle East	m	484	487	219	78	14	1,281
Keel	m	2,071	2,754	2,828	40	32	7,724
Total Lateral	**m**	2,555	3,241	3,046	118	66	**9,026**
Waste Tonnes	t	230,568	297,718	272,399	15,810	12,596	829,091
Expenditures, $M							
Underground Development	$M	12.2	13.8	13.9	-	-	39.9
Mine Other	$M	2.9	3.5	3.5	-	-	9.9
Mill	$M	1.0	1.2	1.2	-	-	3.4
Other	$M	0.5	0.6	0.6	-	-	1.7
Paste Plant	$M	5.0	10.0	0	-	-	15.0
Total Sustaining Capital, $M	**$M**	**21.7**	**29.1**	**19.1**	**-**	**-**	**69.9**

Note: Columns and rows may not sum precisely due to rounding.

21.1.2 Mine Closure

In addition to the Sustaining Capital, the mine plan includes $78.0 million in expenditures for closure activities, to be initiated in 2029. These costs are funded through the existing ARO.

21.2 Operating Costs

Site operating cost estimates were developed based on recent actual costs with specific adjustments for business improvement initiatives underway. They were prepared on an annual basis using a detailed build-up of individual cost centers and considering specific mine site activity levels and cost drivers. The estimates consider current and expected labor headcount and salaries, major consumables and unit prices, power costs based on the recently established renewables contract, and equipment and maintenance costs. The total operating cost estimate includes all site costs related to mining, processing, and general and administrative activities, as well as regional office costs. The total operating cost excludes costs beyond the mill, such as concentrate transportation costs, smelter and refining charges, royalties, and severance taxes.

Processing costs include expected direct costs for ore processing, including crushing and conveying, grinding, flotation, tailings thickening and deposition, nickel concentrate preparation, and copper concentrate preparation prior to shipping. General and administrative costs relate to costs associated with indirect support of the operation, including G&A personnel and functions, administrative facilities, site services, and other support costs.

Detailed first-principles cost build-ups have not been reviewed by the QP. As an operating mine, using actual costs is considered reasonable. Adjustments have been made to include factors such as recent salary increases, paste plant operations, and decreases in certain mine activities. Operating expenses at Eagle are found to be reasonable for a mechanized mine utilizing the longhole and cut-and-fill mining methods. The following tables summarize operating costs, segmenting by major cost centers - the Mine, the Processing Plant, and General and Administrative.

Table 21.3 summarizes the total expected operating expense to mine and process the 3.5 million tonnes of ore included in the production plan.

Table 21.2: Projected Operating Costs

Cost Center	LOM Cost, $M Total	Unit Cost, $/t Average
Mining	245.5	70.29
Ore Transport to Mill	48.7	13.96
Plant	134.3	38.50
G&A	74.0	21.20
Total Operating Costs	**502.1**	**144.00**

Table 21.4 shows the operating costs by year as compared to the production plan by mining area.

Table 21.3: Projected Operating Costs by Year

Item		2026*	2027	2028	2029	2030	Totals
Annual Ore Tonnes by Mining Area							
Eagle	t	-	-	-	-	40,532	40,532
Eagle East	t	509,487	329,675	136,394	179,759	-	1,155,315
Keel	t	118,982	457,720	650,204	607,520	456,207	2,290,633
Total Ore Tonnes	**t**	**628,469**	**787,396**	**786,598**	**787,279**	**496,739**	**3,486,481**
Cost Centre							
Mining	$M	49.9	61.6	55.4	47.0	31.0	245.1
Ore Transport to Mill	$M	8.6	10.8	11.1	11.2	7.1	48.7
Plant	$M	26.4	29.5	29.2	29.6	19.6	134.3
G&A	$M	17.3	18.2	14.4	14.4	9.6	74.0
Total Operating Costs	**$M**	**102.2**	**120.2**	**110.1**	**102.2**	**67.3**	**502.1**
Unit Operating Cost	**$/t**	163	153	140	130	135	144

Note: 2026 excludes January-February actuals

21.2.1 Mine

Mine operating costs include direct costs of the mining process. Mine operating costs were developed individually by work type and activity based upon applying unit costs and work measures for estimation of the costs of activities and consumables such as ground support, subcontractor labor and other, maintenance, Owner's labor, explosives, drill bits, power, diesel, propane, backfill, water treatment, and Other Costs for each of the excavations defined in the Mine Plan. For estimation purposes, costs are built up for primary stopes, secondary stopes, 5 m production sills, 6 m production sills, 10 m production sills, slashes, and drift-and-fill mining methods. The resulting activity cost estimates then provide a total cost for the production tonnages extracted for each year. Service and overhead costs decline over the plan in line with production activities.

While maintenance costs are linked to equipment operating hours, diesel fuel costs are linked to ore production, segmented by mining area. The diesel usage factor for the Keel, which matches that of the Eagle, is based on ore tonnage from that area. It is noted that the Eagle East diesel factor is twice that of the Eagle.

While consumables for capital development have been reported in the capital estimate, for simplicity, labor and maintenance related to capital development are not reclassified and remain an operating expense. This does not impact the all-in sustaining cost of the operation or the Mineral Reserves estimate.

Operating costs of the underground mine are estimated to be $245.5 million over the LOM or average $70.29/t of ore, as itemized in Table 21.5.

Table 21.4: Mine Operating Cost Projection

Activity Related	LOM Cost, $M Total	Unit Cost, $/t Average
Mining Consumables	37.4	10.73
Mine Operations	58.7	16.85
Energy	24.7	7.07
Maintenance	102.1	29.29
Overhead and Services	22.2	6.36
Total Mine Opex	**245.1**	**70.29**

No provision has yet been included for the increased geotechnical risk indicated in Chapter 16. Labor decreases for 2029 with the completion of capital development.

21.2.2 Processing Plant

The annual and unit processing costs for the Humboldt Mill are part of the general operating costs. The mill operating costs are based on the production results at Humboldt operations and are in line with mill operating costs in the industry for similar projects. The processing of Keel mineralized material is not expected to deviate from established operating costs.

Operating costs of the processing plant are estimated to be $134.3 million over the LOM, an average of $38.51/t, with major cost elements provided in Table 21.6.

Table 21.5: Processing Plant Operating Cost Projection

Cost Center	LOM Cost ($M)	Unit Cost ($/t)
Reagents / Grinding / Chemicals	14.5	4.16
Maintenance	25.5	7.31
Power	16.5	4.73
Contract Services	18.3	5.25
Salaries	57.9	16.60
Other Mill	1.6	0.46
Total Mill Opex	**134.3**	**38.51**

21.2.3 General and Administrative, Ore Transportation

Current G&A costs, along with current Ore Transportation costs, have been carried forward for the LOM based on current costs. G&A is above the NSR baseline of $19.00 $/t for 2026 and 2027, with 2028 and 2029 in line with previous targets. The final year of the LOM is a partial year of five months duration, resulting in a cost of $9.6 million. G&A over the LOM totals $74.0 million, equating to an average over the LOM of $21.20/t processed.

Ore transportation from the mine to the mill averages $13.96 /t over the LOM, providing a total operating expense estimate of $48.7 million for the remaining LOM.

22. Economic Analysis

22.1 Economic Analysis

This section presents the key financial indicators derived from the discounted cash flow model supporting the Technical Report for the remaining life of mine of Eagle Mine. The analysis has been prepared on an annual basis, with the NPV calculated as of March 1, 2026. The cash flows and NPV exclude the residual value of the mill, salvage value of equipment and release of working capital at the end of operations.

The economic evaluation reflects a steady-state operating scenario based on the current mine plan from March 2026 to the second half of 2030, incorporating forecast production, operating costs, sustaining capital requirements, and analyst consensus metal price estimates as of December 2025.

Production, operating costs and sustaining capital requirements were covered in previous chapters in this technical report.

22.2 Exchange Rates

All dollar amounts are in US dollars; therefore, no exchange rate is required. All results are expressed in US dollars.

22.3 Metal Prices

Metal prices used were as follows, as shown in Table 22.1.

Table 22.1: Assumed Metal Prices Based on Analyst Consensus Estimates as of December 2025

		2026	2027	2028	2029	2030
Nickel	$/lb	7.50	7.70	8.15	8.15	8.15
Copper	$/lb	5.50	5.00	4.95	4.95	4.95
Cobalt	$/lb	19.00	20.00	20.00	20.00	20.00
Platinum	$/oz	1,500	1,500	1,500	1,500	1,500
Palladium	$/oz	1,245	1,205	1,205	1,205	1,205
Gold	$/oz	4,200	3,825	3,825	3,825	3,825
Silver	$/oz	50.25	44.50	44.50	44.50	44.50

22.4 Summary of Results

The financial model indicates that Eagle Mine generates a positive economic outcome over its remaining mine life. At analyst consensus prices, the project yields an after-tax NPV 8% of $19.0 million, demonstrating positive value generation from the remaining reserves.

Internal rate of return and payback calculations are not applicable and do not compute since this is an operating mine and does not have an initial capital investment. The model indicates average annual operating cash flow over the 2026-2030 operational period of $33.0 million, highlighting continued operating margin generation despite declining ore grades.

The key financial and operating metrics of Eagle Mine's remaining mine life are summarized in Table 22.2.

Table 22.2: Key Financial and Operating Metrics of Eagle Mine's Remaining Mine Life

Financial Metrics		
After-tax NPV 8%	$ millions	$19.0 million
IRR	%	Not applicable[6]
Payback	Yr.	Not applicable[1]
Operating Metrics		
Mine life	Years	March 2026 to H2 2030 (approx. 4.4 years)
Total tonnes processed	Tonnes	3,486,481
Average annual throughput	Tonnes per annum	787,000
Daily throughput	Tonnes per day	2,156
Cash cost[7] (LOM)	$/lb of payable Ni Net of credits	$5.13
All-in sustaining cost[8] (2026-2030 operational period)	$/lb of payable Ni Net of credits	$6.55
All-in sustaining cost[9] (LOM)	$/lb of payable Ni Net of credits	$8.05
Revenue breakdown	% of gross revenue	Nickel – 57% Copper – 37% Other[10] – 6%

22.5 Financial Model Assumptions

22.5.1 Valuation

All inputs are real 2026 US dollars discounted at real rates of return of 8% to determine the after tax NPV. Cash flows have been discounted to March 1, 2026.

22.5.2 Metal Prices

Metal prices were based on analyst consensus estimates as of December 2025 as detailed above.

[6] IRR and payback calculations are not applicable and do not compute since this is an operating mine and does not have an initial capital investment.
[7] Cash cost includes mining, transportation, processing, G&A costs, royalties and treatment/refining costs offset by by-product credits from metals other than nickel
[8] All-in sustaining cost ("AISC") includes cash cost, sustaining CAPEX, royalty buy-down, exploration and closure costs during operating period.
[9] All-in sustaining cost ("AISC") – LOM includes closure costs after operating period in addition to AISC.
[10] Other includes cobalt, platinum, palladium, gold and silver. Total may not add up to 100% due to rounding.

22.5.3 Royalties

Private royalties for both the Eagle East and Keel deposits are included in the economic analysis along with a $2 million royalty buy-down payment.

22.5.4 Income Taxes

Income taxes include only federal taxes as state taxes are covered by the severance tax royalty. Given that Eagle Mine is an operating mine; in calculating income tax, the financial model included forecast tax depreciation and the usage of net operating losses.

A severance tax royalty was also included which is in lieu of state taxes and paid to the State of Michigan at a rate of 2.75% of revenue.

No tax deductions were assumed in connection with the closure costs. Should there be positive taxable income from Eagle or related companies or assets in the future, this would likely reduce the after-tax cost of the closure costs.

22.5.5 Working Capital

Because this is an operating mine, capital has already been sunk into working capital and so no incremental investment in working capital was required. Release of working capital (a positive cash flow) at the end of production in 2030 was not included in the cash flows.

22.6 Annual Production Schedule and Cash Flow Forecast

The Eagle Mine cash flow forecast is shown in Table 22.3.

Table 22.3: Eagle Mine Cash Flow Forecast

	Operational Period	Closure Period	Total Life of Mine	Operational Period					Closure Period
	Mar 2026-2030	2031-2055	Mar 2026-2055	Mar-Dec 2026	2027	2028	2029	2030	2031-2055
Ore Tonnes Mined	3,486,481	-	3,486,481	628,469	787,396	786,598	787,279	496,739	-
Ore Tonnes Milled	3,486,481	-	3,486,481	628,469	787,396	786,598	787,279	496,739	-
Ni Head Grade	1.06%	-	1.06%	1.46%	0.97%	1.01%	0.97%	0.95%	-
Cu Head Grade	0.82%	-	0.82%	1.20%	0.76%	0.74%	0.73%	0.72%	-
Ni Recovery	79.8%	-	79.76%	82.7%	78.7%	78.9%	78.6%	79.1%	-
Cu Recovery to Cu con	76.8%	-	76.76%	78.7%	77.1%	75.4%	75.8%	75.9%	-
Cu Recovery to Ni con	17.5%	-	17.48%	17.0%	16.8%	18.2%	17.8%	17.8%	-
Gross Revenues	**720,454**	**-**	**720,454**	**189,348**	**145,068**	**150,150**	**145,224**	**90,664**	**-**
Treatment Charges	(3,782)	-	(3,782)	(1,032)	(818)	(752)	(752)	(428)	-
Royalty	(22,536)	-	(22,536)	(10,414)	(5,232)	(3,644)	(1,781)	(1,465)	-
Severance Tax Royalty	(19,552)	-	(19,552)	(5,138)	(3,934)	(4,077)	(3,941)	(2,462)	-
Net smelter return	**674,584**	**-**	**674,584**	**172,764**	**135,083**	**141,677**	**138,751**	**86,309**	**-**
Mine	(245,072)	-	(245,072)	(49,944)	(61,648)	(55,440)	(47,038)	(31,003)	-
Transportation cost	(77,773)	-	(77,773)	(15,941)	(16,714)	(17,120)	(17,157)	(10,842)	-
Plant	(134,277)	-	(134,277)	(26,383)	(29,510)	(29,193)	(29,606)	(19,585)	-
G&A	(74,026)	-	(74,026)	(17,309)	(18,248)	(14,426)	(14,426)	(9,617)	-
Exploration Cost	(64)	-	(64)	(64)	-	-	-	-	-
Operating cash flow	**143,371**	**-**	**143,371**	**63,124**	**8,963**	**25,499**	**30,523**	**15,261**	**-**
Sustaining Capex	(69,915)	-	(69,915)	(21,656)	(29,089)	(19,170)	-	-	-
Royalty buy-down payment	(2,000)	-	(2,000)	(2,000)	-	-	-	-	-
Terminal value of Humboldt mill	-	-	-	-	-	-	-	-	-
Closure cost	(1,735)	(78,051)	(79,787)	-	-	-	(108)	(1,628)	(78,051)
Income tax	-	-	-	-	-	-	-	-	-
After-tax cash flow	**69,720**	**(78,051)**	**(8,331)**	**39,468**	**(20,126)**	**6,329**	**30,416**	**13,634**	**(78,051)**

22.7 Cash Flow Profile

Figure 22.1 illustrates the cash flow profile of Eagle Mine using the Financial Model Assumptions above.

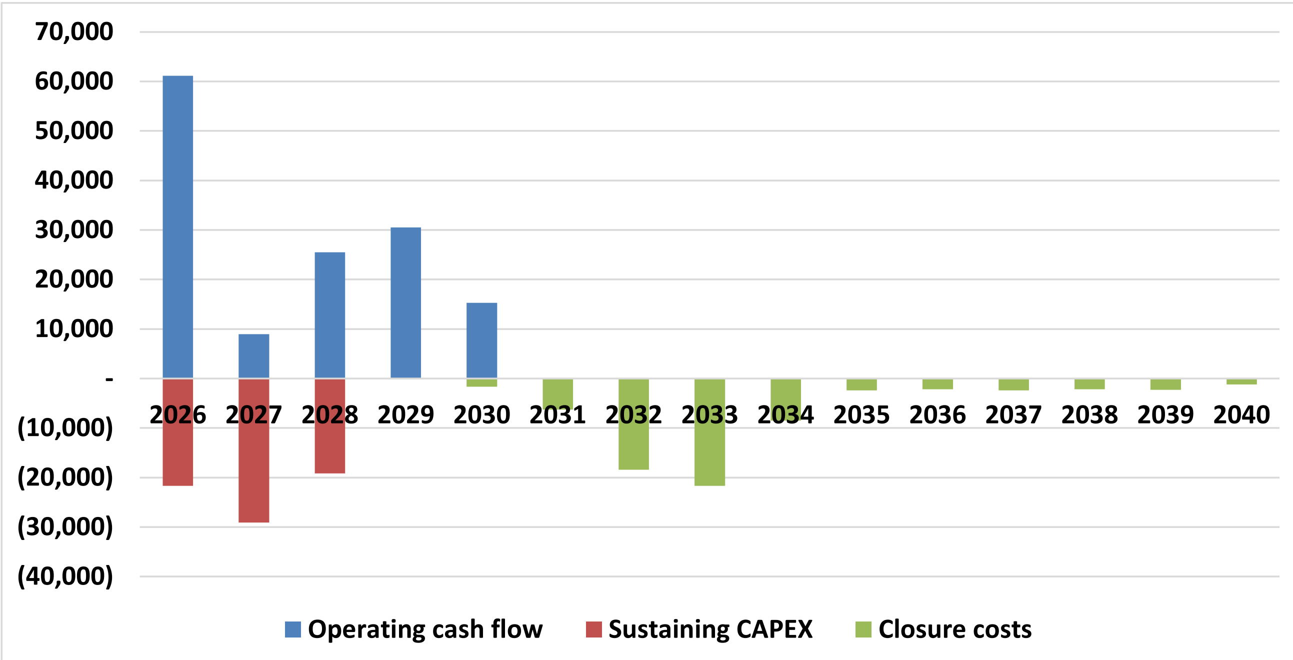


Figure 22.1: Cash Flow Profile for Eagle Mine

22.8 Sensitivity Analysis

The sensitivity analysis evaluates the impact of changes in key variables on the after-tax NPV8% of the project. The results indicate that Eagle Mine's economic performance is most sensitive to operating costs, followed by nickel price, and then copper price. The graph and table below highlight a plus or minus 20% variance in each variable independent of the others.

Using analyst consensus metal price forecast over the life of mine (average metal prices over the forecast period of $7.93/lb nickel and $5.07/lb copper), nickel and copper comprises 90+% of revenue.

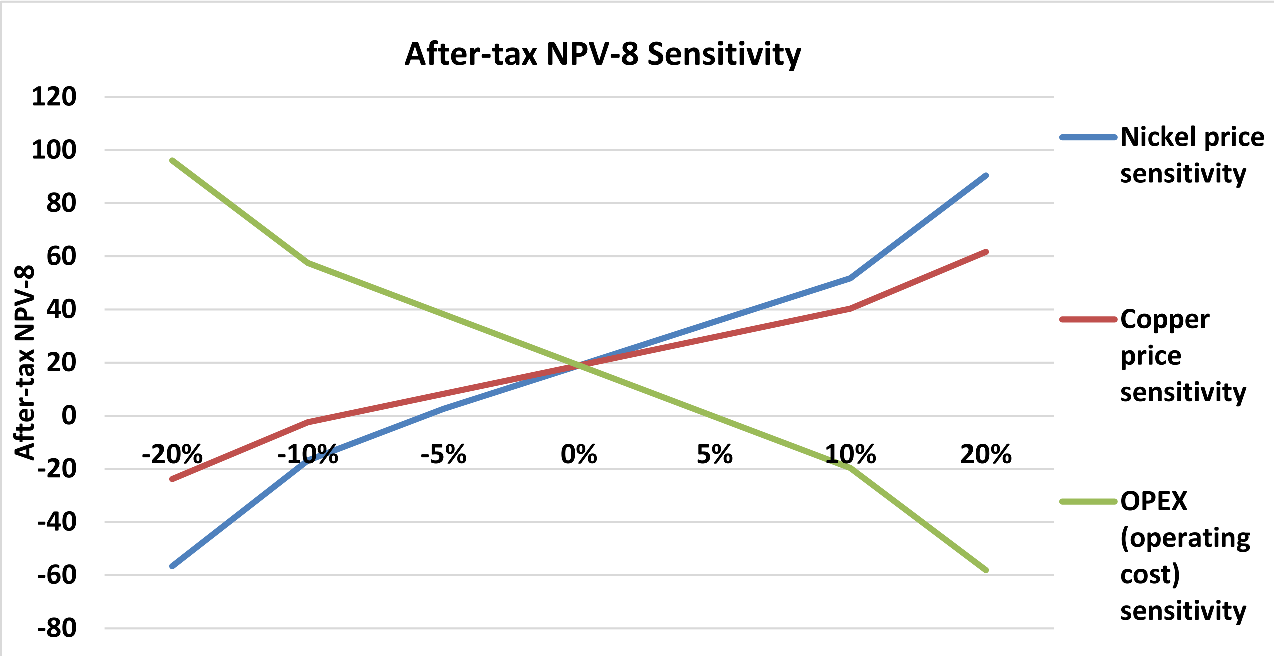


Figure 22.2: After-tax NPV-8% Assuming Various Percentage Changes of Key Variables

22.9 Additional Sensitivity Analysis – Nickel/Copper Price Pairings

An additional sensitivity analysis was carried out using constant nickel and copper price pairs over the forecast period. The range of nickel and copper price pairs were based on analyst consensus metal prices, current metal prices and market participant expectations. Metal prices for metals other than nickel and copper used analyst consensus prices for the 2026-2030 forecast period, as detailed above in this chapter.

Sensitivity analyses were performed on:

a) After-tax NPV-8%; and

b) after-tax free cash flow during the March 2026-2030 operational period of the mine.

The cash flows and NPV exclude the residual value of the mill, salvage value of equipment and release of working capital at the end of operations.

Table 22.4: Sensitivity Table In US$ Millions

After-tax NPV-8%		Nickel price (US$/lb)				
		$7.00	$8.00	$8.50	$9.00	$10.00
	$4.50	(43)	(2)	19	40	90
Copper	$5.00	(22)	19	40	61	111
price	$5.50	(2)	40	61	82	132
(US$/lb)	$6.00	19	61	82	103	153
	$6.50	40	82	103	124	174

A

After-tax free cash flow		Nickel price (US$/lb)				
Mar 2026-2030		$7.00	$8.00	$8.50	$9.00	$10.00
	$4.50	(4)	45	70	94	153
Copper	$5.00	21	70	94	118	177
price	$5.50	45	94	118	143	202
(US$/lb)	$6.00	70	118	143	167	226
	$6.50	94	143	167	192	250

B

Note: A) After-Tax NPV; and B) ,After-Tax Free Cash Flow During The Operational Period (2026-2030), At Various Nickel And Copper Price Pairs

23. Adjacent Properties

There are no adjacent properties to the Eagle Mine.

24. Other Relevant Data and Information

To the knowledge of the QPs, there is no additional information or explanation necessary to make this Technical Report understandable and not misleading.

25. Interpretation and Conclusions

25.1 Data and QA/QC

On completion of the review of Eagle's procedures and the results of their QAQC and mining reconciliation, it is the QP's opinion that the procedures in use are consistent with standard industry practices and that the drill hole database is of suitable quality for use in the estimation of Mineral Resources.

The QP notes that there is a minor risk issue due to selective sampling procedures, based on visual estimates of sulfide mineralization, where some samples within a low-grade area of the interpreted Keel mineral domain wireframe were not sampled.

25.2 Mineral Resources

The Mineral Resources have been estimated in conformity with CIM Estimation of Mineral Resources and Mineral Reserves Best Practices Guidelines (2019) and are reported in accordance with NI 43-101. The classification of Mineral Resources conforms to CIM Definition Standards, and Mineral Resources are reported in accordance with NI 43-101.

The Mineral Resources were estimated as of February 28, 2026, constrained within conceptual geological wireframes, depleted appropriately to reflect mining, and are reported inclusive of Mineral Reserves. The reporting of estimates takes into consideration metallurgical recoveries, concentration grades, transportation costs, smelter treatment charges, and forecasted metal prices in determining economic viability.

Combined Measured and Indicated Mineral Resources for all deposits total 3.3 Mt at a grade of 1.28% nickel and 0.97% copper. Inferred Mineral Resources total 132 kt at 0.93% Ni and 0.71% Cu.

At the selected resource reporting cut-off, the QP considers the resource to have reasonable prospects for economic extraction, with no known environmental, permitting, legal/title, taxation, socio-economic, marketing, political, or other factors expected to materially affect the estimate.

It is the QP's opinion that the MRE is representative of the supporting data, but there are some risks to the estimates, which may include the following:

- Mineral domain models are interpreted from drill hole data and are subject to change with new information or re-interpretation at different cut-off values. Changes in modeling cut-offs could increase or decrease mineralized volumes.
- No mining has occurred in the Keel yet, and the nature of mineralization and grade continuity has yet to be confirmed.
- Some drill core intervals within the low-grade area of the Keel were not sampled and were assigned values of half detection limits during grade estimation.

- Different grade estimation methodologies can be used to support an MRE, and variations in the approach, including estimation parameters and outlier controls used, can have a material impact on the resource estimate.
- Changes in metal prices and mining costs can vary significantly over short periods of time, which has the potential to materially impact the MRE.

25.3 Mineral Reserves and Mining

The Eagle Mine is an underground mine that has been in continuous operation since commercial production was achieved in 2014. The mine produces approximately 2,000 tpd of nickel-copper ore.

The mine presently has two active zones called the Eagle East and Keel zones. Most of the underground sustaining capital expenditures are planned for the development of the Keel.

According to the LOM plan, the Mineral Reserves will be exhausted in 2030, when mine closure is anticipated.

Eagle and Eagle East have low geological and operating risks as they are established mining zones with years of operating history. Keel, on the other hand, is a new production zone that the mine started to develop in 2025 and consequently has a higher degree of risk related to geology and operations.

25.3.1 Geomechanics

Eagle Mine currently manages ground control through accumulated geotechnical information, monitoring, stability forecast models, and different programs for collecting and assessing geotechnical data. The LOM layout and sequence in Eagle East was developed based on as-built experience and previous stability assessments completed for the Eagle East orebody. The Keel LOM layout and sequence were developed based on experience from Eagle East, available geotechnical data in the Keel, and assessments of different LOM options in Keel.

The following geomechanical risks may impact the Mineral Reserves:

- The current LOM layout and sequence have not been assessed numerically, and indications of pillar stability and stress damage are based on assessment of different LOM trade-offs for Keel.
- The longitudinal stopes with strike lengths >35 m at Keel have a higher likelihood of experiencing increased dilution and may require paneling.
- Geotechnical data available in Keel is based on capture from non-oriented resource drill holes. Not all geotechnical parameters are available for every resource drill hole.
- The characteristics of lithological contacts in Keel are likely to be poor in some areas and may impact the local stability of stopes and drifting.
- HW access drifts associated with longitudinal stopes in Keel may experience increased damage and be difficult to re-enter after stope blasts.

25.3.2 Mineral Reserves and Mining Method

Mineral Reserves have been developed from the estimate of Mineral Resources after consideration for mine design and modifying factors as described in Section 15, and QP interpretations are summarized below:

- The data verification procedures used at Eagle Mine comply with industry standards and are adequate for the purposes of Mineral Reserves estimation.
- The Technical Services Department at Eagle Mine prepared the mine design, mine plan, and Mineral Reserves estimate under the supervision of the QP responsible for the estimate.
- The Mineral Reserves estimate for the Project has been prepared in accordance with industry best practices and is compliant with the 2019 CIM Definition Standards.
- The long-term metal prices and exchange rate used to estimate the Mineral Reserves are reasonable.
- No indications of mining, metallurgical, infrastructure, permitting, or other relevant factors that could materially affect the Mineral Reserves estimate were noted during the preparation of this report.
- The Keel presents a greater level of operational risk compared to other zones, due to the absence of prior mining experience in this area.
- Eagle Mine employs appropriate mining methods for the Eagle East, Lower and Middle Keel for the mining conditions where they are applied. For Upper Keel, additional geological and geotechnical investigations within the area will determine whether the currently planned LSLOS method will be maintained or replaced with a more appropriate alternative.
- The underground infrastructure, mine services, and fixed equipment are appropriate for the scale of the underground operation. During the site visit, the QP observed that these installations were of high quality, in working order, and functioning normally. Eagle Mine has constructed or installed most of the required infrastructure to support operations to the end of the mine life.
- The number of units in the equipment fleet and the types, marks, and models are appropriate for the production rate, mining methods, and development requirements at Eagle Mine. The QP reviewed the underground equipment fleet and observed, during his site visit, many of the machines in operation.
- The personnel organization at Eagle Mine is appropriate for the scale of the underground mining operation.

25.4 Metallurgy and Recovery Method

Historical test programs have covered various ore zones, including the Eagle, Eagle East, and Keel zones. Through past production and performance monitoring, the mill operation has developed a solid understanding at the production level of the variation in ore characteristics of these different zones.

The Humboldt Mill, as it is currently configured, will be able to process the ore as described in this Technical Report. The processing facility operates at or near the metallurgical budget. The remaining Mineral Reserves are similar to the material already processed, with the exception of the Keel zone, which is lower-grade material. The processing facility will have no issues treating this incoming material, as it maintains a consistent grade/performance relationship with other Eagle ore. Keel ore fell in the hard range of hardness and is more competent than Eagle East ore as per the SGS grindability testwork. This may result in variation in energy demand and/or ore throughput in the ball mill as compared to treating historical ores.

25.5 Tailings Management

A well-established tailings deposition methodology exists at the HTDF. An effective monitoring program is in place to inspect and monitor the operation, structural integrity, safety, and environmental performance of the facility.

The tailings deposition plan shows that sufficient capacity exists in the HTDF to dispose of tailings produced at the Humboldt Mill through the LOM with tailings deposited at or below an elevation of 461.8 meters (1,515 feet) amsl, which is the maximum permitted tailings elevation. About 2.0 million cubic meters (2.6 million cubic yards) of capacity is available up to an elevation of 461.8 meters (1,515 feet) amsl as of December 31, 2025, to accommodate the estimated in-place tailings volume of 1.7 million cubic meters (2.2 million cubic yards) to be produced from December 31, 2025, through the remaining LOM at an assumed in-place dry density of 1.9 tonnes per cubic meter.

25.6 Infrastructure and Services

The established infrastructure and services to support the Eagle Mine and the Humboldt Mill are adequate for the continuation of operations until mine closure.

25.7 Environmental and Social

The Eagle Mine Site and Mill Site are well managed from an ESG perspective. Since the start of operations, few exceedances of discharge permit requirements have been observed at either site. Closure modeling is in progress, and plans are in place for both sites. Existing environmental models are routinely updated as tailings production estimates are increased and additional tailings slurry is added to the HTDF. Although the exact duration of treatment time increases or decreases slightly as a function of changes to the mine plan, all models to date indicate that the Mill site can achieve closure criteria within several years of the end of operations.

25.8 Cost Estimates

Quantities and cost estimates are of a high level of confidence as long as production rates are maintained. Operating quantities are well defined and understood, as are mining and processing productivities. Unit cost estimates are based on supply contracts and operating history. Little risk of operating cost variances is anticipated, aside from periodic spikes in the unit prices of certain commodities and supplies. The QP considers the forward-looking estimates to be of sound basis and reasonable for continued operations of the mine and mill.

26. Recommendations

26.1 Mineral Resources Estimates

The QP has the following recommendations for Talon, which are expected to be considered by operations management and, as such, have not been costed out individually.

- Sample and assay any available core that was not sampled within the Keel mineral domain volume and establish boundary limits for future drill programs to ensure that all potential mineralization within areas of interestis fully sampled.
- Future model updates are recommended to include sample data from the 7 holes acquired after the data cut-off date and to incorporate any new mapping and geological data from the Keel once mining begins.
- Additional infill drilling is recommended to improve geological understanding, increase confidence in grade continuity, and support upgrading remaining Inferred material to Indicated (and potentially refine mineralized volumes).
- The effort associated with sampling historic core and updating the geology and mineral resource models can be completed internally by Eagle. Depending on the amount of available core, standard laboratory costs per sample would apply and could total between $10,000 to $50,000. The cost of potential infill drilling depends on the quantity of planned drillholes and amount of available historic core. Preliminary costs could vary between $300k to 600k USD (based on 15 to 30, 100m length holes at $200/m USD).

26.2 Mineral Reserves and Mining

26.2.1 Geomechanics

For future study stages, the following is recommended:

- Reconcile existing geotechnical data within and near the Keel ore body, identify data gaps, and collect additional information to close existing parameter uncertainty (e.g., downhole televiewer data to reduce uncertainty regarding structural orientations).
- After data reconciliation (previous bullet), update and revise stability assessments (3D numerical model, backfill strength estimates, pillar stability estimates, footwall offset stability, etc.) based on the current LOM. Review the LOM layout (stope sizing, pillar dimensions, etc.) and sequence based upon the revised assessments.
- The location and orientation of some stope accesses should be reviewed to mitigate or remove challenges related to stability.
- Evaluate the typical overbreak and dilution experienced in Eagle East as a check on ELOS estimates assumed for the LOM stopes.

- The effort associated with the geomechanics recommendations can be completed internally by Eagle. If completed by external consultants, the engineering cost associated may go up to 200,000 USD (dependent upon the gaps identified from the data reconciliation stage). This cost does not include any drilling that may be necessary (dependent on the findings from the data reconciliation)

26.2.2 Mineral Reserves and Mining Method

The following recommendations are made by the QP for Mineral Reserves and Mining Methods:

- The Mineral Reserves estimate reflects risk due to the significant proportion of Probable Reserves (99%) compared to Proven Mineral Reserves. It is recommended that Eagle Mine focus on underground infill drilling within key deposit areas to convert Probable Reserves to Proven Reserves and advance Inferred Mineral Resources to the Indicated category.
- Consider revisiting the NSR cut-off values for each zone, as both costs and mining methods vary across different zones.
- For future Mineral Reserves estimates, investigate whether closure costs and sustaining capital expenditures for the mine and processing plant could be relevant costs for determining the NSR cut-off values. Continue to use all three types of cut-off NSR values (full-cost, marginal cut-off incremental) in the future reserves estimation. For future Mineral Reserves estimations, unplanned dilution should be incorporated across all zones and mining methods. The ELOS estimation should be applied directly within the DSO framework to derive dilution tonnage and grade from the BM. Continue analyzing modifying factors for future Mineral Reserves estimates to ensure they adequately reflect actual operating results. Verify the estimated variations in dilution whereby ELOS increases with vein width and shallower dips. eConduct an economic evaluation of relevant areas and operational levels to ensure profitability is achieved.eEvaluate the performance (dilution, recovery, stability) of the initial Upper Keel stopes and modify design parameters as necessary for subsequent stopes within the zone.eIf the results of the paste fill study are convincing, accelerate the implementation of the paste fill system to enable the mine to benefit from its advantages.
- Continuation of independent audits on a regular basis of Mineral Reserves estimation and mining methods.
- The Ground Control Management Plan and Crown Pillar Management Plan are effective tools utilized by Eagle and should be continued throughout the LOM. These plans should be periodically reviewed and approved by Eagle Mine management.

26.3 Mineral Processing and Recovery Method

Because Keel ore is low grade and more competent, it is recommended that mill operations closely monitor its actual performance and throughput. This will allow comparison with historical production data and supports trend forecasting.

A 1% adjustment factor has been applied to account for the anticipated increase in recovery from the high-pressure slurry ablation (HPSA) unit, which is currently being commissioned. It is recommended to begin operating the HPSA unit to achieve these recovery improvements and continuously track its actual performance benefits

27. References

Barton, N., Lien, R., & Lunde, J. (1974). Engineering classification of rock masses for the design of tunnel support. Rock Mechanics, 6, 189–236.

Bieniawski, Z. T. (1976). Rock mass classifications in rock engineering. In Proceedings of the Symposium on Exploration for Rock Engineering, Johannesburg, November 1976.

Canadian Institute of Mining, Metallurgy and Petroleum (CIM), 2014, CIM Definition Standards for Mineral Resources and Mineral Reserves, adopted by the CIM Council on May 10, 2014. (Canadian Institute of Mining, Metallurgy and Petroleum (CIM), 2019, CIM Estimation of Mineral Resources & Mineral Reserves Best Practice Guidelines, adopted by CIM Council November 29, 2019.

Canadian Securities Administrators, Rules and Policies, National Instrument 43-101, Standards of Disclosure for Mineral Projects, Form 43-101F1 and Related Consequential Amendments, June 24, 2011.

Clark, L.M., Pakalnis, R.C. (1997). An empirical design approach for estimating unplanned dilution from open stope hangingwalls and footwalls.

Deere, D. U., and Deere, D. W. (1989). Rock quality designation (RQD) after twenty years (Contract Report GL-89-1). U.S. Army Corps of Engineers, Waterways Experiment Station.

DNRE. 2010. Part 632, Nonferrous Metallic Mining, Mineral Mining, 1994 PA 451, for Kennecott Humboldt Mill Project, Permit Number MP 01 2010, with amendments annotated. Michigan Department of Natural Resources and Environment, Lansing, Michigan. February 9.

Eagle Mine (2022a). Upper Keel Geotechnical Summary.

Eagle Mine (2022b). Eagle Mine Ground Control Management Plan. Version 11.

Eagle Mine (2022c). Standard Operating Procedure. System: Geotechnical Core Logging

Eagle Mine (2023). Upper Eagle East Expansion. Issued to the Michigan Department of Environment, Great Lakes, and Energy on November 7, 2023.

Eagle Mine (2024). Keel Stope Sizing Recommendations. Issued Jan 29, 2024.

Eagle Mine LLC. 2021. GISTM Consequence Classification for the Eagle Humboldt Tailings Disposal Facility. December 6.

Eagle Mine. 2024. Eagle Mine Paste Backfill Project, Mine Permit Amendment Application. Submitted to the Michigan Department of Environment, Great Lakes, and Energy, Lansing, Michigan, by Eagle Mine LLC, Champion, Michigan. December 2024.

Eagle Mine. 2026a. Q4 2025 Benchmark Deviations – Humboldt Mill, Marquette County (MP 01 2010). Report submitted to Michigan Department of Environment, Great Lakes, and Energy, Lansing, Michigan, by Eagle Mine LLC, Champion, Michigan. January 21.

Eagle Mine. 2026b. Groundwater Discharge Permit (GW1810162) Application. Permit application submitted by Eagle Mine LLC, Champion, Michigan, to the Michigan Department of Environment, Great Lakes and Energy, Lansing, Michigan. January 20.

EGLE, 2022a. Authorization to Discharge under the National Pollutant Discharge Elimination System (NPDES), Permit No. MI0058649. State of Michigan, Department of Environment, Great Lakes, and Energy, Lansing, Michigan. July 30.

EGLE, 2022b. Groundwater Discharge Permit GW1110907, Sewerage System, located at 6510 AAA Road, Michigamme, Michigan. State of Michigan, Department of Environment, Great Lakes, and Energy, Lansing, Michigan. September 29.

EGLE, 2024a. Groundwater Discharge Permit for Eagle Mine, GW1810162. State of Michigan, Department of Environment, Great Lakes, and Energy, Lansing, Michigan. July 30.

EGLE, 2024b. Permit to Install, 405-08C, located at 4547 County Road 601, Champion, Michigan 49814. Michigan Department of Environment, Great Lakes, and Energy, Air Quality Division, Lansing, Michigan. June 26.

EGLE, 2025. Permit to Install, 50-06D v2.0, located at 6510 AAA Road, Michigamme Township, Michigan 49861. Michigan Department of Environment, Great Lakes, and Energy, Air Quality Division, Lansing, Michigan. May 15.

EGLE. 2026. 2025 Financial Assurance Cost Estimate Update – Eagle Mine and Humboldt Mill. Email correspondence from Melanie Humphrey, Michigan Department of Environment, Great Lakes, and Energy, Lansing, Michigan, to Rob Beranek, Eagle Mine LLC, Champion, Michigan. February 26.

EPA, 2025. Paste Backfill Well. Email correspondence from Stephan Jann, US Environmental Protection Agency, Region 5, to Eagle Mine LLC, Champion, Michigan. May 13.

Golder Associates Ltd. (2005). Eagle Project Geotechnical Study. Reference No. 04-1193-020.

Golder Associates Ltd. 2020. Lundin Mining Corporation – Eagle Mine, In Pit Tailings Disposal – Consolidation Modeling. Report prepared for Golder Associates Inc., March.

Hall, B., Manolopoulos, H., Hurley, J., Schauer, J., St. Louis, V., Kenski, D., Graydon, J., Babiarz, C., Cleckner, L., and Keeler, G. 2005. Methyl and total mercury in precipitation in the Great Lakes region. Atmospheric Environment 39:39, 7557-7569.

Henderson, M. 2026. Eagle Tailings Disposal Facility, Independent Tailings Review Report No. 4. Report submitted to Juan Andrés Morel, Lundin Mining Corporation, by Mike Henderson, Independent Tailings Reviewer, Tetra Tech. January 28.

Lundin Mining Corporation. (2023). NI 43-101 Technical Report on the Eagle Mine, Michigan, U.S.A., dated February 22, 2023.

Lundin Mining Corporation. (2025). aif-lmc-ye-2024-final. Annual Information Form February 19, 2025

McCracken, A., & Stacey, T. R. (1989). Geotechnical risk assessment for large-diameter raise-bored shafts. Transactions of the Institution of Mining and Metallurgy, Section A: Mining Industry, 98, A145–A150.

MDEQ, 2007. Part 632, Nonferrous Metallic Mineral Mining, 1994 PA 451, Permit Number MP 01 2007 for Eagle Project, with amendments annotated. State of Michigan Department of Environmental Quality, Lansing, Michigan. December 14.

MDEQ, 2018. Humboldt Mill Mining Permit Application Amendment Request Final Decision – MP 01 2010. Email correspondence from the State of Michigan Department of Environmental Quality, Lansing, Michigan, to Eagle Mine LLC, Champion, Michigan. October 16.

Michigan Department of Environment, Great Lakes, and Energy. 2022. Authorization to Discharge under the National Pollutant Discharge Elimination System (NPDES), Permit No. MI0058649. July 30.

Michigan Department of Environmental Quality. 2018. Humboldt Mill Mining Permit Application Amendment Request Final Decision – MP 01 2010. Letter from H Fitch to J Nutini, Eagle Mine LLC. October 16.

Michigan Department of Natural Resources and Environment. 2010. Nonferrous Metallic Mineral Mining Permit Number MP 01 2010. February 9.

Mitchell, R. J. (1991). Sill mat evaluation using centrifuge models. Mining Science and Technology, 13, 301–313.

Nickson, S.D. (1992). Cable support guidelines for underground hard rock mine operations. Thesis for master of applied science in the faculty of graduate studies at the University of British Columbia.

Open House Management Solutions (Pty) Ltd. (2024). Lundin Mining Eagle Mine Operations: Life of Mine Numerical Modeling Assessment. Reference No. OHMS_LM_Eagle Mine_01_2024.

Potvin, Y., Hudyma, M., and Miller, H.D.S. (1989). Design guidelines for open stope support. CIM, 82(926).

Voconiq. 2025. Local Voices, Pulse Survey Results, Oct./Nov. 2025.

WSP (2022). Technical Memorandum: Eagle East Geotechnical Support. Reference No. 22513889-006-TM-RevA-2000.

WSP (2024). Technical Memorandum: Eagle East Stope Sizing Review and Induced Stress Comments. Reference No. 22513889-009-TM-RevA-2000

WSP 2023c. Application of water cover to limit pyrrhotite oxidation in the Humboldt Tailings Disposal Facility, Eagle Mine, Michigan. Technical Memorandum 31404636.001-001-TM-1. Submitted to Eagle Mine LLC, Champion, Michigan, by WSP USA, Lakewood, Colorado. November 16.

WSP 2024b. Geochemical Characterization of Cemented Paste Tailings. Report 31405687.001-002-RPT-0. Submitted to Eagle Mine LLC, Champion, Michigan, by WSP USA, Lakewood, Colorado. October 25.

WSP 2025. 2024 State of the Humboldt Tailings Disposal Facility, Eagle Mine, Michigan. Draft Report 31405687.9347-001-RPT-A. Submitted to Eagle Mine LLC, Champion, Michigan, by WSP USA, Lakewood, Colorado. February 24.

WSP 2026. 2025 State of the Humboldt Tailings Disposal Facility, Eagle Mine, Michigan. Draft Report 31405687.4269-001-RPT-A. Submitted to Eagle Mine LLC, Champion, Michigan, by WSP USA, Lakewood, Colorado. February 10.

28. Date and Signature Page

"*Bill Bagnell*" {signed and sealed}

Bill Bagnell, P.Eng. (SK) — Signing Date: April 29, 2026

WSP Canada Inc. — Effective Date: February 28, 2026

"*Brian Thomas*" {signed and sealed}

Brian Thomas, P.Geo., (ON, NFLD) — Signing Date: April 29, 2026

WSP Canada Inc. — Effective Date: February 28, 2026

"*Ibrahim Karajeh*" {signed and sealed}

Ibrahim Karajeh, P.Eng., MBA, PMP, CCP — Signing Date: April 29, 2026

WSP Canada Inc. — Effective Date: February 28, 2026

"*David Jin*" {signed and sealed}

David Jin, P.Eng. (ON) — Signing Date: April 29, 2026

WSP Canada Inc. — Effective Date: February 28, 2026

"*Khalid Mounhir*" {signed and sealed}

Khalid Mounhir, P.Eng. (QC) — Signing Date: April 29, 2026

WSP Canada Inc. — Effective Date: February 28, 2026

"*James Smith*" {signed and sealed}

James Smith, P.Eng. (ON) — Signing Date: April 29, 2026

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"*Jason Obermeyer*" {signed and sealed}

Jason Obermeyer, P.E. (MI) — Signing Date: April 29, 2026

WSP USA Inc. — Effective Date: February 28, 2026

"*Devin Castendyk*" {signed and sealed}

Devin Castendyk, P.G., (WY) Signing Date: April 29, 2026

WSP USA Inc. Effective Date: February 28, 2026

"*Emilie Williams*" {signed and sealed}

Emilie Williams P.Eng. (ON, QC) Signing Date: April 29, 2026

WSP Canada Inc. Effective Date: February 28, 2026

29. Certificates

CERTIFICATE OF QUALIFIED PERSON WILLIAM BAGNELL

I, William Bagnell, state that:

(a) I am a Technical Director of Mine Engineering and Stability at:
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(b) This certificate applies to the technical report titled "Technical Report on the Eagle Mine, Michigan USA"; with an effective date of April 29, 2026 and a mineral resources and reserves effective date of February 28, 2026.

(c) I am a "qualified person" for the purposes of National Instrument 43-101 ("NI 43-101"). My qualifications as a qualified person are as follows. I am a graduate of Technical University of Nova Scotia with a B. Eng in Mining Engineering from 1996, I am a member in good standing of the Association of Professional Engineers and Geoscientists of Saskatchewan (12147). My relevant experience after graduation, for the purpose of the Technical Report, includes 29 years of experience in mining operations in underground mines, and evaluation of mineral projects nationally and internationally in a variety of commodities through 16 years of consulting experience. with a strong focus on mine design and scheduling.

(d) I have not completed a personal inspection of the property described in the Technical Report.

(e) I am responsible for Item 16.5 and portions of Sections 1, 4, 6, 12, 19, 25, 26, and 27 of the Technical Report.

(f) I am independent of the issuer as described in Section 1.5 of NI 43-101.

(g) I have had prior involvement with the Property that is the subject of this Technical Report.

(h) I have read NI 43-101 and the parts of the Technical Report for which I am responsible have been prepared in compliance with NI 43-101; and

(i) At the effective date of the Technical Report, to the best of my knowledge, information, and belief, the parts of the Technical Report for which I am responsible contain(s) all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated at London, United Kingdom, this April 29, 2026.

B Bagnell

William Bagnell; P.Eng.

CERTIFICATE OF QUALIFIED PERSON BRIAN THOMAS

I, Brian Thomas, state that:

(a) I am a Senior Principal Geologist at:
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(b) This certificate applies to the technical report titled National Instrument 43-101 Technical Report on the Eagle Mine, Michigan, USA; with an effective date of April 29, 2026 and a mineral resources and reserves effective date of February 28, 2026.

(c) I am a "qualified person" for the purposes of National Instrument 43-101 ("NI 43-101"). My qualifications as a qualified person are as follows. I am a graduate of Laurentian University with a B.Sc. in Geology from 1994, I am a member in good standing of the Association of Professional Geoscientists of Ontario (#1366). My relevant experience after graduation, for the purpose of the Technical Report, includes over 30 years of experience in mine geology and mineral resource evaluation of mineral projects nationally and internationally in a variety of commodities including 9 years of experience in base metals operations in Sudbury and 8 years of experience in gold mining operations located in northern Ontario, and 14 years of consulting experience with a strong focus on gold and base metals related projects.

(d) I have completed a personal inspection of the property, described in the Technical Report, between February 16 to 18, 2026.

(e) I am responsible for Item(s) 1.2-1.4, 1.12.1, 4-12, 14, 23, 24, 25.1, 25.2, 26.1, and 27 of the Technical Report.

(f) I am independent of the issuer as described in section 1.5 of NI 43-101.

(g) I have had no prior involvement in the project that is the subject of the Technical Report.

(h) I have read NI 43-101 and the parts of the Technical Report for which I am responsible have been prepared in compliance with NI 43-101; and

(i) At the effective date of the Technical Report, to the best of my knowledge, information, and belief, the parts of the Technical Report for which I am responsible, contain all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated at Sudbury, Ontario this 29th of April 2026.

Brian Thomas

Brian Thomas; P.Geo. (#1366)

CERTIFICATE OF QUALIFIED PERSON – Ibrahim Karajeh

I, Ibrahim Karajeh, state that:

(a) I am a Senior Principal Consultant
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(b) This certificate applies to the technical report titled National Instrument 43-101 Technical Report on the Eagle Mine, Michigan, USA; with an effective date of April 29, 2026 and a mineral resources and reserves effective date of February 28, 2026.

(c) I am a "qualified person" for the purposes of National Instrument 43-101 ("NI 43-101"). My qualifications as a qualified person are as follows: I am a graduate of the University of Jordan with a Bachelor's degree in Mechanical Engineering. I earned an MBA from the Edinburgh Business School, Heriot Watt University (Scotland). I am a Certified Cost Professional (CCP) with the AACE and a Project Management Professional (PMP), registered with the PMI. I am a registered member in good standing of Professional Engineers of Ontario (PEO), License #100050232. My relevant experience after graduation and over 25 years for the purpose of the Technical Report includes design, construction and project management for large scale and heavy industrial applications for infrastructure and industrial projects in the Oil & Gas, Pulp & Paper, Mining & Mineral Processing, and Energy & Power industrial sectors.

(d) I did not complete a personal inspection of the property described in the Technical Report.

(e) I am responsible for Item(s) 18.2, 18.3, 18.4,18.5, 18.6 and portions of Item 1,12, 25, 26, and 27 of the Technical Report.

(f) I am independent of the issuer as described in section 1.5 of NI 43-101.

(g) I have not had any involvement with the property that is the subject of the Technical Report.

(h) I have read NI 43-101 and the parts of the Technical Report for which I am responsible have been prepared in compliance with NI 43-101; and

(i) At the effective date of the Technical Report, to the best of my knowledge, information, and belief, the parts of the Technical Report for which I am responsible, contain(s) all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated at Mississaugua, ON, this 29th day of April

Ibrahim Karajeh, Professional Engineer, PEO License 100050232; PMP

CERTIFICATE OF QUALIFIED PERSON – DACHUN (DAVID) JIN

I, Dachun (David) Jin, state that:

(a) I am a Team Leader, Metallurgy at:
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Toronto, Ontario M9W 1A2

(b) This certificate applies to the technical report titled National Instrument 43-101 Technical Report on the Eagle Mine, Michigan, USA; with an effective date of April 29, 2026 and a mineral resources and reserves effective date of February 28, 2026.

(c) I am a "qualified person" for the purposes of National Instrument 43-101 ("NI 43-101"). My qualifications as a qualified person are as follows. I am a graduate of Tianjin University with a bachelor's degree in Chemical Engineering graduated in 1996. I am a registered member of Professional Engineers of Ontario (PEO), License #100145629. My relevant experience after graduation, for the purpose of the Technical Report, includes 30 years of process engineering as well as metallurgical and mineral processing projects for various commodities, including gold, silver and base metals, encompassing all phases from conceptual design through to detailed engineering).

(d) I completed a personal inspection of the property from February 16th to 17th in 2026 as described in the Technical Report.

(e) I am responsible for Item(s) 12.3, 13, 17, and portions of Item 1, 25 and 26 of the Technical Report.

(f) I am independent of the issuer as described in section 1.5 of NI 43-101.

(g) I have not had any involvement with the property that is the subject of the Technical Report.

(h) I have read NI 43-101 and the parts of the Technical Report for which I am responsible have been prepared in compliance with NI 43-101; and

(i) At the effective date of the Technical Report, to the best of my knowledge, information, and belief, the parts of the Technical Report for which I am responsible, contain(s) all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated at Toronto, Ontario this 29th of April 2026.

Dachun (David) Jin, P.Eng. PEO#100145629

LICENSED PROFESSIONAL ENGINEER
D. C. JIN
100145629
2026-04-07
PROVINCE OF ONTARIO

CERTIFICATE OF QUALIFIED PERSON KHALID MOUNHIR

I, Khalid Mounhir, state that:

(a) I am a Principal Mining Engineer at:
WSP Canada Inc.
1600, René-Lévesque West Blvd.
Montreal, QC, Canada, H3H 1P9

(b) This certificate applies to the technical report titled Technical Report on the Eagle Mine, Michigan, USA dated April 29, 2026, with an effective date of February 28, 2026 (the "Technical Report").

(c) I am a "qualified person" for the purposes of National Instrument 43-101 ("NI 43-101"). My qualifications as a qualified person are as follows. I am a graduate of Ecole Polytechnique of Montreal with a Bachelor of Science degree in Mining Engineering granted in 2006. I am a member in good standing of the Professional Engineers of "Ordre des Ingénieurs du Québec" License Number 5047938. My relevant experience after graduation, for the purpose of the Technical Report, includes over 19 years of experience of working as a mining engineer on projects involving mineral reserves estimation, mining design and planning, including 13 years in gold mining operations located in Canada and 6 years of consulting experience involving multiple mineral projects nationally and internationally.

(d) I did complete a personal inspection of the property (February 16 to 18, 2026) described in the Technical Report.

(e) I am responsible for Item(s) 15, 16.1, 16.2,16.4, 16.6, 16.7, and portions of Items 1, 11, 25, 26, 27 of the Technical Report.

(f) I am independent of the issuer as described in section 1.5 of NI 43-101.

(g) I have had no prior involvement in the project that is the subject of the Technical Report.

(h) I have read NI 43-101 and the parts of the Technical Report for which I am responsible have been prepared in compliance with NI 43-101; and

(i) At the effective date of the Technical Report, to the best of my knowledge, information, and belief, the parts of the Technical Report for which I am responsible, contain(s) all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated at Montreal, QC, Canada this April 29, 2026.

Signed by Khalid Mounhir

INGÉNIEUR Khalid Mounhir 5047938 QUÉBEC

Khalid Mounhir; P.Eng. License Number 5047938

CERTIFICATE OF QUALIFIED PERSON JAMES SMITH

I, James Smith, state that:

(a) I am a Senior Geotechnical Engineer at:
WSP Canada Inc.
6925 Century Ave, Suite 600
Mississauga, Ontario
L5N 7K2 Canada

(b) This certificate applies to the technical report titled "Technical Report on the Eagle Mine, Michigan USA"; with an effective date of April 29, 2026 and a mineral resources and reserves effective date of February 28, 2026.

(c) I am a "qualified person" for the purposes of National Instrument 43-101 ("NI 43-101"). My qualifications as a qualified person are as follows. I am a graduate of University of Waterloo with a B.ASc. in Geological Engineering from 2012, I am a member in good standing of the Professional Engineers of Ontario (#100523579). My relevant experience after graduation, for the purpose of the Technical Report, includes 14 years of experience in geotechnical engineering in the areas of underground mine stability of mineral projects nationally and internationally in a variety of commodities through 14 years of consulting experience with a strong focus on gold and base metals related projects.

(d) I completed a personal inspection of the property described in the Technical Report in April 16, 17, and 18, 2024.

(e) I am responsible for Item 16.3 and portions of Items 1, 12, 25, 26, and 27 of the Technical Report.

(f) I am independent of the issuer as described in Section 1.5 of NI 43-101.

(g) I have had prior involvement with the Property that is the subject of this Technical Report. I have provided rock mechanics consulting services for the Property periodically from 2022 to 2025.

(h) I have read NI 43-101 and the parts of the Technical Report for which I am responsible have been prepared in compliance with NI 43-101; and

(i) At the effective date of the Technical Report, to the best of my knowledge, information, and belief, the parts of the Technical Report for which I am responsible, contain(s) all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated at Mississauga, Ontario this April 29, 2026.

James Smith; P.Eng. (#100523579)

CERTIFICATE OF QUALIFIED PERSON JASON OBERMEYER

I, Jason Obermeyer, state that:

(a) I am a Vice President, Geotechnical Engineering at:
WSP USA Inc.
7245 West Alaska Drive, Suite 200
Lakewood, Colorado, USA 80226

(b) This certificate applies to the technical report titled "NI 43-101 Technical Report on the Eagle Mine, Michigan, USA", with an effective date of April 29, 2026 and a mineral resources and reserves effective date of February 28, 2026.

(c) I am a "qualified person" for the purposes of National Instrument 43-101 ("NI 43-101"). My qualifications as a qualified person are as follows. I am a graduate of the University of Texas at Austin with a Bachelor of Science degree in civil engineering (2001) and a Master of Science degree in geotechnical engineering (2002). I am a Professional Engineer in good standing and registered in the State of Michigan (License No 6201063841). My relevant experience after graduation and over 23 years of professional work for the purpose of the Technical Report includes leading or assisting with engineering evaluations, design work, and operational support for tailings and waste rock management at numerous mine sites. This work has included geotechnical characterization, seepage analysis, slope stability analysis, tailings deposition planning, reclamation cover evaluation and design, dam safety inspection, and other related work.

(d) I did not complete a personal inspection of the property described in the Technical Report. My most recent inspection of the Humboldt Tailings Disposal Facility occurred on October 28, 2025.

(e) I am responsible for Items 12.4.1, 12.5.5, 18.1, and 25.5 and portions of Items 1.8 and 27 of the Technical Report.

(f) I am independent of the issuer as described in section 1.5 of NI 43-101.

(g) Since August 2019, I have served as a representative of WSP USA Inc. in the role of Engineer of Record for the Humboldt Tailings Disposal Facility. In that capacity, I have reviewed performance-related data for the facility and assisted with engineering evaluations pertaining to the facility. Otherwise, I have not had any involvement with the property that is the subject of the Technical Report.

(h) I have read NI 43-101 and the parts of the Technical Report for which I am responsible have been prepared in compliance with NI 43-101; and

(i) At the effective date of the Technical Report, to the best of my knowledge, information, and belief, the parts of the Technical Report for which I am responsible contain all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated at Lakewood, Colorado, this 29th day of April 2026.

Jason Obermeyer, P.E. (Mi) (License No 6201063841)

CERTIFICATE OF QUALIFIED PERSON (Item 20)

I, Devin Castendyk, state that:

(a) I am a Vice President and Technical Fellow, Geologist at:
WSP USA Inc.
7245 Alaska Drive, Suite 200
Lakewood, Colorado 80226
United States of America

(b) This certificate applies to the technical report titled Technical Report on the Eagle Mine, Michigan USA; with an effective date of April 29, 2026 and a mineral resources and reserves effective date of February 28, 2026.

(c) I am a "qualified person" for the purposes of National Instrument 43-101 ("NI 43-101"). My qualifications as a qualified person are as follows:

- I am a licensed Professional Geologist in the State of Wyoming, USA, issued by the Wyoming Board of Professional Geologists, license number PG-4124.
- I am a graduate of University of Auckland, New Zealand with a PhD in Environmental Science in 2005, University of Utah with a Master of Science in Geology in 1999, and Hartwick College in Oneonta, New York with a Bachelor of Arts in Geology with Honors in 1996.
- I am a member in good standing of the Society for Mining, Metallurgy and Exploration (SME), the Acid Drainage Technology Initiative, Metal Mining Sector (ADTI-MMS), and the Nevada Water Resources Association (NWRA).
- My relevant experience after graduation, for the purpose of the Technical Report, includes over 21 years of experience as an Associate Professor of Water Resources at the State University of New York at Oneonta, USA (2005 to 2015), a Senior Geochemist at Hatch Associates, Lakewood, Colorado, USA (2015 to 2017), a Senior Geochemist at Golder Associates, Lakewood, Colorado, USA (2017 to 2022) and a Vice President at WSP, Lakewood, Colorado, USA (2023 to present).
- In 2023, I served as QP for the previous 43-101 conducted for Eagle Mine, Michigan, USA, and was responsible for Item 20.

(d) I did not complete a personal inspection of the property described in the Technical Report. I previously inspected the underground mine on September 9, 2022 and the Humboldt Tailing Disposal Facility on September 5, 2024.

(e) I am responsible for portions of sections 1, 12, 25, 26, 27 and Item 20 of the Technical Report, Environmental Studies, Permitting, and Social or Community Impact.

(f) I am independent of the issuer as described in section 1.5 of NI 43-101.

(g) I have served as Lead Geochemist on multiple studies involving the underground mine and the Humboldt Tailings Disposal Facility since 2015. Otherwise, I have not had any involvement with the property that is the subject of the Technical Report.

(h) I have read NI 43-101 and the part of the Technical Report for which I am responsible has been prepared in compliance with NI 43-101; and

(i) At the effective date of the Technical Report, to the best of my knowledge, information, and belief, the part of the Technical Report for which I am responsible contains all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated April 29, 2026.

Signed by Devin Castendyk, PhD, PG(WY)

CERTIFICATE OF QUALIFIED PERSON Emilie Williams

I, Emilie Williams, state that:

(a) I am an Independent Consults with:
WSP Canada Inc.
93 Cedar Street
Sudbury ON P3E 1A7

(b) This certificate applies to the technical report titled Technical Report on the Eagle Mine, Michigan USA; with an effective date of April 29, 2026 and a mineral resources and reserves effective date of February 28, 2026).

(c) I am a "qualified person" for the purposes of National Instrument 43-101 ("NI 43-101"). My qualifications as a qualified person are as follows. I am a graduate of McGill University with a B.Eng in Mining Engineering (2000). I hold a M.A.Sc in Civil Engineering from the University of Toronto (2002). I am a member in good standing of the Professional Engineers of Ontario (since 2019) and the Ordre des Ingénieurs du Québec (since 2004) (PEO license: 100544900). My relevant experience after graduation, for the purpose of the Technical Report, includes over 20 years of experience in underground mine planning, economic assessment and financial modeling.

(d) I did not complete a personal inspection of the property described in the Technical Report.

(e) I am responsible for Item(s) 21, 22 and portions of 1 and 15 of the Technical Report.

(f) I am independent of the issuer as described in section 1.5 of NI 43-101.

(g) I have not had any involvement with the property that is the subject of the Technical Report.

(h) I have read NI 43-101 and the parts of the Technical Report for which I am responsible have been prepared in compliance with NI 43-101; and

(i) At the effective date of the Technical Report, to the best of my knowledge, information, and belief, the parts of the Technical Report for which I am responsible, contain(s) all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated at Mississauga this April 29, 2026.

Signed by Emilie Williams

Emilie Williams; P.Eng. PEO license: 100544900 wsp.com